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24679—81

Hydraulic four-way control valves for nominal pressure to 32 MPa. Specifications

(CT 3057-81)

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6, 10, 16, 20, 32

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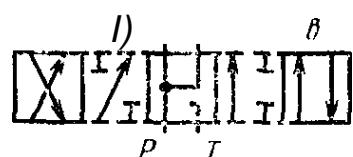
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		6	10	16	20	32
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$$\begin{array}{r} 7) - 16, \\ - 32 \end{array}$$

$$\{ >/?/? By 74 6 \\ 10)$$

$$(\begin{array}{r} 74 \\ 20 \quad 2 \end{array} = 16)$$

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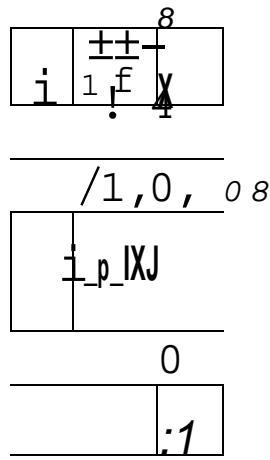
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$$\begin{array}{r} 129 \\ (10 \quad By - 6) \end{array}$$

$$(\begin{array}{r} By - 16, \\ 20 \quad 32 \end{array})$$

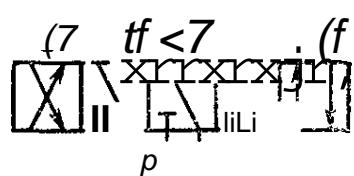
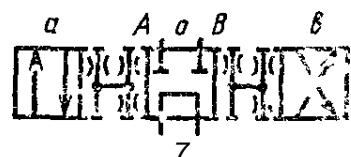
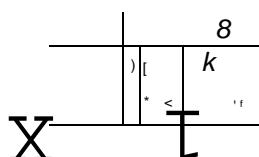
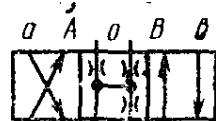


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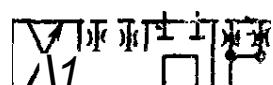
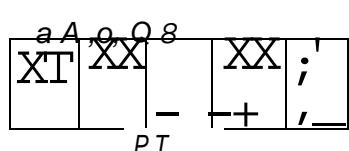
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		D_y				
		6	10	16	20	32
1,	,	(/ ²):				
20, X 32		6, BIO, X 16, X	32 (320)	32 (320)	32 (320)	32 (320)
		16, 20, 32	-	-	25 (250)	25 (250)
20, X 32		6, BID, X 16, X	32 (320)	32 (320)	32 (320)	32 (320)
		16, 20, 32	-	-	28 (280)	28 (280)
			0	0	0,5 (5)	0,5 (5)
2.		(/ ²):				
		Dy 6 10 £> 16,20	6(60)	15 (150)		
					25 (250)	25 (250)
					6(60)	15 (150)
3	,	(/ ²):				
			6(60)	6(60)	25 (250)	25 (250)
			0,6 (6)	0,5 (5)	0,8 (8)	0,8 (8)
			0,6 (6)	0,5 (5)	1,0 ()	()

		D,				
		6	10	16	20	32
104	, 54 , 64 , 64 ,			0,5 (5)	0,5 (5)	0,5 (5)
	:			0,5 (5)	0,5 (5)	0,5 (5)
	:			—	—	—
	1,2 (12) 0,4 (4)	U (12) 0,5 (5)				
	:			—	—	—
			0,6 (61) 0,2 (2)			
4.	(W(B):					
1 574	44, 74, 94, 134, 573, 573 , 574 ,	12,5	—	—	—	—
154, 573, 573	14, 24, 34, 54, 64, 64 , 84, 84 , 124, 574, 574	—				
	14, 54, 64, 64 , 154,	16	—	—	—	—
			20	—	—	—
			32	—	—	—

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	6	10	16	20	32		
24,34, 44, 74, 84, 84 , 94,124,134, 574,574 , 574 , 574	,						
14,54,64,64 , 164	,			125			
14,54,64,64 , 104	,			80			
44,84 , 94	-	-	-	63			
14,64,64 , 104	(-	-	125	-		
)	-	-	-	200		500	
	,	.3	,4	80	-	-	
				.5	,160	500	
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	D _y				
	6	10	16	20	32
	-	-	0,04 0,04	0,08 0,08	0,11 0,11
	-	-	0,06 0,06	0,10 0,10	0,13 0,13
	9,05 0,63	0,06 0,06	0,06 0,06	0,11 0,11	0,14 0,14
	0,04	0,02 0,03	-	-	-
	0,04	0,02 0,04	-	-	-
(),	-	-	2,0	2,0	2,0
			7200 15000		

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	Dy,				
	6	10	16	20	32
10 , ³ (. . . ±10):					
	1,9	3,2			
	3,5	3,2			
	—	10,2	—	—	
«0» 10) m	—	—	—	—	
	8,9	19,3			70,7
	4,5	9,7			35,4
	4,9	5,0			17,3
10) m	—	—	—	—	
	4,46	9,7			35,4
	4,4	4,7			18,1
	2,3	4,7			17,3
, ():					
	45 (4,5)	50(5)	78 (7,8)	()	150 (15)

	6	10	16	20	32
1239					,
)	()	(
		45 (4,5)			—
		120	120		—
		120	160		—
12					
		,			
				0,05	0,05
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 $D_v = 6 - 5 / ; - 10 - 12 / ; D_v = 16 - 16 / ; D_v = 20 - 32$
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 $D_y 16, 20 - 32$

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 6 (100 / 2) $D_y 10$ - 0,8 (8,0 / 2) 10
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$D = 6$, /

	(/ *)	
	10 (100)	32 (320)
,	,	-
,	(-
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:		
14, 24, 574, 574		
, 574, 574		
44, 74, 124, 574, 574 , 134, 574	30	30
34, 84, 84	30	20
573, 573	30	16
54, 64, 64 , 154	25	16
94	20	16
	15	12,5
:		
573, 573	16	12,5
64, 64 , 154	15	16

 $D = 10$, /

	(/ ^)	
	10 (100)	32 (320)
,		
,		
,		
44, 574, 574		
; 574, 574		
14, 24, 34, 74, 84, 84 , 124, 134, 574	80	60
54, 64, 64 , 94, 154, 574 , 574	80	45
573, 573	70	45
	45	25
:		
14, 24, 44, 54, 64, 64 , 84, 84 ,		
94, 124, 134, 154, 574, 574	80	65
34, 74, 573	70	45

$D_y = 16 \quad , \quad /$

	, (/ ²)		
	10 (100)	25 (250)	32 (320)
,	-	-	!
24, 34, 44, 74, 84, 84 , 94, 124, 134, 574, 574 , 574 , 574	240	180	170
14, 64, 64 , 104	160	110	100
54	145	100	90
,	-	-	-
24, 34, 44, 74, 84, 84 , 94, 124, 134, 574, 574 , 574 , 574	180	180	170
14, 64, 64 , 104	115	80	70
54	100	70	65
,	-	-	-
	180	180	170

 $D_y = 20 \quad , \quad /$

	, (/ ²)		
	10 (100)	25 (250)	32 (320)
,	-	-	-
24, 34, 44, 74, 84, 84 , 94, 124, 134, 574, 574 , 574 , 574	450	320	300
14, 54, 64, 64 , 104	250	180	160
,	-	-	-
24, 34, 44, 74, 84, 84 , 94, 104, 124, 134	450	320	300

	, (/ *)		
	\0 (100)	25 (250)	32 (320)
14, 54, 64, 64 , 574, 574 , 574 , 574	190	135	120
-	450	320	300

Dy =32 , /

	, (/)		
	10 (100)	25 (250)	32 (320)
24, 34, 44, 74, 84, 84 , 94, 124, 134, 574, 574 , 574 , 574	1050	750	680
14, 54, 64, 64 , 104	630	450	400
24, 34, 44, 74, 84, 84 , 94, 124, 134	1050	750	680
14, 54, 64, 64 , 104, 574, 574 , 574 , 574	450	320	280
-	1050	750	680

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6	10	16	20
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	D _y)	32 (320)	§	I	S	—	LO		§	*—*	(/ *)	8	LO (μ0)	to	32 (320)
14	25	120	35	150	60	290	370	45	230	320	50	290	360		
24	25	120	35	150	40	200	260	60	260	350	60	390	490		
34	25	120	35	150	60	300	370	60	260	350	60	390	490		
44	25	120	35	150	60	260	380	60	260	350	60	390	490		
54	25	120	35	150	50	260	340	45	230	320	50	290	360		
64	50	220	35	150	60	350	450	45	230	320	55	360	450		
64	50	220	35	150	60	310	390	45	230	320	55	360	450		
74	25	120	35	150	60	300	370	60	260	350	60	390	490		
84	25	120	35	150	60	300	370	60	260	350	60	390	490		
84	25	120	35	150	60	300	370	60	260	350	60	390	490		
94	35	140	35	150	70	390	490	100	610	900	70	450	565		
104	..	—	—	—	70	380	490	100	610	900	80	800	1000		
124	25	120	35	150	40	200	260	45	230	320	45	280	350		
	25	120	35	150	60	300	370	60	260	350	60	390	490		
154	25	120	35	150	—	—	—	—	—	—	—	—	—		
573	35	140	35	150	—	—	—	—	—	—	—	—	—		
573	35	140	35	150	—	—	—	—	—	—	—	—	—		
574	50	220	35	150	60	290	370	60	260	350	60	390	490		
574	25	120	35	150	60	260	380	60	260	350	60	390	490		
574	—	—	—	—	60	300	370	60	260	350	60	390	490		
574	25	—	35	150	—	—	—	—	—	—	—	—	—		
574	—	—	—	—	40	200	260	60	260	350	60	390	490		

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 $D_y = 16, 20 \quad 32$

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 $D_y = 16, 20 \quad 32$

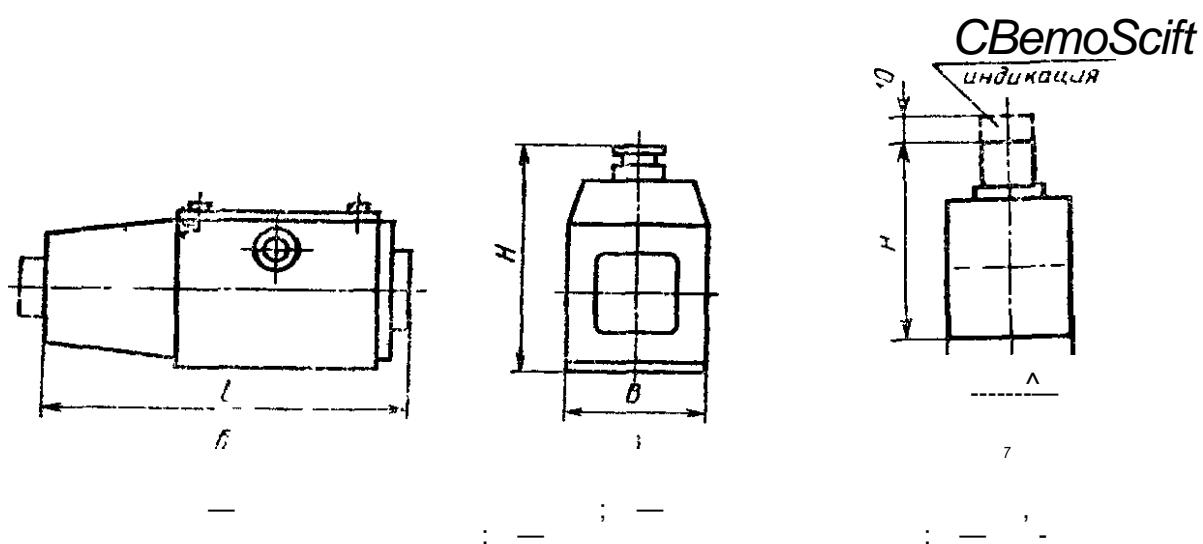
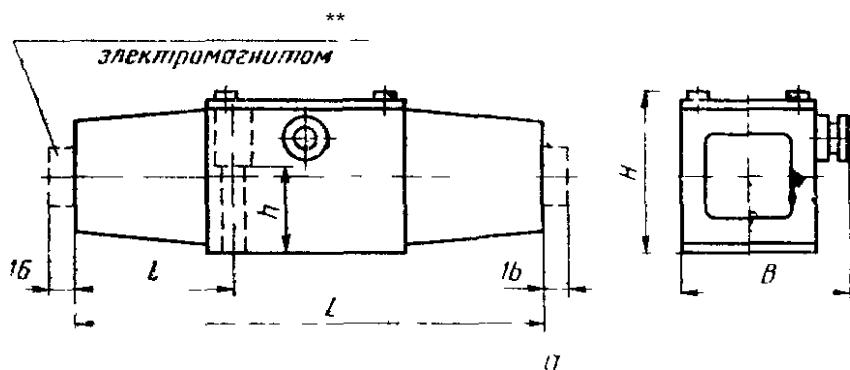
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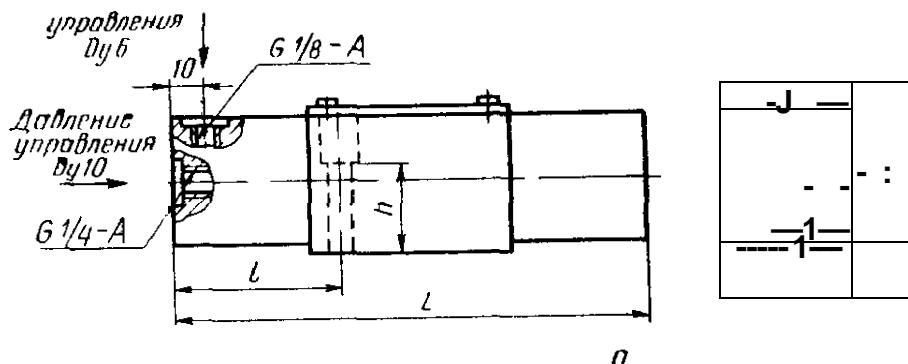
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$D_y = 6, 10$ 

D_y	L		$/$							h	
	1	16		1	1	1	1	1	1		
6	194	142	76	—	—	44	—	—	75	42	-
10	295	215	121	91	70	70	90	131	120	40	-
	257	196	102	91	70	70	90	131	140	40	-

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D =6 10

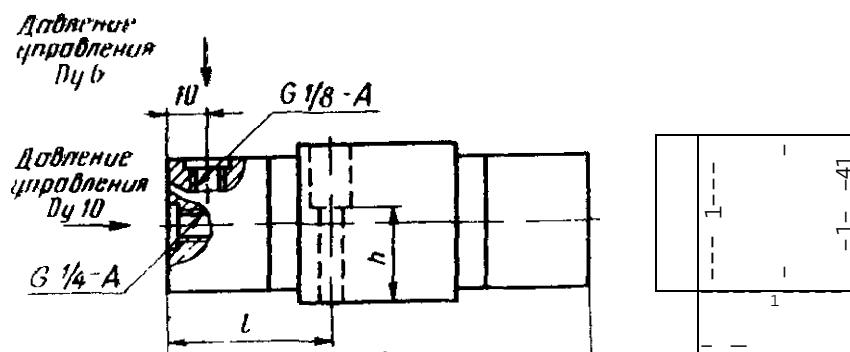
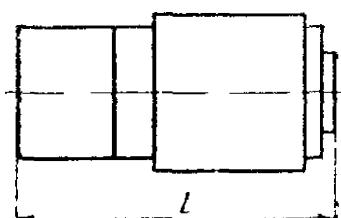
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6	155	130	44	50	56	42
10	200	170	70	90	73	40

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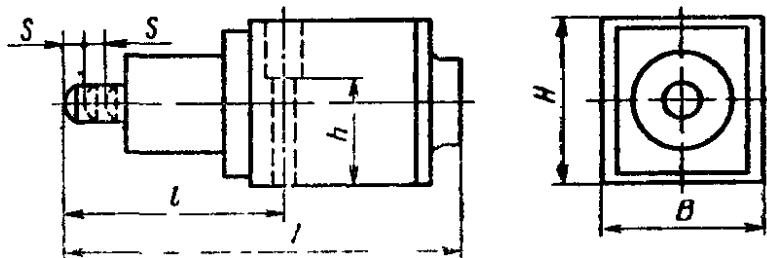
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		6	10					
6	0,4—1,2	160	125		44	50	58	42
10	0,45—1,2	200	170		70	90	73	40
	0,15—0,6	215	175		70	90	81	40

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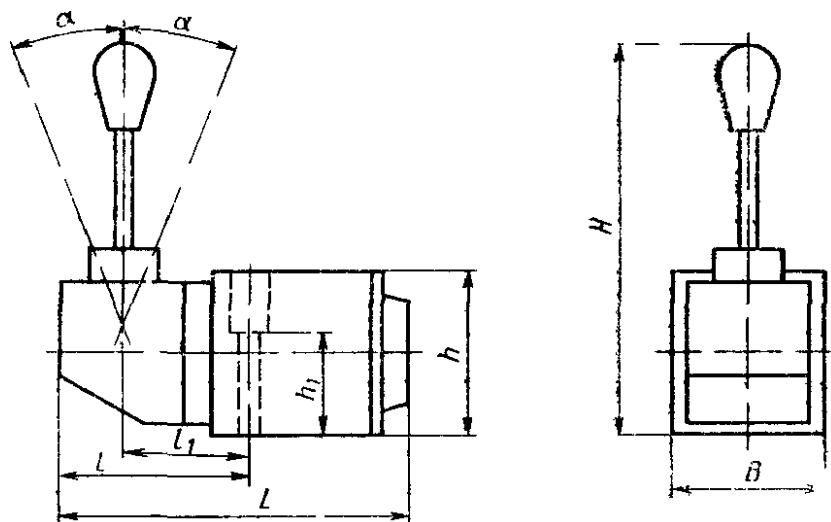
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	<i>L</i>	1					<i>S</i>
6	2 144,5		82	44	50	42	2,5
	3 157,5						
10	2 186		95	70	90	40	3,2
	3 189						

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D_y = 6 10

Размеры, мм

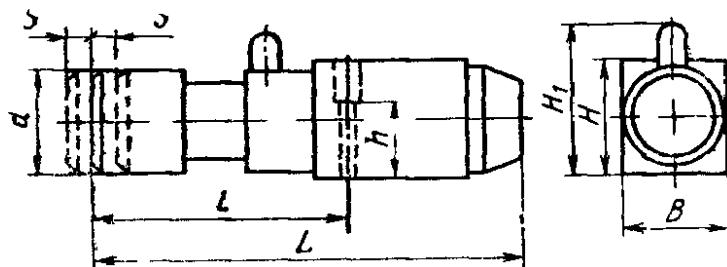
°	<i>L</i>			<i>t</i>	<i>h</i>	<i>h</i>		*
6	145	44	120	67	49	50	42	15°
10	165	70	200	70	48	90	40	21®

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$\Sigma = 6 \quad 10$

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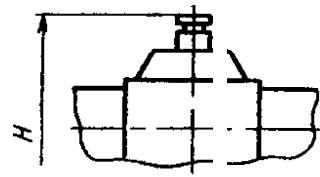
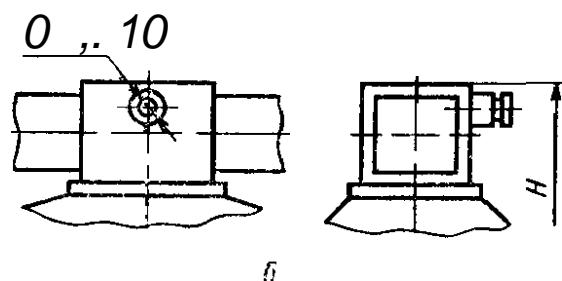
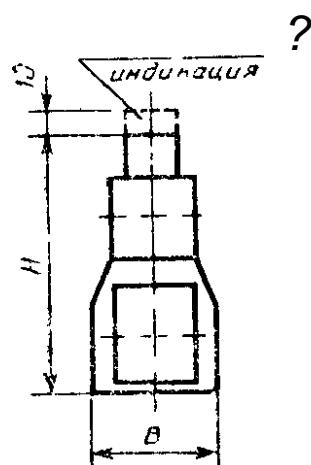
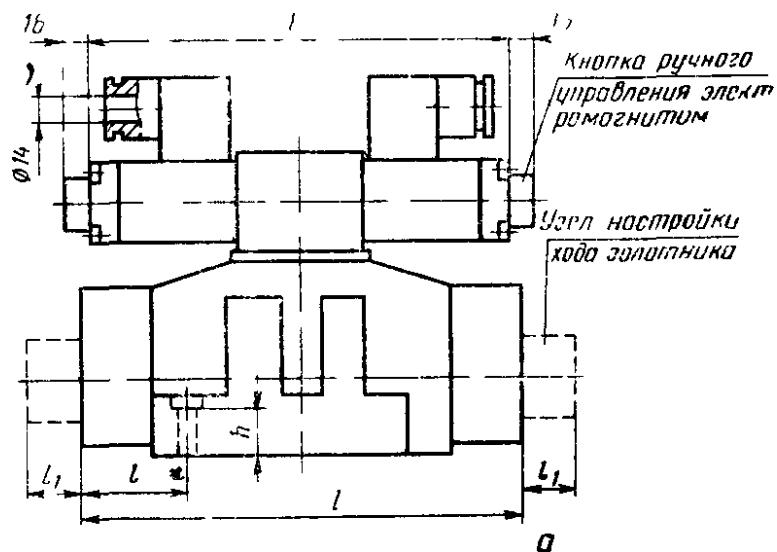
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	L				d	I	h	s
6	181	44	50	57	43	105,5	42	2.5
10	; 191	; 70	78	—	58	96,5	40	3.2

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$D_y = 16, 20, 32$

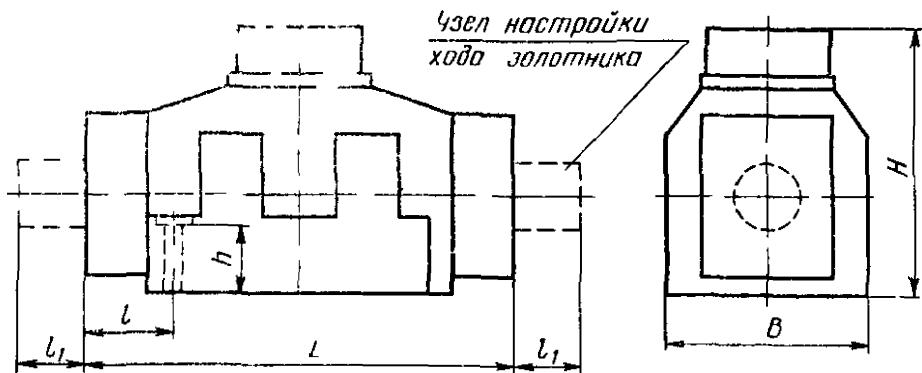


°		L		$L!$				1		11	h
		()			$\angle \Sigma$	*	6	6		
16	2	225	196	194	194	92	175	—	—	47	47
	3	196	225							47	76
20	2	282	251	295	257	118	225	202	246	49	49
	3	251	291							49	89
32	2	430	382	200	280	255	300	—	—	77	77
	3	382	434							77	129

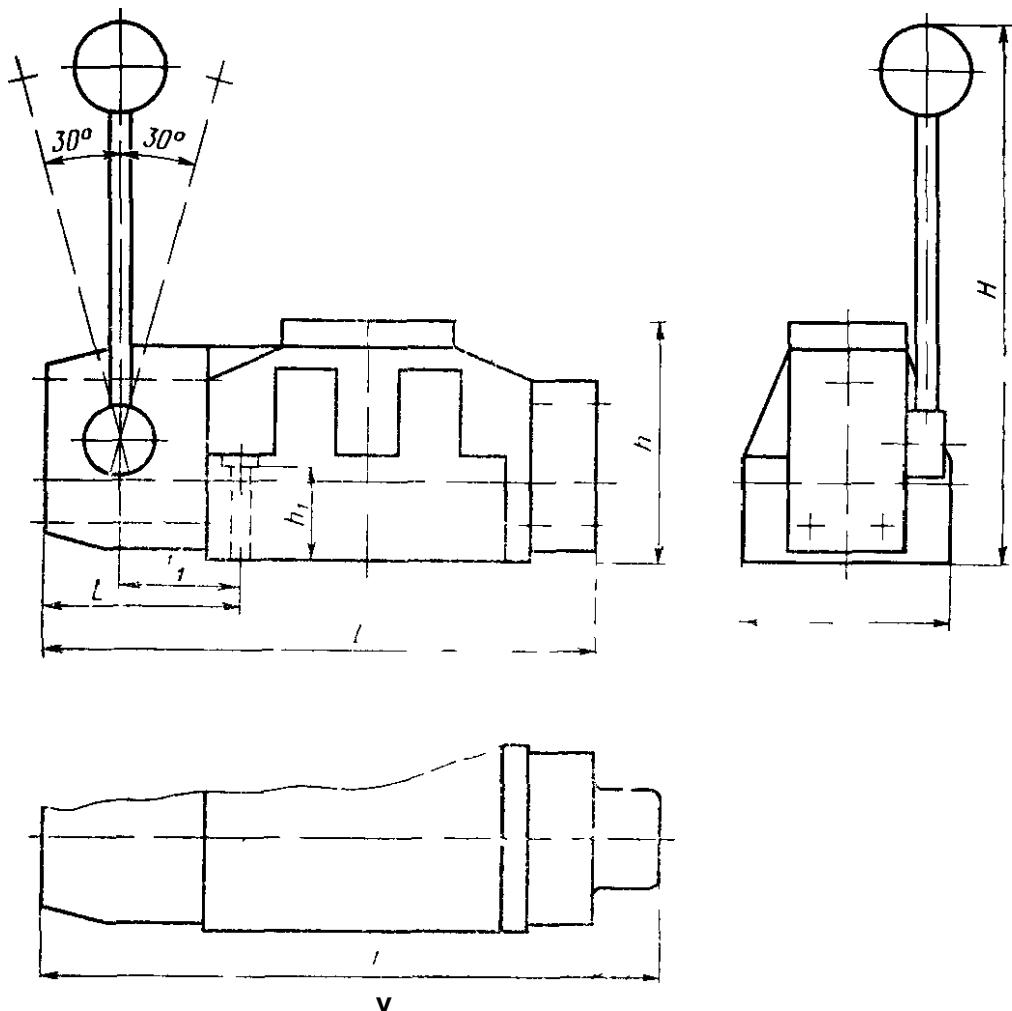
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$$D_y = 16, 20 \quad 32$$

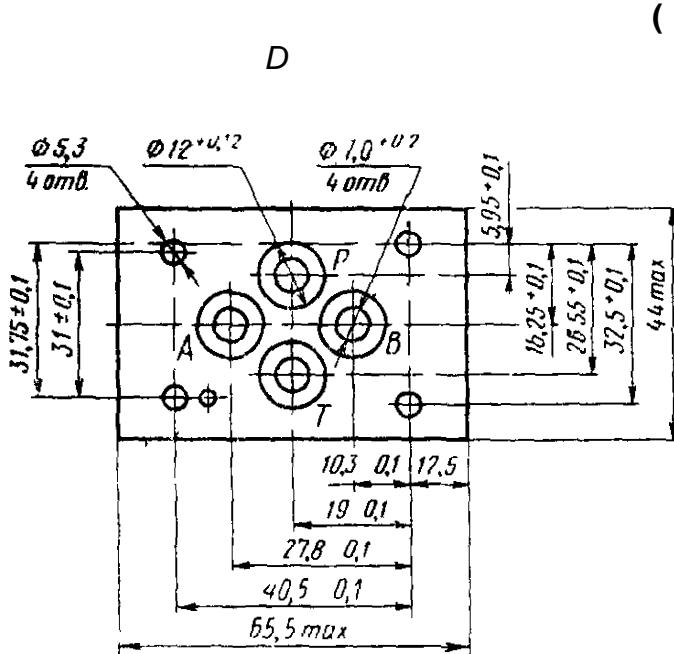


◦	(<i>L</i>		-	(1		-	<i>11</i>	<i>h</i>
16	2	225	196	92	110	47	47	44	43	
	3	196	225			47	76			
20	2	282	251	118	142	49	49	54	41	
	3	251	291			49	89			
32	2	430	382	200	195	77	77	80	49	
	3	382	434			77	129			

$D_y = 16, 20 \quad 32$


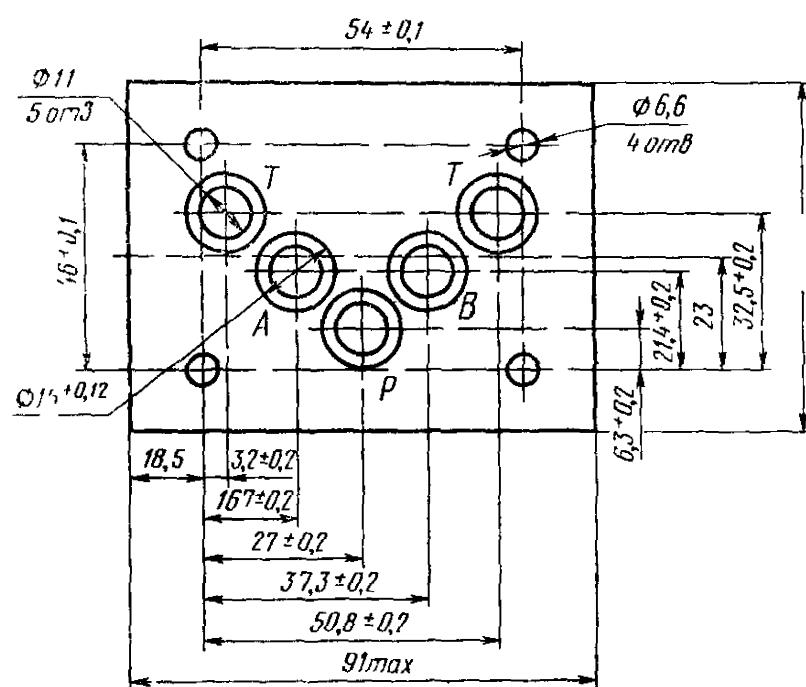
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	<i>L</i>							
°	8»	. 8,	1				<i>h</i>	Ai
16	235	265	88	54,5	92	220	100	43
20	310	340	104	59	118	330	145	41
32	465	515	158	92	200	535	195	49

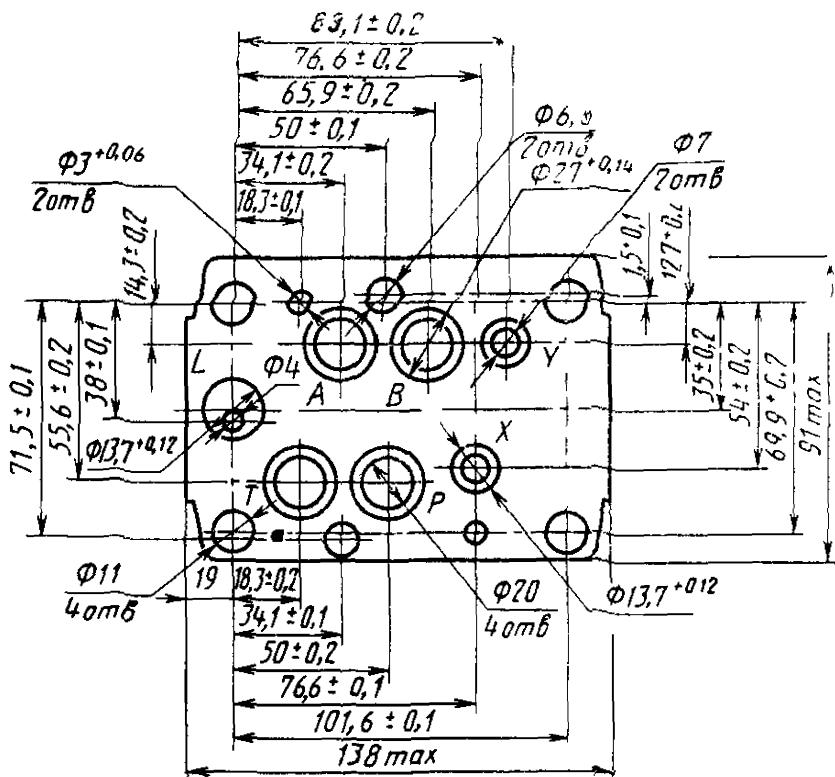
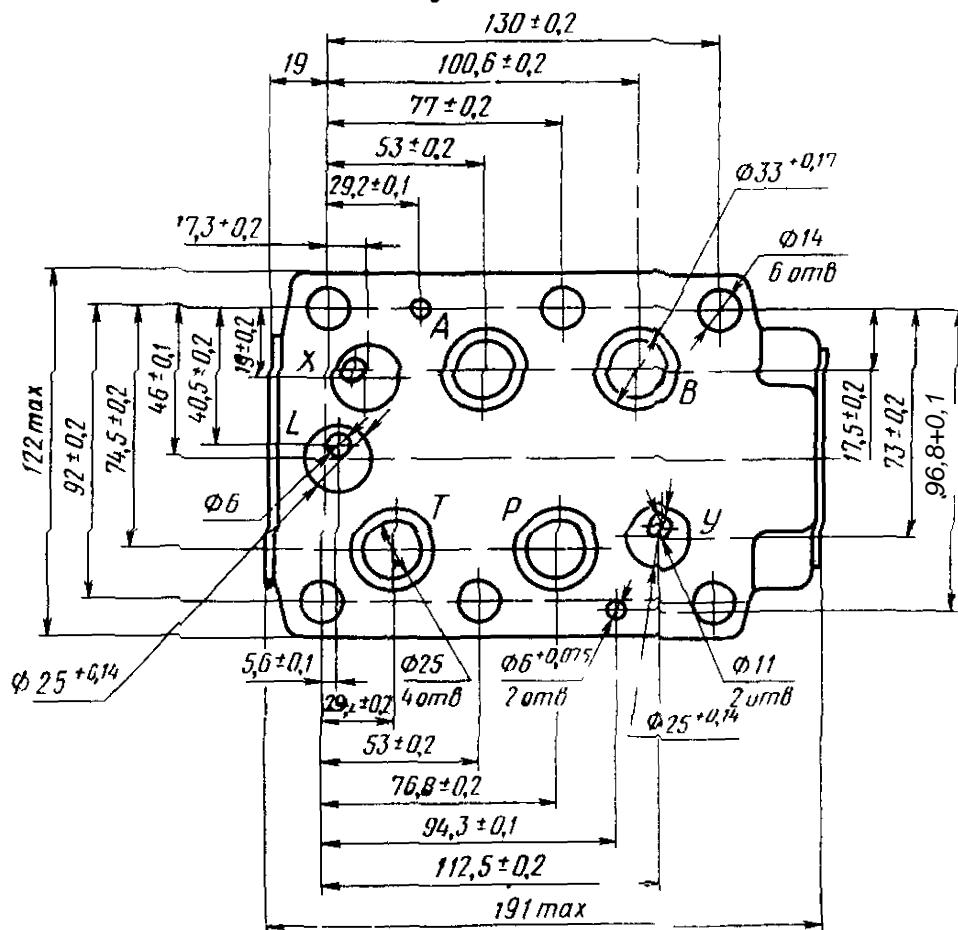


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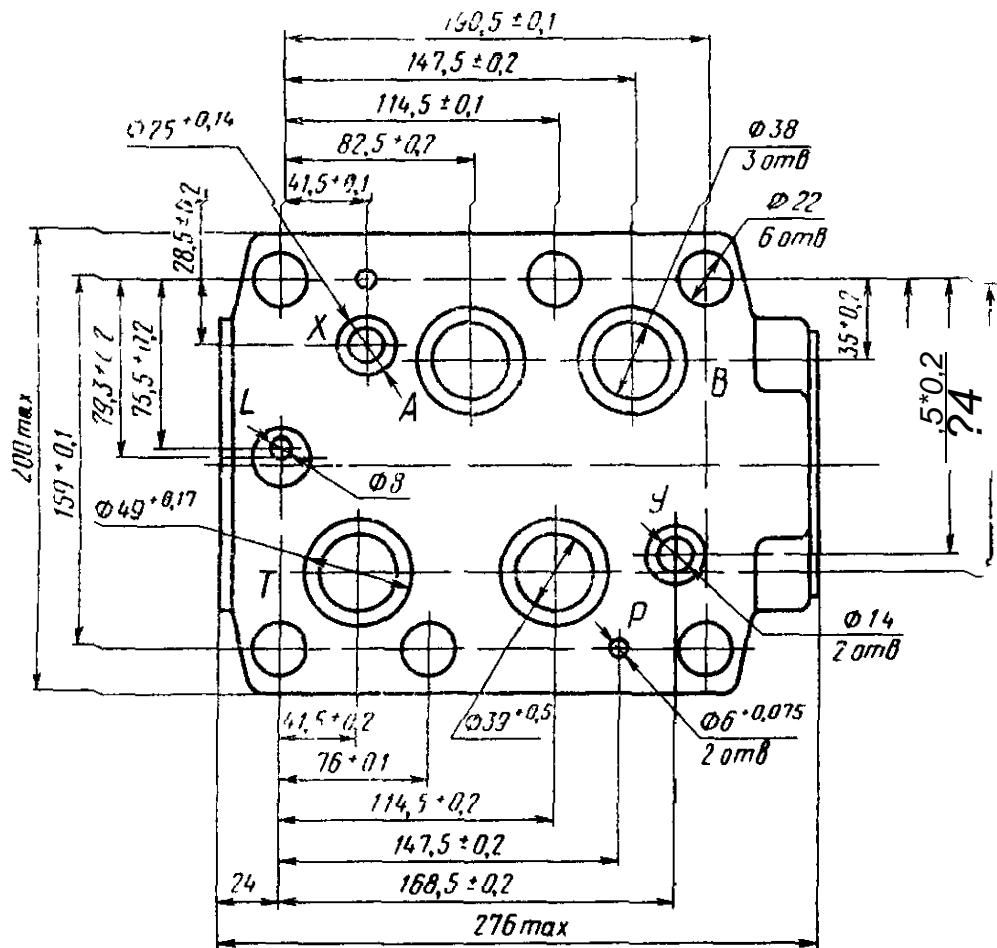
 $D_y = 10$ 

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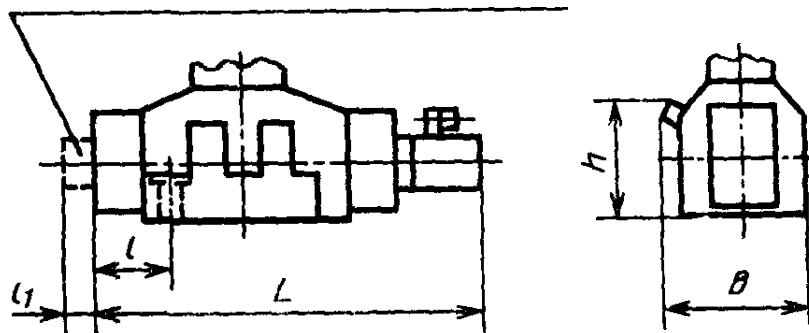
$D_y = 16$ Черт. 11
 $D_y = 20 \text{ мм}$ 

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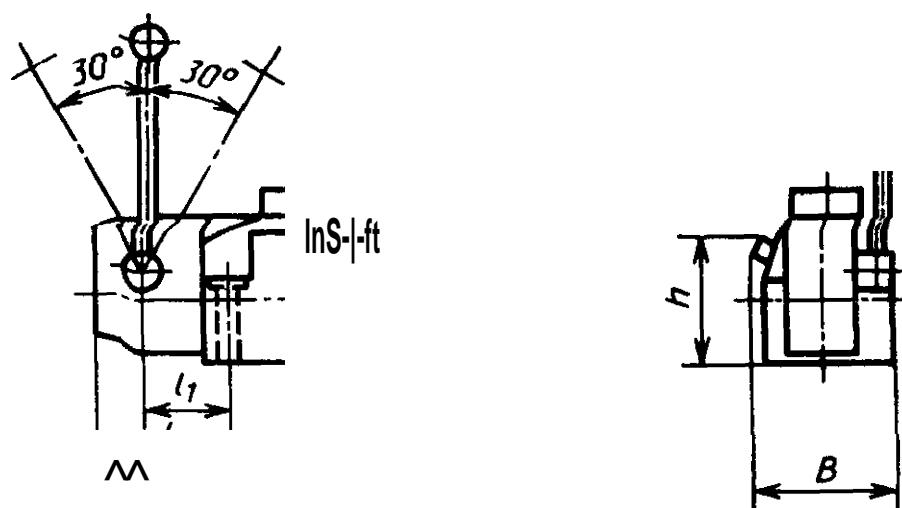
$$D_y \sim 32$$



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		L		I		h									
		()													
		-	-	-	-										
16	2 3	306 306	306 335	47 47	47 76	44	114	94	9,8 10,8	8,7 9,4					
20	2 3	390 359	359 399	49 49	49 89	54	197	107	21,3 23,3	17,4 18,1					
32	2 3	536 488	488 540	77 77	77 129	80	90ft	130	51,1 56	47,3 50,8					



◦	1	1	<i>h</i>		<i>h</i>	,
16	350	88	54,5	114	94	8,9
20	412,5	104	59	127	107	15,4
32	575	158	92	200	130	50,!

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2.4.

0,9

2.

2.5.

 $D_y=6 \quad D_y=10$

2.6.

9.032.

IV

2.7.
1,5 .

750 . — .
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2.8.
10 . — .
25 , . . 3). . 8.
2.7, 2.8. (, . . 3).
2.9. .
— 16962.1 16962.2. II
(, . . 2)
2.10. 50 % . 2.7 2.8.
2.11.

()

2.10, 2.11. (, . . 3).

3.

12.2.086. — 12.2.040
(, . . 2).

4.

9833 ;

5.

5.1. — 20245 22976.
5.2. 30—35 2/ ().
(, . . 2).

6.

6.1. — 20245.

6.2.

20245.

3 —

2 —

6.3.

8 / ,
30 ,
1 .

30 / .

(

3).

6.4.

(, . 2).

D = 6 10 — , Z_y = 16,

20 32 —

20 %

(

2).

6.5.

0,9
8 / .

6.6.

. 1.4 (. 2

. 2).

6.7.

34, 44, 74, 84, 84 , 134

(
6.8.

20 $D_y = 6$ 10 10 % 8 /
 $D_y = 16,,$
32 , . 1.4 . 2 . 8.

6.9. 8

6.6—6.9 (2).

6.10.

2

6.11.

6.12.

100

100

9×10^{-5}

6.13.

6.14.

6.15.

8

6.10—6.15. (3).

7.

7.1. , — , 15108.

; (7.2.
; (7.3.

III— 1, 2991 16536 15841 II—1

7.4.
100
1000
7.3, 7.4. (

8.

8.1.

8.2. ,
>20 (200 / ²) = 0 / ² ()
8.3.

13 17216. 0,025

8.2, 8.3. (

9.

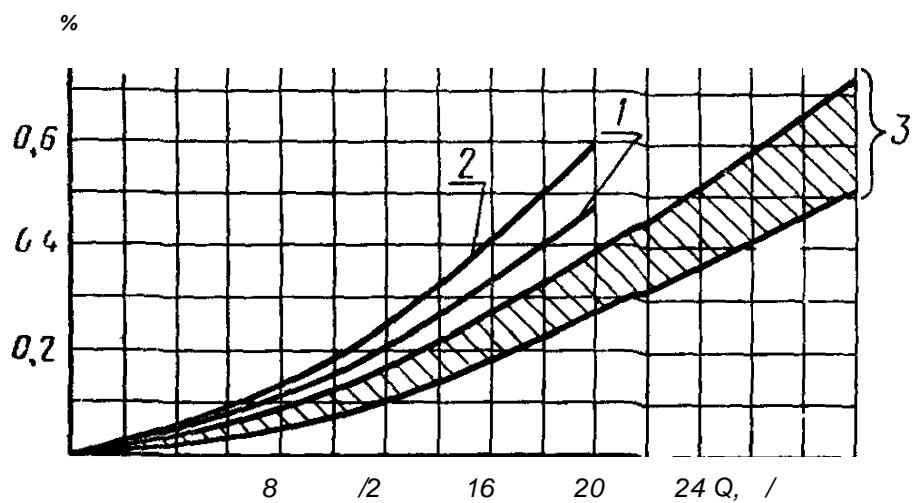
9.1.

? £&

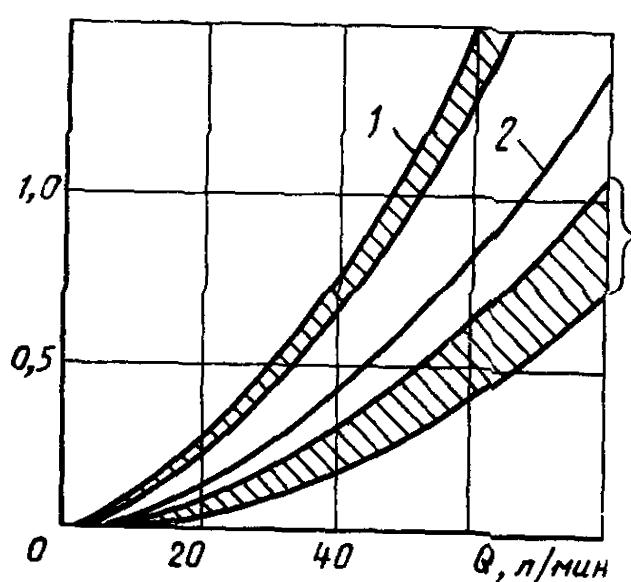
9.2.

, — 12 €
24 0

—6



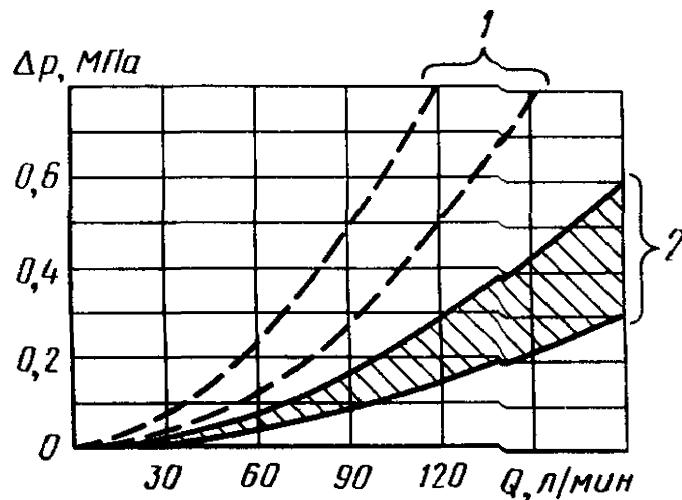
1 — +7 3 — 64 64 ; 2 — ~ * 94;
. 1

Dy —10

1 — ^ 64, 64 , 14, 54, 154, 573, 573 ' 2 —
64, 64 , 14, 54, 154, 3 _ -

. 2

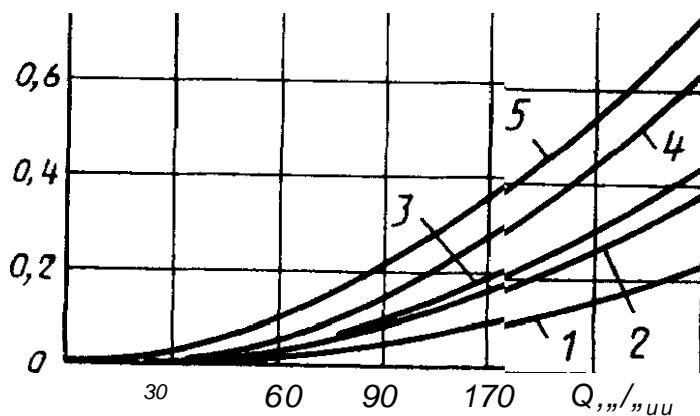
—16 , 44, 64, 64 94



/ — 104? 2 —

. 3

£> =16 44 94

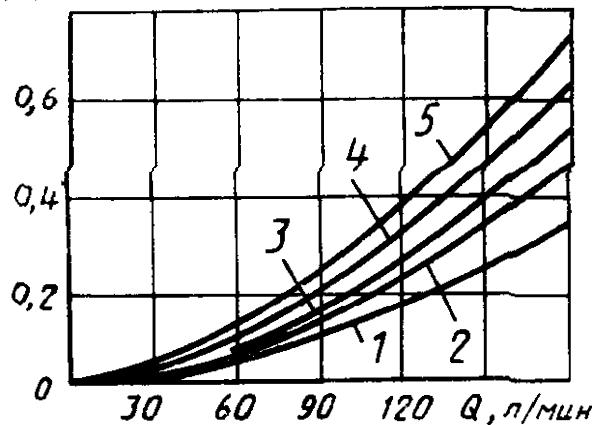


—+ 94; 2 — -* (); 3 — -+ \ 4 — -* ; 5 — -+

. 4

$Z_y = 16$

64 64

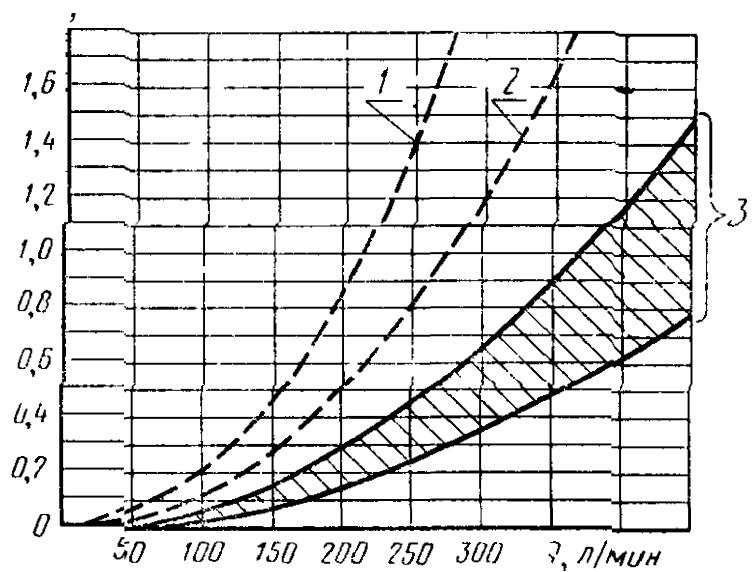
 $\Delta p, \text{МПа}$ 

1 — + ; 2 — ^ ; 3 — . ; 4 — - - - ; 5 — - - - - ;

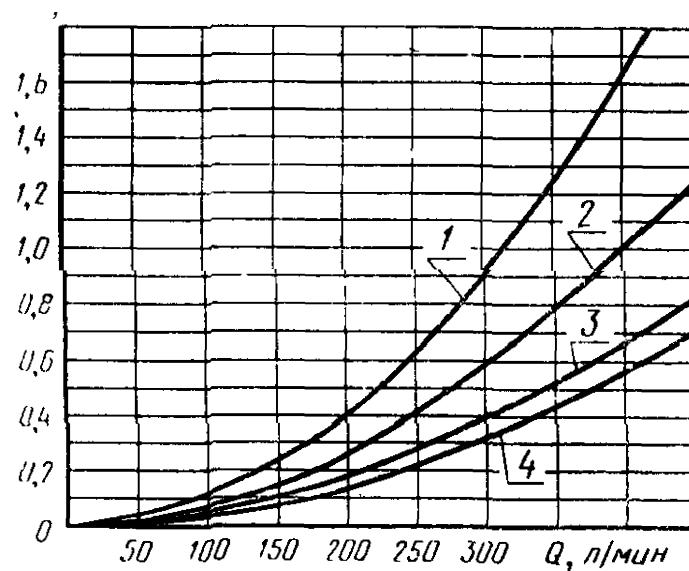
. 5

20

, 44, 64, 64 , 84 , 94

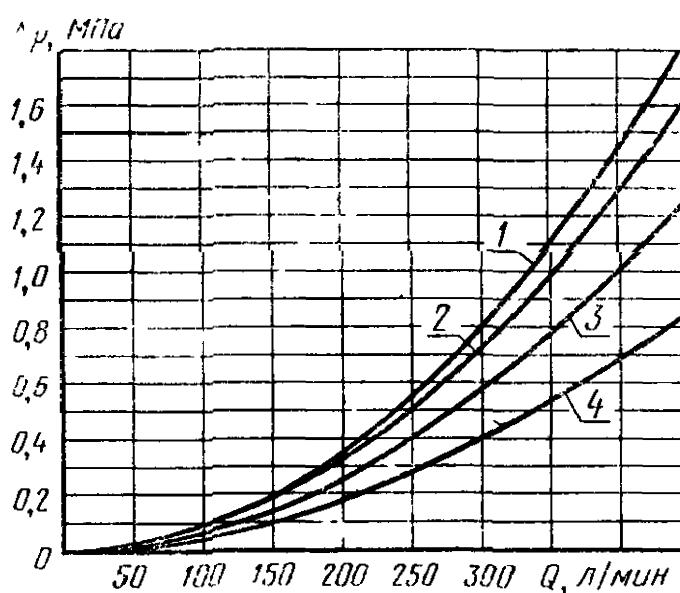
1 — + 1(, 2 — ^
104; 3 —

6

$D = 20$ $44, 84, 94$ 

1 — Δ^* ; 2 — Δ ; 3 — \sim^*
; 4 — \wedge

. 7

 $Dy = 20$ $64, 64$ 

1 — Δ^* ; 2 — Δ ; 3 — \sim^*
; 4 — \wedge

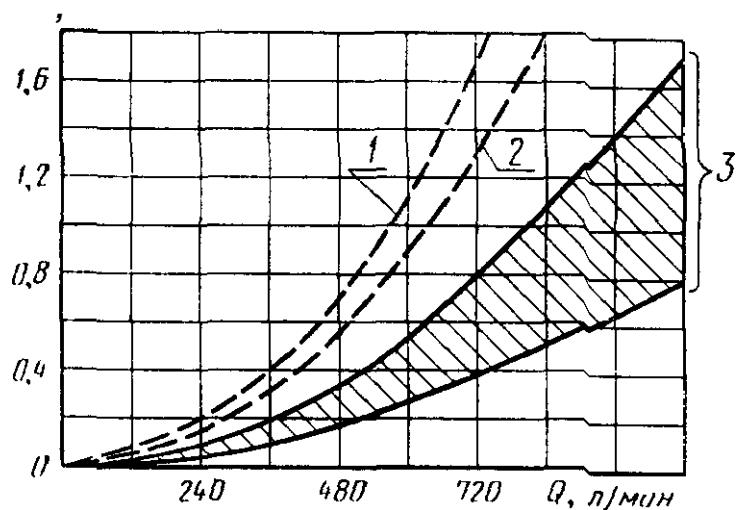
. 8

. 40

24079—81

$\Sigma = 32$

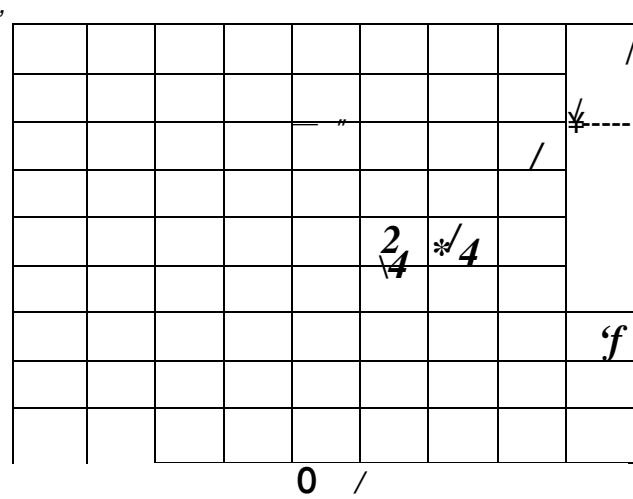
, 44, 64, 64 , 84 , 94



$j \text{---} + 104; 2 \text{---} + ^\wedge$
4; 3 —

. 9

$D_y = 32$ 44, 84 94

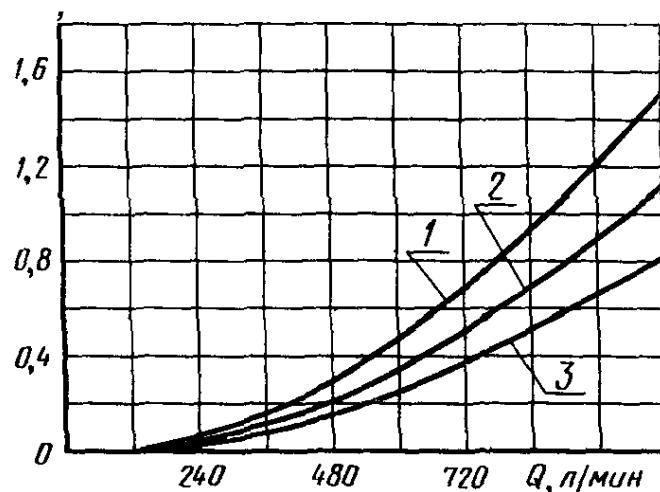


$J \text{---} -^* ; 94; 2 \text{---} + 7 \text{---}$
-» ; 4 — ^ +

. 10

$Z_y = 32$

64 64



J — ^ - * ; 2 — + " ; 3 — - *

. 11

. 1-11.
 30—35 ^/ ().

(, . 2).

	Z)y=6	Dy=10	=6	f> =10
,	12, 24, 48,		36, 110, 220, 380	
,			50 60 (220)	
,	26	43		
,			46	64
,			130	430
, ° , -			55	
° ,			150	
	15000		7200	
14254			IP54	
()			100	
,	2,5	3,5	2,5	3,5
,	25	90	18	47
(), %		40, 60, 100		

(, . 2, 3).

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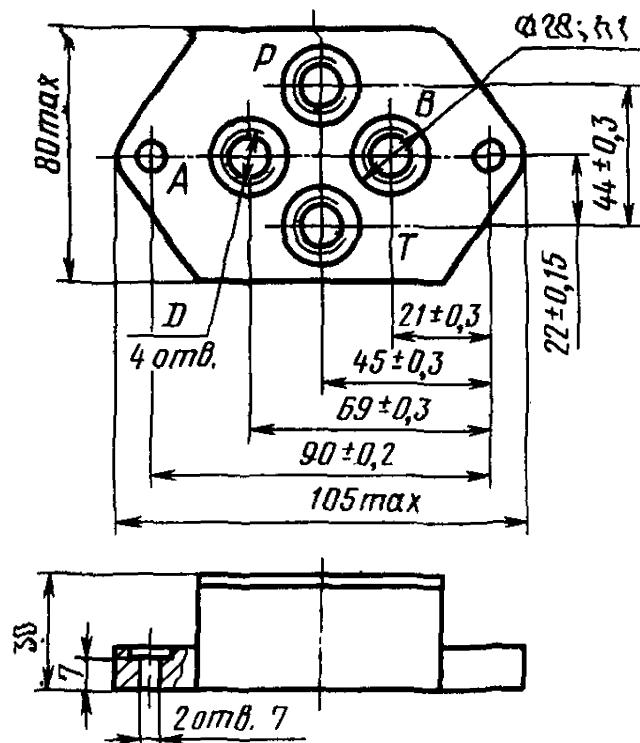
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
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20 24 — , 19 23 — , 18 22 — ,
 , 21 25 — ,
 ; 22, 23, 24, 25 — ,
 ; 14 — .
 (16, 20, 32): 08 — 08 , 10 —
 01,0 , 12 — 0 1,2 .
 ; 15 — (16, 20,
 32); 50 — 0,50 , 70 — (16. — 20,
 ; 16 — (32).
 32): — (16. — 20,
 ; 17 — :
 4, 04 15150.

6.44 ()
6.14	41 4447 0083 00
6.14	41 4441 0285 00
6.14	41 4442 0127 00
6.14	41 4443 0278 08
6.14	41 4444 0036 00
6.14	41 4441 0387 06
BE 6.574	41 4437 0082 07
6.574	41 4431 0089 08
.6.574	41 4432 0049 00
6.574	41 4433 0127 09
6.574	41 4434 0022 01
6.574	41 4431 0140 00
BE 10.44 ()
10.14	41 4447 0087 07
10.14	41 4441 0287 09
10.14	41 4442 0129 06
10.14	41 4443 0282 04
0.14	41 4444 0037 10
10.14	41 4441 0317 09
BE 10.754	41 4437 0073 08
10.574	41 4431 0091 03
BMP 10.574	41 4432 0051 06
10.574	41 4433 0131 02
10.574	41 4434 0023 00
10.574	41 4431 0104 04
X— 16.44 ()
X— 16.14	41 4445 0321 04
X— 16.14	41 4443 0362 05
X— 20.44 ()
X— 20.14	41 4441 0411 01
X— 20.14	41 4445 0243 01
X— 32.14 ()
X— 32.14	41 4443 0363 04
X— 32.14	41 4441 0412 00
— 16.574	41 4445 0244 00
X— 16.574	41 4443 0364 03
X— 32.14	41 4441 0413 10
— 16.574	41 4435 0107 03
X— 16.574	41 4433 0178 10
X— 16.574	41 4431 0151 08
X— 20.574	41 4435 0118 00
X— 20.574	41 4433 0179 09

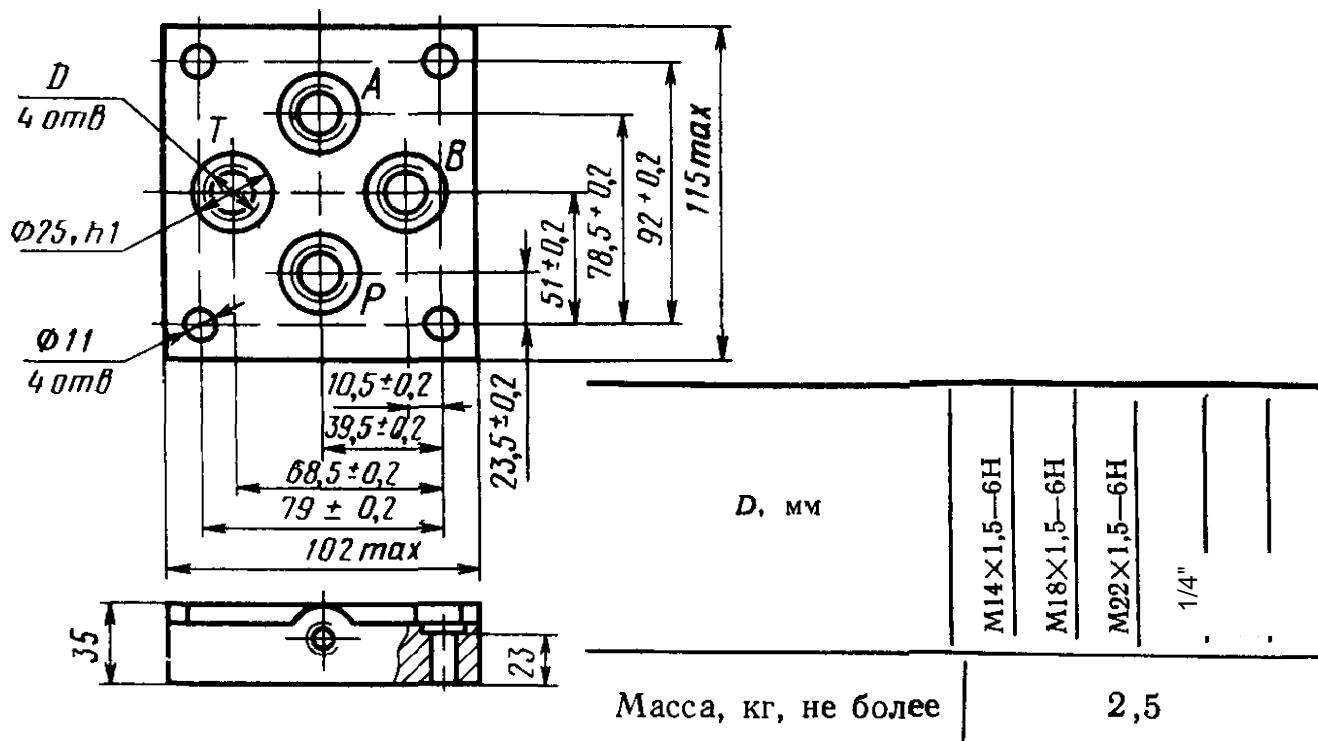
X—	20.574		41 4431 0152 07
X—	32 74		41 4435 0119 10
—	—574		41 4433 0180 05
X—	32.574		41 4431 0153 06
	16.44 ()	41 4445 0239 08
	16 4		41 4443 0231 05
	6.14		41 4441 0286 10
	20.44 ()	41 4445 0232 04
	27.14		41 4443 0365 02
	20.14		41 4441 0414 09
	32.44 ()	41 4445 0235 01
	32.14		41 4443 0366 01
	32 4		41 4441 0415 08
	16.574		41 4435 0120 06
	16.574		41 4433 0130 03
	16.574		41 4431 0090 04
	20.574		41 4435 0105 05
	20.574		41 4433 0181 04
	20.574		41 4431 0154 05
	32 74		41 4435 0106 04
	32.574		41 4433 0182 03
	32.574		41 4431 0155 04

8 if*

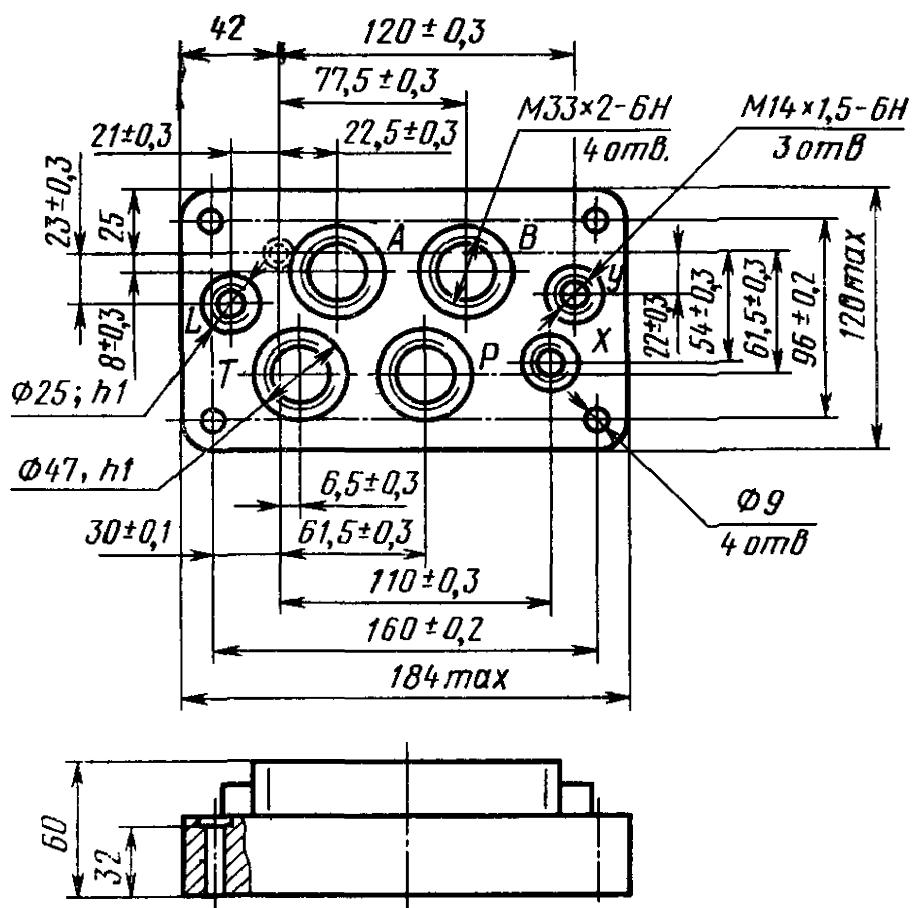
*D,* , ,

~ 114 1,5—

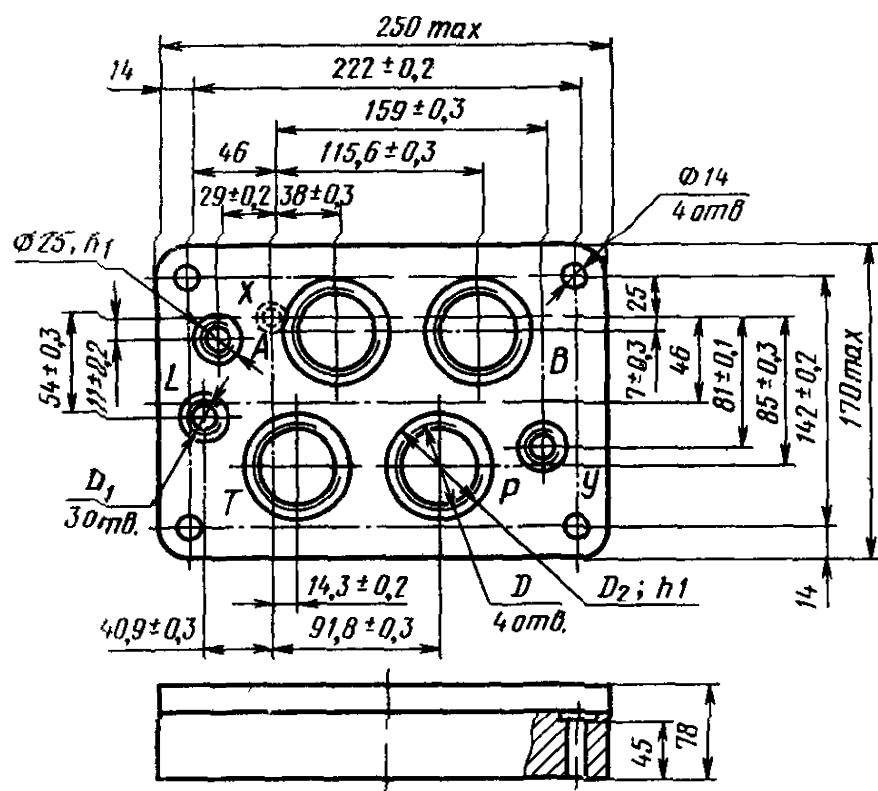
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$D_v = 10$ 

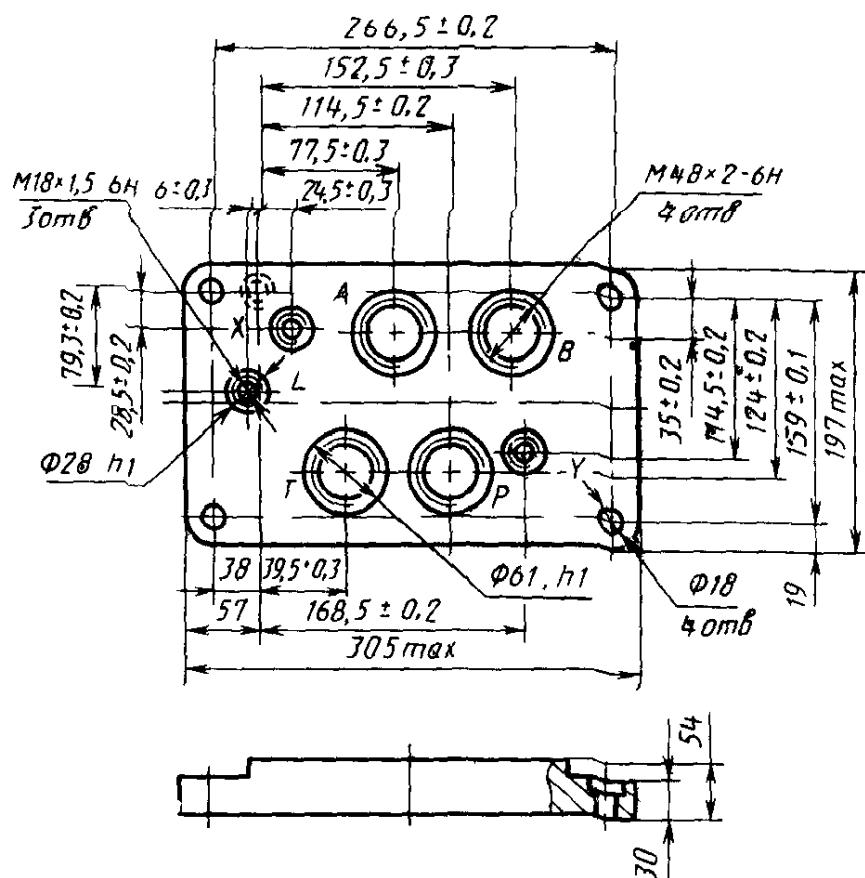
(, . 8).

 $D_y = 16$ 

, 3

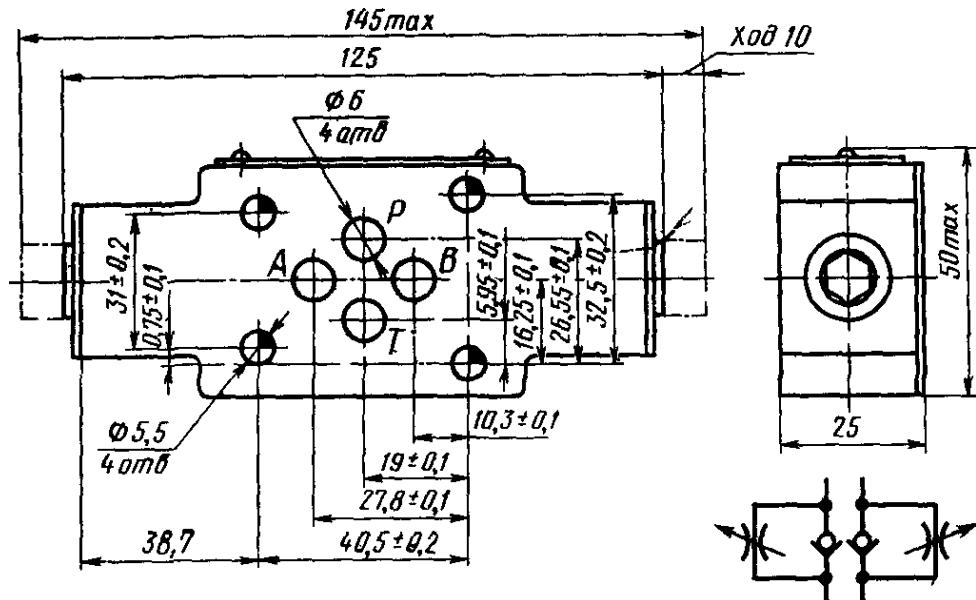
$D = 20$ 

D	D_t	$D,$, , \$
42 2—6	MI 4 XI,5—6	56	
48 2-6	MI 4X1,5—6	61	19

$D = 32$ 

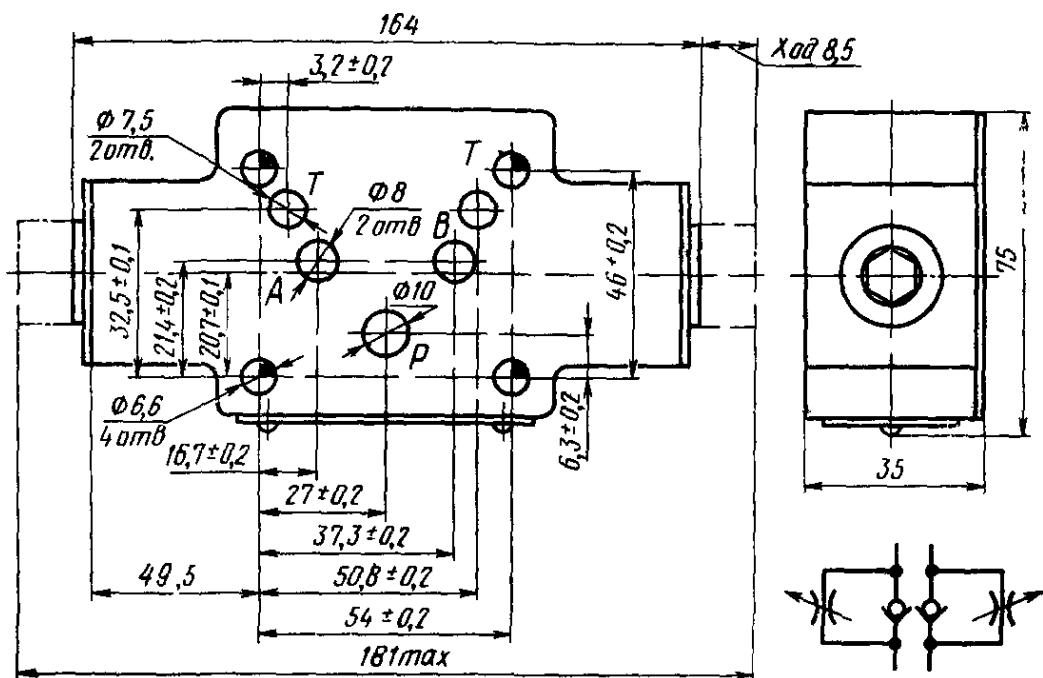
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$D_y = 16$ 

0,8

.1

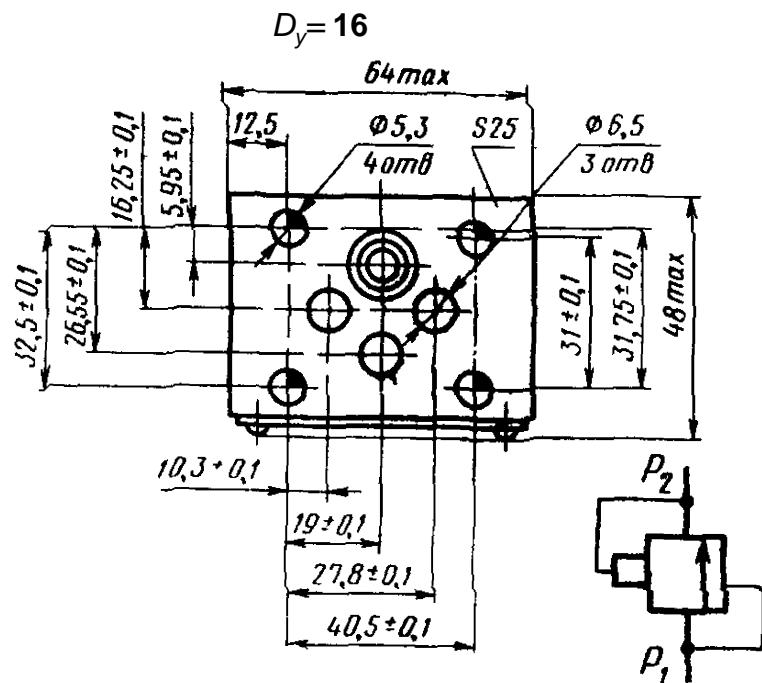
 $D = 20 \quad 32$ 

2,2

.2

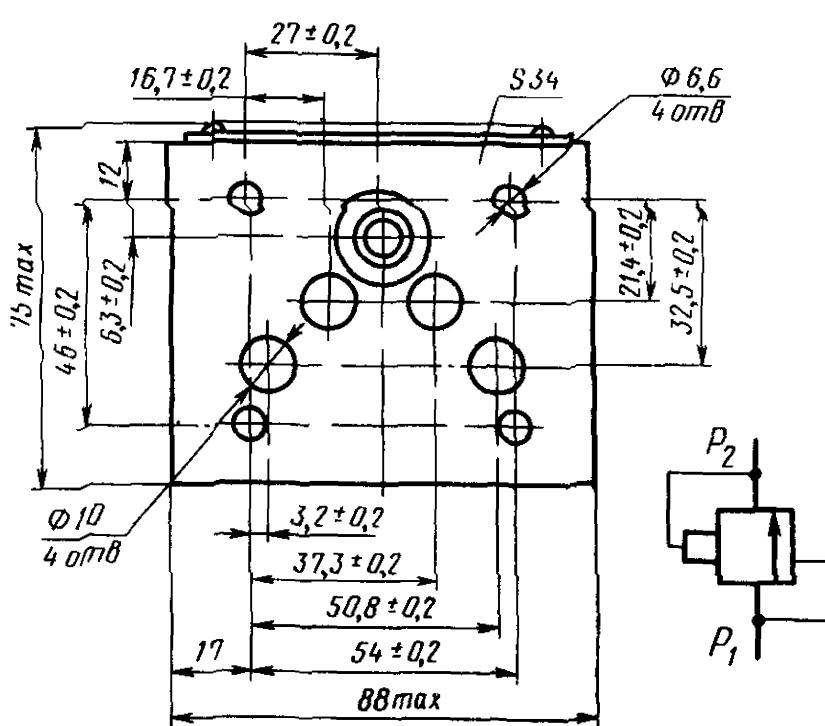
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— 20 32



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2, 3)

			()			
			-	-	I^*	I^*	Dy_t^*
			,	,			
			,		6	10	16
						20	32
			20				
			-	-	0,0052	0,0073	
			-	-	0,0064	0,0095	
			-	-	0,0052	0,0069	
			-	-	0,0064	0,0066	
			-	-			
			32			0,0020	0, 025
			20	0,0030	0,0053		0,0031
			32	0,0050	0,0033		
			20	0,0088	0,0057		
			32	0,0054	0,0036		
			-	-	0,0072	0,0053	
			20		0,0059		
			-	-	0,0080	0,0057	
			20		0,0070		
			32	0,0056	0,0062	0,0029	0,0032
			-			0,0018	0,0050
			20	0,0056	0,0060	0,0020	0,0031
			-	20	0,0056	0,0059	

		/ « / , D_f , '				
		6	10	16	20	22
-	-	—	—	—	—	—
-	20	—	—	0,0034	0,0041	0,0050
-	32	—	—	0,0021	0,0029	0,0031
-	20	—	—	0,0037	0,0052	0,0054
-	32	—	—	0,0023	0,0033	0,0034
-	20	—	—	0,0034	0,0045	0,0050
-	32	—	—	0,0021	0,0028	0,0031
-	20	—	—	0,0037	0,0051	0,0053
-	32	—	—	0,0023	0,0032	0,0033

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<i>ia</i> ,		,	
2.781—68	1,3	15841—88	7.3
9.032—74	2.6	16517—82	2.1
12.2.040—79	3	16536—90	73
12.2.086—83	3	16962.1—89	2.9
2991 —85	7.3	16962.2—90	2.9
9833—73	4	17216—71	8.3
14254—80	2	17411—81	2.1
15108—80	7	20245—74	5.1, 6.1, 6.2
15150—69	3	22976—78	5.1
15151—69	2.3		

7. (1991 .)
 1982 .,
 1985 .,
 1988 . (8—82, 11—85, 12—88).

8. 1988 .
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