



**3325—85**

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3325—85\*

## **Rolling bearings** Tolerance margins and technical requirements for shaft and housing seatings Fits

**3325—55**

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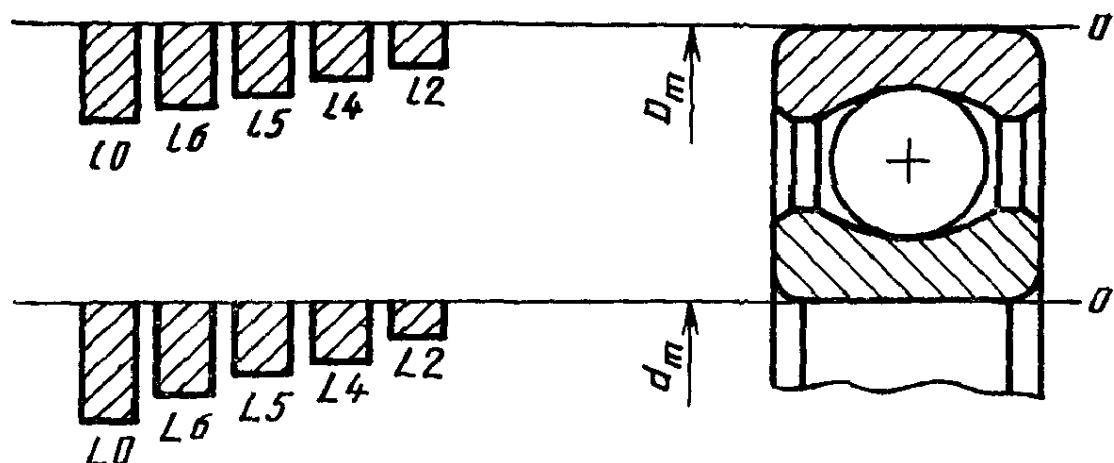
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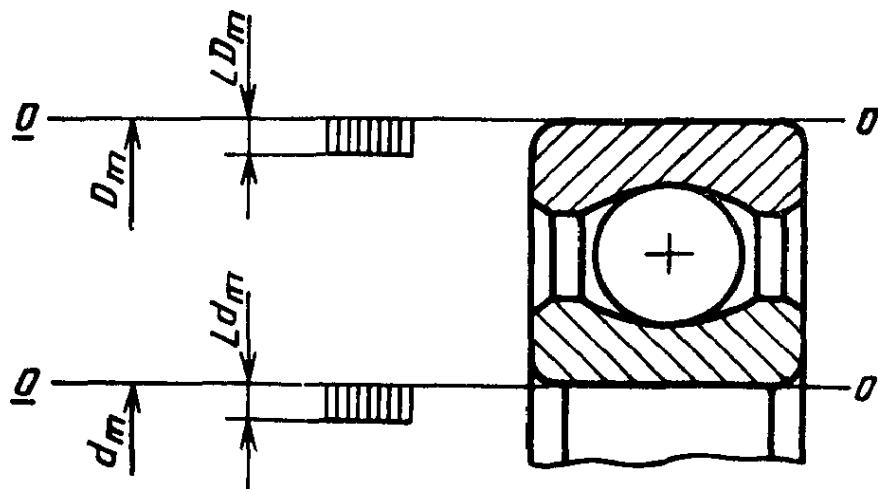
1.1.

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Ldm, LO, L6, L5, L4, L2,

Ld<sub>m</sub> —LO, L6, L5, L4, L2 —  $d_m$ , 6, 5, 4, 2 — 520—71;  
L —

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$ID_m$ , 10, 16, 15, /4, 12 —

$D_m$  —

$/D_m$  —

/0; /6, /5, /4, 12 —

$I$  —

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25346—82, 25347—82

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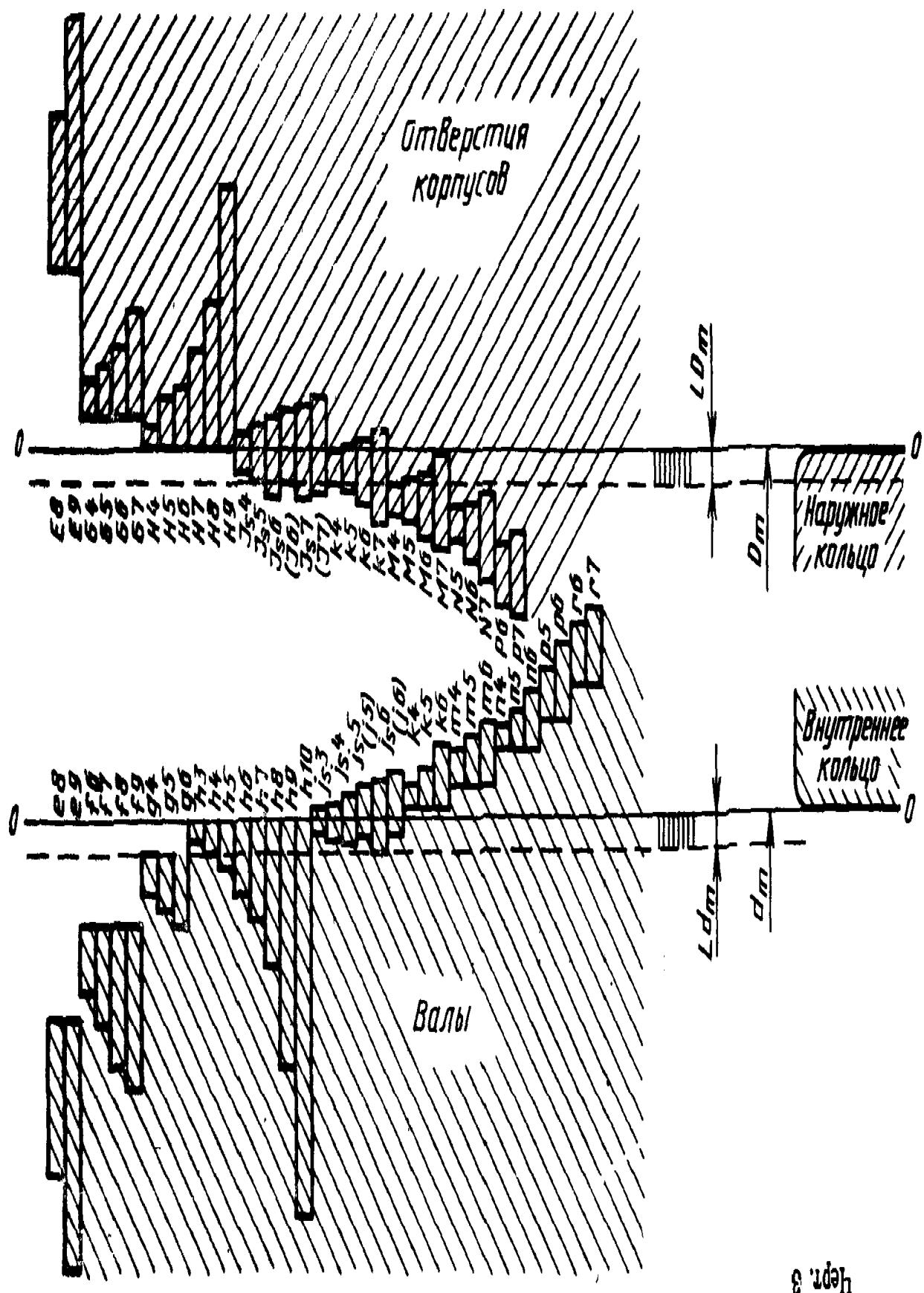
1.6.

Квалитеты	Поля допусков для основных отклонений																		
	e	f	g	h	$J_s$	j	k	m	n	p	r	E	G	H	$J_s$	J	K	M	N
для вала								для отверстия корпуса											
3			$h3$	$J_s3$															
4		$g4$	$h4$	$j_s4$		$k4$	$m4$	$n4$				$G4$	$H4$	$J_s4$		$K4$	$M4$		
5		$g5$	$h5$	$j_s5$	$(j5)$	$k5$	$m5$	$n5$	$p5$			$G5$	$H5$	$J_s5$		$K5$	$M5$	$N5$	
6	$f6$	$g6$	$h6$	$j_s6$	$(j6)$	$k6$	$m6$	$n6$	$p6$	$r6$		$G6$	$H6$	$J_s6$	$(J6)$	$K6$	$M6$	$N6$	$P6$
7	$f7$		$h7$						$r7$			$G7$	$H7$	$J_s7$	$(J7)$	$K7$	$M7$	$N7$	$P7$
8	$e8$	$f8$	$h8$							$E8$		$H8$							
9	$(e9)$	$f9$	$h9$							$(E9)$		$(H9)$							
10				$(h10)$															

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2. $h9$   $h10$ 

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520—89		!		h	is	J	k	m	n	p	
		(£) m i m i m i m i mi						m i m i m i			p6
	L0 8	L0/f7 L0/f8 L0/I9		L0 h7 !							
		L6 f6	m i m i m i m i m i m i								L6 P6
		m i		L6 7							
		L6 fS									
4			m lif-l	mi	(¥) m i m i m i						
			L4 g5	L4 h5	L4 js5	(£) L4 k5	L4 m5	n5			
2			L2 h3	L2 js3							
		1 £ m i m i				m i m i m i					

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		G		J <sub>s</sub>	3		M	N	P
L0		[G7 1 1/0 J	L / 1	[ V ] L /0 J	(S7 1 1 16 /	7 1 L io J	7 ] 1/0 J	N7 • i .	[-1 10 J
L0 7	8/		8//0						
	( 9//0)			( 9//0)					
L6		5L L 16	\ L /6 J	L /6 J	\ i6 )	f 1 L 16 J	M7 ] L /6 J	[ J	[ S-1 16 J
L6 7	8 16		8 /6						
			f <sup>H91</sup> V 16 )						
		1 6 1 1/5 J	I L /5 J	f J <sub>s</sub> 6 ] L /5 J	( <sup>j6</sup> ) ( 15 J	fK6 ] 1 /5 J	6 I 1 /5 J	6 I /15 J	P6 /5
		06 1 L 14 J	L 61 14 J	f J <sub>s</sub> 6 1 L 14 J	1 <sup>j6</sup> ) 14 J	6 I L 14 J	61 L 14 J	f/4 J	P6 /4
		G4 12	4 /2	J <sub>s</sub> 4 U		K4 12	M4 12		
		5 I L 12 J	5 ] L 12 J	85 1 L J		[K5 I I 12 1	51 L 12 J	N5.1 1° J	

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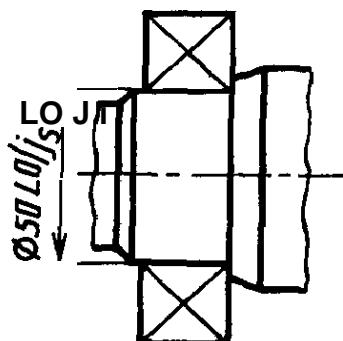
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25347—82;j<sub>s</sub>6—050LO/j<sub>s</sub>6 ( 050 L0—j<sub>s</sub>6, 05 4- ),

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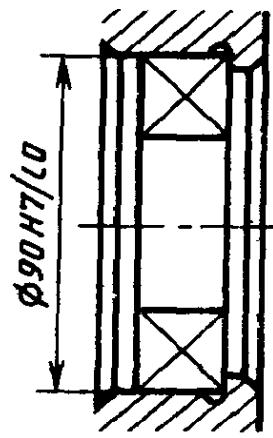
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—09 7/ ( 09 7—/0, 090 ).

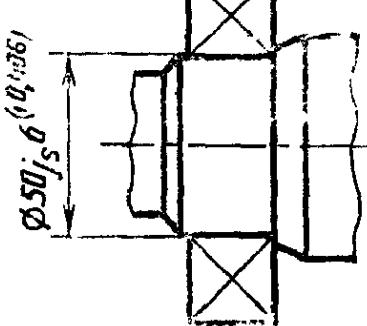
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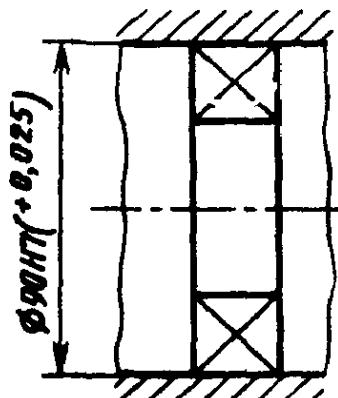
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Черт. 5



Черт. 6



Черт. 7

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 $Ra$   $Rz$ 

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		80	80 500	500	2500
		$Ra$		$Rz$	
	0' 6 5 4 2	1,25 0,63 0,32 0,16	2,50 1,25 0,63 0,32	(5,0) 2,5	20,0
	0 6, 5 4 2	1,25 0,63 0,32	2,50 1,25 0,63	(5,0) 2,5	20.0
	0 6, 5 4 2	2,50 1,25 0,63	2,50 2,50 0,63	(5,0) (5,0)	20,0 20,0*

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 $Ra$ 

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 $Rz$ 

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$F_r$

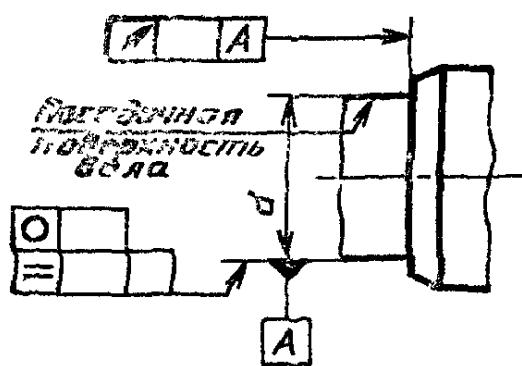
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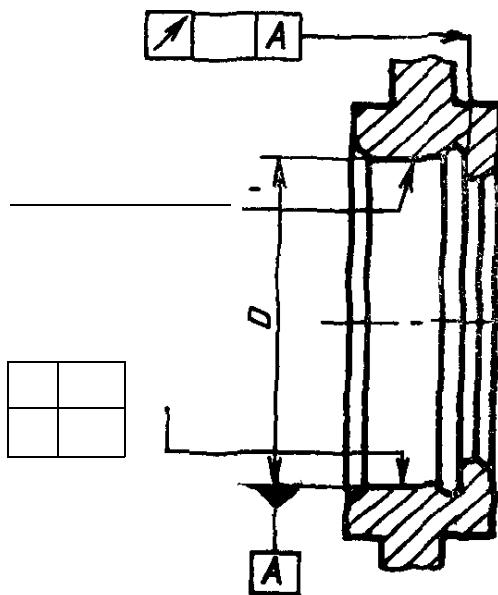
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Черт. 8



Черт. 9

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<i>D, d</i>			

0,6 2,5 1,50,70,4 1,5 0,70,4

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3	6	2,00 80,5	2,0 ,5	1,61,0	1,61,0 3 011.310.61 3.011	30,6 6 2,6	1,2 6 2.61,2
6	10	2,51,00,5	2,5 1,00,5	2 01,0	2,01,0 4.0 1,50,8 4,0 1,50,8	8 3,0 1,6 8 3,01,6	
10	16	2,01,310.61 3.01	1,30,6	6 2,61,2	2,61,2 4,52,01,0 4,52,01,0 9	4,0 2,0 9 4,02,0	
18	30	3,51,50,8	3,5 50,8	3,01,6	3,01,6 5,02,0 1,0 5,02,0 1	4,0 2,010 4,02,0	
30	50	4,02,01,0	4,0 2,01,0	4,02,0	4,02,0 6,02,51,4 6,02,51,412 5,0 2,812 5,02,8		
		5,02,01,0	5,0 2,01,0 10	4,02,0	4,02,0 7,53,01,6 7,53,01,615	6,0 3,215	6,03,2
80	120	6,02,51,2	6,0 2,51,2 12	5,02,4 12	5,02,4 9,03,52,0 9,03,52,0 18	7,0 4	7,04,0
«	180	6,03,0 1,5 6,0	3,01,512	6,03,0 12	6,03,010,04,02,21(1,04,02,221)	8,0 4,420	

D, d	( )																								
	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	0 и 6 5 и 4	2	
Св 180 до 250	7,0	3,5	1,7	7,0	3,5	1,7	14	7,0	3,4	14	7,0	3,4	11,5	5,0	2,5	11,5	5,0	2,5	23	10,0	5,0	23	10,0	5,0	
Св. 250 до 315	8,0	4,0	—	8,0	4,0	—	16	8,0	—	16	8,0	—	13,0	5,3	3,0	13,0	5,3	3,0	26	10,6	6,0	26	10,6	6,0	
Св. 315 до 400	9,0	4,0	—	9,0	4,0	—	18	8,0	—	18	8,0	—	14,0	6,0	4,0	14,0	6,0	4,0	28	12,0	8,0	28	12,0	8,0	
Св. 400 до 500	10,0	—	—	10,0	—	—	20	—	—	20	—	—	16,0	—	—	16,0	—	—	32	—	—	32	—	—	
Св. 500 до 630	11,0	—	—	11,0	—	—	22	—	—	22	—	—	17,5	—	—	17,5	—	—	35	—	—	35	—	—	
Св. 630 до 800	12,0	—	—	12,0	—	—	24	—	—	24	—	—	20,0	—	—	20,0	—	—	40	—	—	40	—	—	
Св. 800 до 1000	14,0	—	—	14,0	—	—	28	—	—	28	—	—	22,5	—	—	22,5	—	—	45	—	—	45	—	—	
Св 1000 до 1250	16,0	—	—	16,0	—	—	32	—	—	32	—	—	26,0	—	—	26,0	—	—	52	—	—	52	—	—	
Св. 1250 до 1600	19,0	—	—	19,0	—	—	38	—	—	38	—	—	31,0	—	—	31,0	—	—	62	—	—	62	—	—	
Св 1600 до 2000	23,0	—	—	23,0	—	—	46	—	—	46	—	—	37,5	—	—	37,5	—	—	75	—	—	75	—	—	

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<i>D,</i> <i>d</i>					<b>HIH</b>			

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2000	2500	27,0	-	27,0	-	54	-	-	51	-	-	44,0	-	-	44,0	-
2500	31 0	-	-	-	-	-	-	-	-	-	-	52,0	-	-	52,0	-

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.10 18		lh	5	3,0	2,0
.18 30	21	13	6	4,0	2,5
.30 50	25	16	7	4,0	2,5
.50 80	30	[9	8	5,0	3,0
.80 120	35	22	10	6,0	4,0
.120 180	40	26	12	8,0	5,0
.180 250	46	29	14	10,0	7,0
.250 315	52	32	16	—	—
315 400	57	36	18	—	—
.400 500	63	40	—	—	—
.500 630	70	44	—	—	—
.630 800	80	50	—	—	—
.800	90	56	—	—	—
.1250	105	66	—	—	—
.1250 1600	125	78	—	—	—
.1600 2000	150	92	—	—	—
2000 2500	375		—	—	—

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	0	6	8				
3 6	18	J2	5	4	2,5		
.6 10	22	15	6	4	2,5		
.10 18	27	18	8	5	3,0		
18 30	33	21	9	6	4,0		
.30 50	39	25	11	7	4,0		
.50 80	46	30	13	8	5,0		
.80 120	54	35	15	10	6,0		
.120 180	63	40	18	12	8,0		
180 250	72	46	20	14	10,0		
.260 315	81	52	23	16	12,0		
.315 400	89	57	26	30	13,0		
.A GO 500	97	63	27	—			
.500 630	110	70	30	—	—		
630 800'	125	80	35	—	—		
.800 1000	140	90	—	—	—		
.J000 1250	165	106	—	—	—		
.1250 1600	196	126	—	—	—		
.1600 2000	230	(50	—	—	—		
.2000 2500	280	175	—	—	—		
.2500 3150	330	210	—	—	—		

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18 30	21	13	9	6	4	13	9	6	2,5	1,5
30 50	25	16	11	7	4	16	11	7	2,5	1,5
50 80	30	19	13	8	5	19	13	8	3,0	2,0
80 120	35	22	15	10	6	22	15	10	4,0	2,5
120 180	40	25	18	12	8	25	18	12	5°	3,0
180 250	46	29	20	14	10	29	20	14	7,0	3,5
250 315	52	32	23	23	-	82	23	16	8,0	-
315 400	57	36	25	25	-	36	25	18	9,0	-
400 500	63	40	27	27	-	40	27	20	10,0	-
500 630	70	44	1	-		44	30			-
630 800'	80		—	—	—	50	-	-	-	-
800 1005	00		-	-	—	56	-			-
1000 1250	105	—	-	-	-	66	-	-	-	-
1250 160	125		-		-	78		-	-	-

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L5 i»5	L0 js6	L5 h5	L0 h6		L0 ft	L0 ft		J,6 15	J,7 10	H6 15	H7 10	H8 <b>iL</b>	G7 <b>JL</b>	
js5	L6 j.6	L4 h5	LG h6		L6 8	L6 8		J,6 14	J,7 c	H6 14	H7 i	W <b>iL</b>	.16	
12 js4		L2 h4						U 12		H5		HW		
L5 n5	JJ) n5	i m5	U) k5	L5 k6	L0 iL	L5 iL	L0 i.e	N6 15	N7 10	MG 15	M7	K6 <b>iF</b>	K7 II)	P7
U 5	LG n6	L4 L6	L6 L4	L6 k6	L6 it	L4 it	L6 j.6	N6 14	N7 16	M6 14	M J	K6 1G	K7 1	P7
L2 4		L2 m4		ia 1(4)		M		12		M5 e		K5 12		
L5 jf	L0 i							« 15	S3					
js5	L6 j.6							J,5 14	W 1G					
U								W 12						

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L0/n6	L0/m6	L0/k6	L0/j»6	N7/J0	M7/W	K7//0	J»7//0	P7/J0
L6/n6	L6/m6	L6/k6	L6/j <sub>s</sub> 6	N7/Z6	M7//6	K7//6	J.7//6	P7//6

L0/j<sub>s</sub>6  
L6/j\*6

J\*7//0  
Jsi7//6

LQ/j<sub>a</sub>6; L0/h6;  
L6/j.6; L6/h6

7/ ; 7/ ; H7//0; M7//6;  
K7//6; H7//6

LC/h6; L0/g6; L0/f6;  
L6/h S; L6/g6; L6/f6

H7//0; H7//6

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$\frac{D_k}{D}$  >1,25 — ,

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*db* —  
*D* —  
*D* —

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8		8' 12' 16'
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= 12°		6'
= 26°		5'
= 36°		4'
-		4'
=45°—60°		
	= 9^	2'
	:	
		2' 6'
	:	
	-	2' V
		8'
		1'
	:	
		1" 4'
5720—75		4°
24954—31		3°
5721—75		2°
9942—80		3°

Sxw"70/m&amp; ? ^

2534-32

520—71

Поля допусков и посадки системы ОСТ: ОСТ 1011, ОСТ 1012, ОСТ 1021, ОСТ 1022, ОСТ 1023, ОСТ 1024, ОСТ 1027, ГОСТ 3325—55		L	L <sub>3</sub>	—	X	D	C	C <sub>2a</sub>
Характер посадки	вал	L <sub>п</sub>	L <sub>3п</sub>	—	X <sub>п</sub>	D <sub>п</sub>	C <sub>п</sub>	—
	корпус	легкогоход- вая класса 2	легкогоход- вая класса 3		ходовая класса 2	движения класса 2	сколь- класса 2	сколь- класса 2а
		с зазорами				переходные (с зазором)		
		для						
Поля допусков по ГОСТ: ГОСТ 25346—82, ГОСТ 25347—82 и соответствующие посадки		e8	e9	f6	f7	f8	g6	h6
		$\frac{L_0}{e8}$	$\frac{L_0}{e9}$	$\frac{L_0}{f6}$	$\frac{L_0}{f7}$	$\frac{L_0}{f8}$	$\frac{L_0}{g6}$	$\frac{L_0}{h6}$
				$\frac{L_6}{f6}$	$\frac{L_6}{f7}$	$\frac{L_6}{f8}$	$\frac{L_6}{g6}$	$\frac{L_6}{h6}$
								$\frac{L_6}{h7}$
		для отверстия						
		E8	E9				G7	H7
		$\frac{E8}{E8}$	$\frac{E9}{E9}$				$\frac{G7}{G7}$	$\frac{H7}{H7}$
							$\frac{H8}{H8}$	$\frac{H8}{H8}$
							$\frac{H8}{H8}$	$\frac{H8}{H8}$

25347—82

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3—	—	4= *		1			7	
				"			7	
,	C-J <sup>1</sup> <sub>3</sub>	<sup>1</sup> <sub>rf</sub> eg	— CJ	5 <sup>‘</sup> <sub>—</sub> £	CJ ; >1	1 U & \$ <sub>—</sub> CJ 0	X <sup>‘</sup> <sub>&gt;</sub>	
,	)							

	h8	h9	hUO		js€	(j6)	k6	m6	n6		r6	r7
L0/h8	L0/h9				L0	L0	L0	_L0	10	L0	L0	L0
					js'6	06)	k6	m6	n6	P6	r6	r7
L6/h8	L6/h9				L6_	L6	L6	L6_	L6	L6_	L6	L6
					js6	06)	k6	m6	n6	p6	r6	r7

	H9				J <sub>s</sub> 7	(J7)	K7		N7	P7	
9 10					JL7	(J7) /0	K7 /0	M7 Kb	N7 10	P7 to	
9 /6					J»7 /6	(J7) /6	K7 /6	M7^ /6	N7 /6	P7 /6	

520—71	5					
1011, 1012, 1022, 1024, 3325—55			,			
1021, 1023, 1027,				Tin	*\	
	—	—	—	=	—	
				—		

g5	h6	Js5	(J'&)	K5	m5	n5	
L5 g5	L5 h>5	L5_ js5	L5 (j5)	L5 K5	L5_ m5	L5_ n 5	
45 g5	L4 hS	L4_ j <sub>s</sub> 5	L4 (j5)	L4 K5	L4 rn5	L4_ n5	

25345-82,  
25347-82

G6	H6	J <sub>s</sub> 6	(J6)	K6	M6	m	
G6 /5	H6 /5	J <sub>s</sub> 6 15	(J6) 15	K6 /5	/5	m /5	
G6 14	H6 14	J <sub>s</sub> 6	(J6) 14	K6	M6 /4	N6 14	

1.

2-

2.

4		2									
		1		Cx		i, ni	Hi	Tx			
		-		-		-		-			
- 1						j					
	5		g4	h3	h4	js^	js4	k4	4	4	
L5		L2		L2		L2		L2		L2	
5		h4		h3		h4		Js3		Js4	
L4								k4		4	
EI											

	6	G4	G5	4	5	Js4	JsS	K5	M5	N5
	6 /5	G4 /2	G5 /2	4 /2	5 12	Js4 J2	Js5 12	K5 12	MS 12	N5 12

, [+] [-])

1 ®

i		, rf <sub>m</sub>		, 16																
				X	I	X &	s	X	X	1	i	X	X	X	t	X				
1»	180	0	'25	+52	+27	+40	+15	+28	+3	+12,5	-12,5	+14	-	0	-25	-14	-39	-43	-68	
.	180	250	-	-30	+60	+31	+40	+17	+33	4	+14,5	-14,5	+16	-13	0	-29	-15	-44	-50	-79
.	250	315	0	-33	+66	+34	+52	+20	+36	+4	+16,9	-1+0	+16	'16	0	-32	-17	-49	-56	-88
.	315	400	0	-40	173	+37	+57	+21	+40	+4	+18,0	-18,0	+18	'18	0	-36	-18	-54	-62	-98
.	400	500	0	-45	480	+49	+63	+23	+45	5	+20,0	-20,0	+20	0	-40	-20	-60	-68	-108	
5 0	630	0	'50	+88	+44	+70	+26	+44	0	+32,0	-22,0			0	-44	-22	'66	-76	-120	
.	630	800	0	-75	+100	+50	+80	-30	+50	0	4-25,0	-25,0		0	-	-24	-74	-80	-130	
.	800	1000	0	-100	+112	+56	+90	+34	+56	0	+28,9	-28,0		0	-56	26	-82	-86	-142	
		0	-125	+132	+66	+106	+40	+66	0	+33,0	-33,0			0	-66	-28	-94	-98	-164	
,	1250	1600	0	'160	1156	+78	+126	+48	78	0	+39,0	-39,0		0	-78	3^	-108	'	J8	
.	1600	2000	0	'200	+184	+92	+150	+58	+92	0	+46,0	-46,0		0	-92	-32	-124	-120	-212	
,	2000		0	-250	+220	+110	+178	+68	+110	0	+55,0	-55,0		0	-	"34	-144	-130	-240	

				(+) (−) ,															
				L0/m6		L0/k6		L0/j <sub>s</sub> 6		‘6		L0/h6		Wgi					
i		, d <sub>m</sub>		/															
		0	s x	0 x	§ x	0 x	% 2	0	§ p	0	t 1 0	:	s x	“ x 31	£ 0	0 31	£ 31	“ x 31	£ 0
0,6	3	0	-8	+18	+1	+16	+2	+14	0	+11,0	-3,0	+12	-2	+8	-6	+5	-8	+2	-12
.3	6	0	-8	+24	+8	+20	+4	+17	+1	+12,0	-4,0	+14	-2	+8	-8	+4	-12	-2	-18
.6	10	0	-8	+27	10	+23	+6	+18	+1	(12,5	-4,5	+15	-2	+8	-9	+3	-14	-5	-22
.10	18	0	-8	+31	+12	+26	+7	+20	+1	+13,5	-5,5	+16	-3	+8	-	+2	-17	-8	-27
.16	30	0	-10	+38	+15	+31	+8	+25	+2	+16,5	-6,5	+19	-4	+10	-13	+3	-20	-10	-33
,30	50	0	-12	+15	+17	+37	+9	+30	+2	+20,0	-8,0	+23	-5	+12	-16	+3	-25	-13	-41
.50	80	0	-15	+54	+20	+45	+11	+36	+2	+24,5	-9,5	+27	-7	+15	-19	+5	-29	-15	-49
.®)	120	0	-20	+55	+23	+55	+13	+45	+3	+31,0	-11,0	+33	-9	+20	-22	+8	-34	-16	-58
.12»	180	0	-25	+77	+27	+55	+15	+53	+3	+37,5	-12,5	+39	-11	+25	-25	+	-39	-18	-68
.180	250	0	-30	+90	+31	+76	+17	+53		+44,5	-14,5	+46	-13	+30	-29	+15	-44	-20	-79
.250	315	0	-35	+101	+34	+37	+20	+71	+4	+61,0	-16,0	+51		+35	-32	+18	-49	-21	-88

i		.		(+), (-), ,															
				10		m		l,		l06		10/116		l06					
x	x	x	x	0	0	x	0	4	x	2	0	x	*	1	4	*	0	x	
, 315	400	0	-40	+113	+37	+97	+21	+80	+4	4 58,0	-18,0	+58	-18	+40	-36	22	-54	-22	-98
, 400	500	0	-45	+125	+40	+108	+23	+90	+5	+65,0	-20,0	+65	-20	+45	-40	+25	-60	-23	-108
. 500	«00	0	-50	+138	+44	+120	+26	+94	0	+72,0	-22,0			+50	-44	+28	-66	-26	-120
. (90		0	-75	+175	+50	+155	+30	+125	0	+100,0	-25,0			+75	-50	+51	-74	-5	-130
. 800	1000	0	-100	+212	+56	+190	+34	+157	0	+128,0	-28,0			+100	-56	+74	-82	+14	-142
.» 1260		0	-125	+257	66	+231	+40	+191	0	+158,0	-33,0			+125	-66	+97	-94	427	-164
. 1250	1600	0	-160	4316	178	—	+48	+231	0	+199,0	-39,0			+160	-78	+133	-108	+50	-188
. 1600	2000	0	-200	+384	+92	+350	+51	+292	0	+246,1	-46,0			+2»	-92	+168	-124	+80	-212
, 2500		0	-25	4-450	+11	4-428	+68	+360	0	+305,0	-55,0			+250	-	+216	-144	+120	-240

		Chord Progression																			
		I		IV		V		VI		VII		I		IV		V		VI		VII	
		C		G		D		A		E		B		C		G		D		A	
		*		7		N7		7		7		V		J7		7		G7			
		£>,	*																		
		4)	*	X	4)	11	8	X	a	X	X	01	X	1	4)	8	*	X	X	4)	
2,5	3	0	-8	-6	-16	-4	-14		-12	0	-10	+5	-5		-6	+10	0	+12	+2		
,3	6	0	-8	-8	-20	-4	-16	0	-12	+3	-9	+5	-6	+6	"6	+12	0	+16	+4		
.6	10	0	-8	-9	-24	-4	-19	J	-15	+5	-10		-7	+8	-7	+15	0	+20	+5		
,10	13	0	8	-	-29	-5	-23	J	-18	+5	-12	+9	-9	+10	-8	+18	0	+24	+6		
,15	30	0	-9	-14	-35	-7	-28	0	21	+6	-15	+10	-10	+12	-9	+21	0	+28	+7		
,30	50	0	-11	-17	-42	-8	-33	J		+7	-18	+12	-12	+14	-11	+25	0	+34	+9		
,50	80	0	-13	-21	-51	-9	-39		-30	+9	-21	+5	-15	+18	-12	+30	0	+40			
,80	120	0	-15	-24	-59	-10	-45	0	-35		-25	+17	-17	122	-13	+35	0	<b>if</b>	+12		
120	150	0	-18	-28	-68	-12	-52	0	-40	+12	-28	+20	-20	+26	-14	+40	0	+54	+14		
,150	180	0	-25	"28	-68	-12	-52	0	-40	+12	-28	+20	-20	+26	-14	+40	0		+14		

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D, D <sub>fl</sub> )	7	N7	7	7	V	J7	7	07	,		,		,		,			
									X 19	!	f <sup>t</sup> 0	1	*	t X 4)	X 4)	X 4)	X 4)	
. 180 250	0	-30	-33	-79	-14	40	0	-46	4*1?	-33	+23	-23	+30	-16	+46	0	+61	+15
. 250 315	0	-35	-36	-88	-14	46	0	42	+16	-38	+26	-26	+36	-16	+52	0	+59	+17
. 315 «0	0	-40	-41	-98	-16	-73	0	47	+17	-40	+28	-28	+39	-18	+57	0	+75	+18
. 400 500	0	-45	-45	-108	-17	-80	0	43	+18	-45	+31	-31	+43	-20	+63	0	+83	+20
500 630	0	-50	-78	-148	-44	-114	-26	-95	0	-70	+35	-35			+70	0	+92	+22
, 630 800	0	-75	-88	-168	-50	-130	-30	-	0	^80	+40	-40			+80	0	+104	+24
800 1000	0	-100	-100	-190	-56	-146	-34	-124	0	-90	+45	-45			+90	0	+116	+26
. 1250	0	-125	-120	-225	-66	-171	-40	-145	0	-105	+52	-52			+105	0	+133	+28
, 1250 1600	0	-160	-	-265	-78	-203	-48	-173	0	-125	+62	-62			+125	0	+155	+30
. 1000 2000	0	-200	-170	-320	-92	-242	-58	-208	0	-150	+75	-75			+150	0	+182	+32
, 2000 2500	0	-250	-195	-370	-	-285	48	-243	0	-175	+87	-87			+175	0	+209	+34
, 2500 3150	0	-310	-240	-450	-135	-345	-78	-286	0	-210	+105	-105			+210	0	+248	+38

D,	D_	7//0	NP	7//0	7//0	VII»		J7//0		7/		G7//0							
1	X	si	0	i	*	s	1	i	0	i	0	«	X	V	1	s	:		
0	0	X	X	X	X	X		X	X	X	X		X						
2,5	3	0	-8	+16	-2	+14	-4	+12	-6	+10	-8	+5	-13	16	-12	0	-18	-2	-20
3	6	0	-8	+20	0	+16	-4	+12	-8	+9	-11	+6	-14	+6	-14	0	-20	-4	-24
6	10	0	-8	+24	+1	+19	-4	+15	1	+10	-13	+7	-15	+L	-16	0	-23	-5	-28
10	18	0	-8	+29	+3	+23	-3	8	-8	+12	-14	+9	-17	+8	J	-26	-6	-32	
18	30	0	-9	+35	+5	+28	-2	+21	-9	+15	-15	+10	-19	+9	-21	0	-30	-7	
, 30	50	0	-11	+42	+6	+	-3	+25	-11	+18	-18	+12	-23	+11	-25	0	-36	-9	-45
. 50	80	0	-13	+51	+8	+39	-4	+30	-13	4	-22	+15	-28	+12	-31	0		-10	-53
. 80	120	0	-15	+59	+9	+45	f	+35	-15	+25	-25	+1?	-32	+13	-37	0	-50	-12	12
. 120	150	0	-18	+08	+10	+52	-6	+40	-18	+28	-30	+20	-38	+14	-44	0	-58	-14	
, 150	180	0	-25	+68	+3	+52	13	+40	-25	+28	-37	+20	-45	+14	A1	0	-65	-14	-79
. 180	250	0	-30	+79	+3	+60	-16	+46	-30	+33	-43	+23	-53	+16	-60	0	-76	-15	-91

(+) (-), ,

7/0 N7/10 7/0 7/ 1,9 7( 09

D,

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		*	*		2	0	2	0	(9)	i		2	0	<9	£	(9)	9	2	0	2		2
. 250	315	0	-35	+88	+1	+66	-21	+52	-35	+36	-51	+26	-61	+16	-71	0	-87	-17	-104			
. 315	400	0	-40	+98	+1	+73	-24	+57	-40	+40	-57	+28	-68	+18	-79	0	-97	-18	-115			
, 400	600	0	-45	+108	o	+80	-28	+63	-45	+45	-63	+31	-76	+20	-88	0	-108	-20	-128			
. 500	630	0	-50	+148	+28	+114	-6	+96	-24	+70	-50	+35	-85				0	-120	-22	-142		
. 630		0	-75	+18	+13	+130	-25	+110	-45	+80	-75	+40	-115				0	-155	-24	-179		
. 800	1000	0	-	90	0	+146	-44	+124	-66	+90	-100	+45	-145				0	-190	-26	-216		
. 1250		0	-125	+225	-5	+171	-59	+145	-85	+105	-125	+52	-177				J)	-230	-28	2258		
. 1250	1600	0	-160	+265	-20	+203	-82	+173	-112	+125	-160	+62	-222				0	-285	-30	-315		
, 1600		0	-200	+320	-30	+242	-108	(-2(18-142	+150	-200	+75	-275				0	J50	£2	482			
, 2000	2500	0	-250	+370	-55	+285	-140	+243	-182	+175	-250	+87	-337				0	-425	-34	-459		
. 2500	3150	0	-310	+450	-70	+345	-175	+286	-232	+210	-310	+105	-415				0	-520	-38	-558		

J.6 16 6

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&amp;

d<sub>ra</sub>

0,6	3	-7	+4	+8	-2	+6	0+3,0
3	6		64£	+12	+4	+9	+1+4,0
6	10	-7	+1	+15+6	+10	+1	+1,5
			±!	3+12	+18	+7	+12 +1+5,5
? 18	30	-8	+218+15	+21+8	5+2	+6,5	
30	50	~	+33	+17	+25+9	+18	+2
50	80	12	+3!9+20	+30+11	+21		+9,5
			4 5+45	ffff	+35+13+	+3+	
120	180	18	+512+27		+ 15+28	+3	+1+5
		42	+60+31	+46	+174-33	+4+1+5	
260	315	45	+616+34	+52+20	+36	+4+	16,0
315	400	£	+ 3+37	+57+21	+40	+4+	
400	500	•35	+40	+63	+23	<45	+5 4 0
LB 500 10 630		-40+88+44+70	444		0+22,0		

10 X X	10 8 X	X	8 4	X X X	X X	X	X X	X X
-3,0	+4	-2	0	-6	-2	-8	-6	-12
-4,0	+6	-2	0	-8	-4	12	-10	-18
-4,5	+7	-2	0	-9	-5	-14	-13	-22
-5,5	+8	-3	0	-11	-6	-17	-	-27
-6,5	+9		0	-13	d.	-20	-20	-33
-8,0	+	1	0	16		-25	-25	-41
-9,5	+12	-7	Q	-19	-10	49	-30	-49
-11,0	+13	-9	0	-22	-12	-34	-36	-58
4+5	+14	-11	0	-25	-14	-39	-43	-68
4+8	+16	-13	0	-2?	-15	-44	-50	~
-16,0	+16	-16	0	42	-17	-49	-*4)6	-88
4+0	+18	-18	0	-36	-	-54	-62	-98
-20,0	+20	-20	0	-40	-20	-60	-68	408

(+) , (-) ,

L6/n6

L6/k6

L6/j<sub>6</sub>

6

L6/g6

6

I

		X	X	X	X	0	X	нас.	наим.	0	X	1	X	X	§	§	s	
Q>6 3		-7	+17	+4	+15	+2	+13	0	+10,0	-3,0	+11	-2	+7		+5	-8	+1	-12
j 6	2	-7	+23	+8	+19	+4	+16	+1	+11,0	-4,0	+13	-2	+7	4	+3	42	4	-18
,	0	-	+26	+16	+		+17	id	+11,5	-4,5.	+14	4	<b>11</b>	4	+2	4	4	-22
.10 18	2	-7	+30	+12	+25	+7	+19	+i	+12,5	-5,5	+15	-3	+7	41	+1	.17	-9	-27
.18 30	0	-8	+36	+15	+29	+8	423	+2	+14,5	-6,5	+17	-4	+8	43	")"1	-20	42	-33
.30 50	0	-10	+43	+17	+&	±		+2	+18,5	-8,0	+21	-5	+10	-16	+1	45	-15	41
.50 80	0	-12	+51	+20	+42	+ii	+33	+2	+21,5	-9,5	+24	-7	+12	<b>1</b>	£	49	48	-49
.80	0	j-15	+60	+23	+50	+13	446	+3	+26,0	-11,0	+28	-9	+15	<b>-4</b>	+3	44	-21	-58
.120 180	0	-18	±!	+27	+58	+15	+46	+3	+30,5	-12,5	+32	41	+18	-25	+4	49	-25	-68
:180 250	0	-22	+82	+31	+68	+17	+55	+4	+36,5	-1+5	+38	-13		-	<b>+1</b>	-44	-28	-79
,280 315	0	-25	+91	+34	+W	+20	+61	+4	+41,0	-16,0	+41	-16	+25	42	+8	49	-31	-88
→, 315 400	0	-30	+103	+37	+87	+21	+70	+4	+48,6	-18,0		-18	+30	-35	+12	-54	-32	-98
.400 500	0	-35	+115	+40	+98	+23	+80	+5	+55,0	-20,0	+55	-20	+35	4(1	+15	-60	-33	-108
.500 630	0	-40	+128	+44	+110	+26	+84	0	+62,0	-22,0		+40	44	+18		-36	-120	

6

		, ,																	
				7		N7		7		7		V		J7		7		G7	
D,		JL, 1																	
				• s	• s	0	• s		%	0 s	i	t	• s	s t s	i	• % 0 <sup>1</sup>	i		
25	3	0	-7	-6	-1	-4	-14	-2	-12	0	-10	+5	-5	+4	-6	+10	0	+12	+2
, 3	6	0	"7	-8	10	-4		0	-12	+3	-9	+6	-6	+5	-6	+12	0	+16	+4
. 6		0	-7,	9	-24	-4	-19	0	15	+5	-10	+7	-7	+8	-7	+15	0	+20	
. 18		0	"7	-	-29	-5	-23	0	-18	+6	-12	+9	-9	+	-8	+18	0	+24	+6
, 18	30	0	-8	-14	-35	-7	-28		-21	+6	-15	+10	-10	+12	-9	+21	0	+28	+7
30	50	0	-9	-17	-42	-8	-33	0	-25	+7	-18	+12	-12	+	-	+25	0	+34	+9
50	80	0	J	-21	-51	-9	-39	0	-30	+3	-21	+15	-15	+18	-12	+	0	+44	+10
. 80	120	0	-13	-24	-59	-10	-45	0	15	+10	-25	+17	-17	+22	-13	+35	0	+47	+12
, 120	150	0	-15	-28	-68	-12	-52	0	-40	+12	-28	+20	-20	+26	-14	+40	0	+54	+14
. 150	180	0	-18	-28	-68	-12	-52	0	-40	+12	-28	+20	-20	+26	-14	+40	0	+54	+14
. 180	250	0	-20	-33	-79	-14	-50	0	-46	+13	-33	+23	-23	+30	-16	+	0	+61	+15

D, 0 ,		, ,																
		7	N7	w	K7	V	J7	H7	G7									
x )	39	s <sub>0</sub>	i	* o 10	t i s id %	o x id x	i s a x	v t a x	i a	e s 1 1 x	i s a	i x s	i s p	o x s	2	«	1 t x	
.250 315	0	-25	-36	-88	-14	-66	0	-52	+16	-36	+26	-26	+36	46	+52	0	+69	+17
.315 400	0	-28	41	-98	-16	-73	0	-57	+17	-40	+28	-28	+39	-18	+57	0	+75	+18
,400 500	0	-33	-45	-108	-17	-80	0	-63	+18	-45	+31	-31	+43	-20	+63	0	+83	+20
500 630	0	-38	-78	-148	-44	-114	-26	-96	0	-70	+35	-35			+70	0	+92	+22
.630 800	0	<b>-45</b>	-88	-108	-50	-130	-*	-110	0	-80	+40	-40			+80	0	+104	+24
.W0 1001)	0	-60	-100	-190	<b>-50</b>	-146	-34	-124	0	-90	+45	-45			+90	0	+116	<b>+26</b>

6

D,								(+) ,		(-) ,									
		X	—	0	1	X	—	X	X	«	»	X	—	1	i	0	>	i	X
2,5	3	0	-7	+10	£	+14	-3	+12		+10	-7	+5	-12	46	1-11	0	-17	4	-49
6		2		+20	+L	+		+12	-7	+9	-10	+6	-18	tl	43	£	49	4	43
.6	10	0	-7	+24	+2	+19	-3	+15		+10	-12	+7	44	+7	45		42	-5	47
.10	18	0	-7	+29	+<	+23	-2	+18	-7	+12	-13	+9	-16	+8,	-17		-25		31
.18	30	0	-8	+35	+6	+28	-1	+21		+15	-14	+10	-18	+9	40	0	-29	4	-46
.30	50	2	-9	+42	+8	+83		+25	-9	+18	-16	+12	-21	+	43	£	-34		-43
,50	80	0	-	+51	+10	+39		+30	41	+21	-20	+15	-26	+12	-29	0	1	-10	41
.80	120	2	-13	+59	+	+45	-3	+35	-13	+25	-23	+17	-30	+13	-35		-48	-12	-60
.128	150	0	45	+68	+13	+52		+40	45	+28	-25	+20	45	+14	-41	0	-55	44	49
.150	180	2	-18	+68	+10	+52		+40	-18	+28	40	+20	48	+14	-44	£	48	44	42
.180	250	0	-20	+79	+13	+60		+46	-20	+33	-33	+23	43	+16	40	0	-66	-15	41

D, 0		m m		(+), (-), ,															
				J <sub>s</sub> 7//6		J7//6		7//6											
« ft	i 1C	s	s 80	t s X	£	t	£	0 s	i «		£	0 s	%	g	£	0	£		
.250	315	0	-25	+88	+11	+66	-11	+52	-25	+36	-41	+26	-51	+16	-61	0	-77	-17	-94
,315	400	0	-28	+98	+13	+13	-12	+57	-28	+40	-45	+28	-56	+18	-67	0	-85	-18	-103
.400	500	0	-33	+108	+12	+80	46	+63	-33	+45	-51	+31	-64	+20	-76	0	"96	-20	-116
.500	630	0	-38	+148	+40	+	+6	+96	-12	+70	-38	+35	-73			0	"108	-22	-130
,630	800	0	-45	+168	+43	+130	15	+110	-15	+80	-45	+40	-85			0	'125	-24	-149
.800	J000	0	-60	+190	+40	+146	+4	+124	-26	+90	-60	+45	-105			0	'150	46	-176

5

i	d <sub>m</sub> , ,	(+) (4), ,													
		15/		L5/m5		L5/k5		mt		15/15		15/ 5			
		v	s <sub>i</sub> s	( s s :	0	> %	0	i 3	2 «	t » X	2	1	1 2	i X X	
0,6 3	0 -5	+13	+4	+	+2	+9	0	+7,0.	-2,0	+7	-2	£	4	+3	4
.3 6	0 -5	+18	+8	44	+4	+11	+i	+7,5	-2,5	+8	-2	-	+5	4	+1 -9
.6 10	0 -5	+21	40	+17	£	42	+i	+8,0.	4,0	+9	~	+5	4	0	
.10 18	0 4	+25	+12	t-20	+7	+14	+i		-4,0	+10	4	+5	4	-1	
.18 30	0 4	+30	45	+23	+8	+17	+2	+10,6	-4,5	+11	-4	1	4	-1	
.30 50	0 4	+36	+	+28	+9	+21	+2		-5,0	+14	-5	+	-	4	
.50 80	0 -9	+42	+20	+33	+11	+24	+2	+15,5	-6,5	+15	~7	-	-13	-1	
.80 120	0 40	+48	43	+38	+13	+28	+3	+17	4,5	+16	4	+10	-15	-2	-27
.120 180	0 -13	+58		+46	45	+34	+3	+22,0	4,0	+20	41	+13	48	+1	-32
.ISO 250	0 -15	+66	41	+52	+17	+39		+25,0	-10,0	+22		+15	-20	0	-35
,250 315	0 -18	+75	+34	+61	+20	+45	+4	+205	-11,5	+25	-16	+18	-23		40
.315 400	0 -23	+85	47	+69	+21	+52	+4	+35	-12,5	+30	-18	+23	-25	+5	43

S

D,	L	S															
		N6				J6				6				G6			
		X (X)	I S	X X X	si * S	X X X	si i t	S X S	s: t S								
5,5	3	0	-5	-4	-10	-2	-8	0	-6	+3,0	-3,0	+2	-4	46	0	+8	42
		0	-5	-5	-13	1	-9	+2	-6	+4,0	-4,0	+5	-3	+8	0	412	4*4
	10	0	-5	-7	-16	-3	-12	+2		*4,5		+5	-4	+9	0	414	49
10	18	0	4	-9	-20	-4	-15	+2	-9	+5,5	-5,5	±6	-5	+11	0	+17	46
18	30	0	-6	-	-24	-4	-17	+2	-11	+6,5	-6,5	+8	-5	413	0	+20	+7
30	50	0	-7	-12	-28	-4	-20	+	-13	W.			-6	416	0	+25	49
50	80	0	-9	-14	-33	-5	-24	+4	-15	+9,5	-9,5	+13	-6	419	0	+29	410
80	120	0	-10	-16	-38	-6	-28	+4	-18	+11,0	-11,0	416	-6	+22	0	434	
120	150	0	-11	-20	-45		-33	+4	-21	+12,5	-12,5	+18	jj	+25	0	•139	414
1	180	0	-13	-20	-45	-8	-33		-21	+12,5	-12,5	418	-7	+25	0	439	414
180	260	0	-15	-22	-51	-8	-37	+5	-24	±14,5	-14,5	422	-7	429	0	444	415
260	315	0	-18	-25	-57	-9	-41	+5	-27	+16,0	-16,0	+25	-7	+32	0	+49	417

D..		, ,															
		N6								V		J6		6			
:	*	X	X	V	5	I	»		1	X	X	«	X	«	X	&	S
⋮	⋮	X	X	X	X	I	»	S	1	X	X	«	X	«	X	&	S
315	400	(1	-5»	-26	-62	-10	-46	+7	49	+18,0	-18,0	+29	-7	+36	0	+54	+18
400	500	0	-23	-27	-67	-10	-50	+8	-32	+20,0	-20,0	433	-7	+10	0	+60	+20
500	630	0	-28	-44	-88	-26	-70	0	-44	+22,0	-22,0			+14	0	+66	+22
630		0	-35	-50	-100	-30	-80	0	-50	+25,0	-25,0			+50	0	+74	+24



D,		(+) , , ,															
		£														J6//5	
		&	*	s%	†	‡	0	5	s	>	X)	2		X	Q	1	X
, 315	4§	0		+62	+6	+46	-10	+29	-27	+18,0	-38,0	+7	-49	0	-56	-18	-74
, 400	500	0	-23	+67	+4	450	-13	+32	-31	+20,0	-43,0	+7	-56	0	-63	-20	-83
. 500	630	0	-28	+88	+16	+70	-2	+44	-28	+22,0	"50,0			0	-72	-22	-94
, 630	800	0	-35	+100	+15		-5	+50	-35	+25,0	"60,0			0	-85	-24	-109

i	, d <sub>ffl</sub> ,	, ,														
		5		5		5				15		h5		g5		
		s' 0	“ £	V 4>	£ £	:	X £	4) 4)	X X	a £	£ £	X 4)	s %	a) 4)	£ 5	g 4)
0,6 3	0	-4	+8	+4	+	+2	+4	0	+2	-2	+2	4	0	-4	4	4
.3 6	0	-4	+13	+8	+9	+4	+6	+1	+2	4	+3	-2	0	4	)	
.6 10	0	-4	+16	+10	+12	+6	+7	+1	+3	4	+4	-2	0	4	4	41
.10 18	0		+20	+12	+15	+7	+9	+1	+4	-4	+5	4	0	4	-6	44
.18 90	0	-5	+24	+15	+17	+#	+11	12	+4	-4	+6	-4	0	4	4	-6
,30 50	0	4	+28	+17	+20	+9	+13	+2	+5		+0	4	0	41	4	40
.50 80	0	7	+33	+20	+24	+11	+15	12	+6	4	+6	-7	0	43	40	43
.80 120	0	4	+38	+23	+28	+13	+18	+3	+7	-7	+6	4	0	45	42	-27
.120 180	0	-10	+45	+27	+33	+15	+21	-"3	+9	4	+7	-	0	48	-14	-32
,180 250	0	-12	+51	+31	+37	+17	+24	+4	+10	-10	+7	-13	0	-20	45	45

J rf <sub>g</sub>		(+) (−) ,																	
		L4/n5			/		L4/k5		,5		L4/h5			L4/g5					
		X	X	X	S	0	i	%	IS	i	8	5	S	S	S	0	X	a	S
0,6	3	0	-4	+12	+4	+10	42	+8	0	46,0	-2,0	46	-2	44	4	42	-6		
.3	6	0	4	+17	+8	+13	44	410	41	46,5	-2,5	+7	-2		-5	0	-9		
.6	10	0	-	+28	+10	410	+	+11	+1	+7,0	-3,0	43	-2	44	-6	-1	-11		
10	13	0		424	412	+13	+7	413	41	48,0	-4,0	+9	4	+1		J	-14		
,18	30	0	-5	429	415	+22	48	+15	+2	+9,5	4,5	4	4	+5	-9	-2	46		
.30	50	0	-5	434	417	+20	+9	419	42	4   5	-5,5	412	-	46	-	-3	-20		
,50	80	0	-7	440	420	431	+	422	42	+13,5	-6,5	413	-7	+7	-13		-23		
.80	120	0	-8	446		+35	413	426	+3	+15,5	-7,5	414	4	+8	-15		-27		
.120	180	0		455	427	+43	415	+31	t3	+19,0	-9,0	417	41	+18	46		42		
.180	250	0	-12	463	431	449	+17	436	+1	+22,8	-10,	419	43	412	-20		45		

4

D, »	D <sub>eff</sub>		N6		5		V		J6		6		G6			
	£	s	£	si S	£ a	%	£ «	£ X	£ a	· X	£ a	X 5	£ 8)	£ v	£ 8	£ X
2,5 3	0	-4		-10	-2	-8	0	4	+3,0	-3,0	+2	4	+6	0	+8	+2
,3 6	0	-4	-5	-13	-1	-9	+2	-6	+4,0	-4,0	+5	-3	+8	0	+12	+4
6	0	-4	-7	-16	-3	-12	+2	-7	+4,5	-4,5	+5	-4	+9	0	+14	+5
10 18	0	-4	-9	-20	-4	-15	+2	-9	+5,5	-5,5	+6	-5	+11	0	+17	+6
,18 30	0	-5	-11	-24	-4	-17	+2	-11	+6,5	-6,5	+8	-5	+13	0	+20	+7
30 50	0	-6	-12	-28	-4	-20	+3	-13	+8,0	-8,0	+10	-6	+16	0	+25	+9
.50 80	0	-7	-14	-33	-5	-24	+4	-15	+0,5	-9,5	+13	-6	+19	0	+29	+10
,80 120	0	-8	-16	-38	-6	-28	+4	-18	+11,0	-11,0	+16		+22	0	+34	+12
,120 150	0	-9	-20	-45	-8	-33	+4	-21	+12,5	-12,5	+18	-7	+25	0	+39	+14
.150 180	0	-10	-20	-45	-8	-33	+4	-21	+12,5	-12,5	+18	-7	+25	0	+39	+14

D, 0,	N6	, ,												G6		
		V		J6												
		X	X	X <sup>1</sup> ft	X <sup>1</sup> ffl	X	X <sup>1</sup> i	X	X <sup>1</sup> ft	X <sup>t</sup>	X	X <sup>1</sup> ft	X	X <sup>8</sup> a	X <sup>1</sup> *	
, 180 250	0	-	-22	-51	-8	-37		"21	+14,5	-14,5	+22	-7	+29	0	*44	+15
. 250 315	0	-13	-25	-57	-9	41	+5	-27	+16,0	-16,0	+25	-7	+32	0	+49	+17
. 315 400	0	-15	-26	-52	-10	-46	+7	-29	+18,0	-18,0	+29	-7	+36	0	+54	+18

D, V	N6//4	(+) (−) ,													
		J6//H				J6//4				G6//4					
		4 X 45	:	0	1 N X	4 5	1 3 18 X	X	5 (0)	0 s	— —	X	i s	5 X	X X
2,5 3	0 -4 +10 0 +8 -2 +6 -4 +3,0 -7,0 +4 -6 0 -10 -2 -12														
,3 6	0 +13 +1 +9 -3 +6 -2 +4,0 -8,0 43 -9 0 -12 -4 -16														
.6 10	0 -4 +16 +3 +12 -1 +? -2 +4,5 -8,5 4-4 -9 0 -13 -5 -18														
.18	-4 +20 +5 +15 0 +8 -2 +5,5 -9,5 +5 -10 0 -15 -6 -21														
.18 30	0 -5 +24 +6 +17 -1 +11 +6,5 -11,5 +5 -13 0 -18 -7 -25														
.3» 50	0 +28 +6 +20 -2 -3 +8,0 -14,0 +6 -16 0 -22 - -31														
50 80	0 -1 +33 +7 +24 +15 -3 +9,5 -16,5 +6 -20 0 -26 -10 -36														
120	0 -8 +38 +8 +28 -2 +18 -4 +11,0 -19,0 +6 -21 0 -30 -12 -42														
.120 150	0 -9 +45 + +33 -1 +21 -5 +12,5 -21,5 +7 -27 0 -34 -14 -48														
150 180	0 40 +45 +10 +33 -2 +21 4 +12,5 - -28 0 -35 -14 -49														

Продолжение табл. 16

D, D <sub>w</sub>	N6//4	(+) (−), ,														
		6/		J <sub>3</sub> 6//4				/4				G6//4				
		X ta	*	V X	i X	0 X	i X	0 <sup>4</sup> X	i X	0 X	3 X	X X	i X	0 X	<sup>1</sup> t X	
100 250	0	-	451	+11	+37	-3	+24	-6	+15	-25,5	+7	-3+		-40	-	-55
253 315	0	-13	+57	+12	+41	-1	+27	-8	+18,0	-29,0	+7	-38	0		-17	-62
315 400	0	-15	48	+11	+46	-5	+29	-8	+18,0	-33,0	+7	-44	0	-51	-ft	-69

1	,	,												
		4		V		*		f t		/		.		
0,6	0	-4,9	+7	-4	+5	+2	+3	0	+1,5	-1,5	0	"3	"2	"5
,3 6	0	-1,0	+12	+8	+8	+4	+5	+1	+2,0	-2,0	0		-4	"8
,6 10	0	-4,0	+14	+10	+10	+6	+5	+1	+2,0	-2,0	0	-4	-5	"9
.10 18	0	"4,0	+17	+12	+12	+7	+6	+1	+2,5	-2,5	0	-5	-6	-
.18 30	0	-1,0	+21	+15	+14	+8	+8	+2	+3,0	-3,0	0	-	"7	"13
,30 50	0	-4,0	+24	+17	+16	+9	+9	+2	+3,5	-3,5	0		-9	"16
,50 80	0	-5,0	+28	+20	+19	+11	+10	+2	+4,0	-4,0	0		"10	-18
.80 120	0	"5,0	+33	+23	+23	+13	+13	+3	+5,0	"5,0	0	"10	-12	"22
,120 180	0	-0,5	+39	+27	+27	+15	+15	+3	+6,0	"6,0	0	"12	-14	"26
.180 250	0	"9,0	+45	+31	+31	+17	+18	+4	+7,0	-7,0	0	"14	-15	-29

2

rf <sub>a</sub>								(+)		4					
				L2/m4		12/						L2/M		Ufel	
		Q	S	I	S	(S)	t	Q	S	X	X	X	X	Q	S
0,6 3	0	-4,0	+11	+4	+9	+2	+7	0	+5,5	-1,5	+4,0	-3	+2,0	-5	
.3 6	0	-4,0	+16	+8	+12	+4	+9	+i	+6,0	-2,0	+4,0	-4	0	-8	
,6 10	0	-4,0	+18	tio	+14	+6	49	+i	+6,0	-2,0	+4,0	"4	-1,0	-9	
,10 18	0	-4,0	+21	+12	+16	+7	+10	+i	+6,5	-2,5	+4,0	-5	-2,0	-	
.18 30	0	-4,0	+25	+15	+18	+8	+12	+2	f7,0	+3,0	+4,0	-6	-3,0	-13	
30 50	0	-4,0	+28	+17	+20	+9	+13	+2	+7,6	-3,5	+4,0	"1	-5,0	-16	
.50 80	0	-5,0	+33	+20	+24	+11	+15	+2	+9,0	-4,0	+5,0	*-8	-5,0	-18	
,80 120	0	"5,0	+38	+23	+28	+13	+18	+3	+10,0	-5,0	+5,0	-10	-7,0	-22	
.130 180	0	-6,5	+45	+21	+33	+15	+21	+3	+12,0	-6,0	+6,5	-12	-7,5	-26	
.18» 250	0	"9,0	+54	+31	+40	+17	+27	+4	+16,0	-7,0	+9,0	-14	-6,0	-29	



D,	,	(+) , (-) , ,										
		5/2		5/2		5/		j <sub>s</sub> 5		5/2		
		,	*	,	,	,	,	,	Q	,	,	
U	0	"3,0	+8	+12	+6	-1,0	+4	-	+2,0	-5,0	0	4
3 6	0	-3,0	+12	+1,0	+8	0	+5	-3,0	+2,5	45	0	J 42
,6 10	0	-3,0	+4	+5,0	+10	+1,0	+5	-4,0	+3,0	-6,0	0	J -5 44
18	J_	-3,0	+17	+6,0	+	+1,0	+6	-5,0	+4,0	-7,0,	0	41 4
, 18 30	0	-1,0	it	+82	+14	+1,0	+8		+4,5	-8,5	0 4	-7 -20
. 30 50	0	4,0	it	+W	+16	+1,0	+9	-6,0	+	-9,5	JL 4!	-9
. 50 80	-	4,0	it	+1+0	+19	+2,0	+10	-7,0	+6,5	-10,5	0 j)	-27
. 80 120	-0	-5,0	+	+13,0	+23	+3,0	+13	-7,0	+7,5	-12,5	0 ^20 42	42
150	0	-5,0	+39		+27	+4,0	+15	-8,0	+9,0	-14,0	0 J3	-14 -37
. 150 180	0	-6,5	it		+27	+2,5	+15	-9,5	+9)0	-15,0	0 -	-14 -38
. 110 250	0	-8,0	+45	+	+31	+3,0	+18	40,0	+10,0	-18,0	0	-15
250 315	0	-10,0	it	+17,0	+36	+3,0	+20	-13,0	+,	41,5	0	47 -50
, 315 400	0	-12,0	+55	+18,0	+39	+2,0	+22	-15,0	+12,0	-24,5	0	48 -55

d,	*	15	1(6)										16		ha		\$	
			X	X	&	S	X	8	X	X	X	X	V	X	X	X	X	X
10 18	0	-8	+23	+12	-18	+1	+5,5	-5,5	+8	-3	0	-11	-6	-17				
18 30	0	-10	+28	+15	+21	+8	+15	+2	+6,5	-6,5	+9	-4	0	-13	-7	-20		
30 50	0	-12	+33	+17	+25	+9	+18	+2	+8,0	-8,0	+11	-5	0	-11	-9	-25		
50 80	0	-15	+39	+20	+30	+11	+21	+2	+9,5	-9,5	+12	-7	0	-19	-10	-29		
	0	-	+4	+		413	+25	+3	+	-	+13	4	0	-22	-12	-34		
100 180	0	-25	+52	+27	+40	+15	+28	43	+12,5	-12,5	+14	-11	0	-25	-14			
180 250	0	-30	+60	+31	+6	+17	+33	+4	+5	-14,5	+18	-13	0	-29	-15		z	
250 315	0	-35	+66	+34	+52	+20	+36	+4	+16,0	-16,0	+16	-16	0	-32	-17	-49		
315 400	0	-40	+73	+37	+57	+21	+9	+4	+18,0	-18,0	+18	-18	0	-36	-18	-51		

d, °		d <sub>m</sub>		(+) (−),													
				I		I		L0/k6		L0/j <sub>s</sub> 6		L0/J6		L0/h6			
				•	«	0°	š	0	s	0	•	0	8	0 <sup>a</sup>	1	0 <sup>1</sup>	«
10	18	0	-8			+12	+20	+7	+20	+1	+13,5	-5,5	+16	{8	-	*1*2	-17
.18	30	0	-10	+38	+15	+31	+8	+25	+2	+16,5	-6,5	^ 19	-4	+10	-13	+3	-20
.30	50	0	-12	+45	+17	+37		+30	+2	+20,0	-8,0	+23	-5	+12	-16	+3	-25
.50	80	0	-15	+54	+20	+45	tü	+36	42	+24,5	-9,5	+27	J1	+15	-19	+5	-29
.80	120	0	-20	+65	+23	+55	+13	+45	43	+31,0	-11,0	+33	4	+20	-22	+8	-34
120	180	0	-25	+77	+27	+65	115	+53	+	+37,5	-12,0	+39	-	+25	-25	+11	-39
.180	350	0	-30	+90	+31	+76	+17	463	+4	+44,5	-14,0	+46	-13	+30	-29	+15	-44
.315		0	-35	+101	+34	+87	+20	+71	+4	+51,0	-16,0	+51	-16	+35	-32	+18	-49
,315	400	0	-40	+113	+37	+97	+21	+80	+4	+58,0	-18,0	+58	-18	+40	-36	+22	-54

D, .	D <sub>m</sub> , .	.											
		N7		7		7		V		J7		7	
.	.	.	.	.	.	.	.	.	.	.	.	.	.
18 30	0	-9	-7	-28	0	-21	+6	-15	+10	-10	+12	-9	+21 0
30 59	0	-11	-8	-33	0	-25	+7	-18	-2	-12	+14	41	+25
50 80	0	-13	-9	-39	0	-30	+9	-21	+15	-15	+18	-12	+30 0
80 1120	0	45	-10	-45	0	-35	+10	-25	+17	47	+22	43	+35 0
120 150	0	-18	42	-52	0	-40	+12	-28	+20	-20	+26	44	+40 JI
150 180	0	-25	»12	-52	0	-40	+12	-28	+20	-20	+26	-14	
1«0 250	0	-30	-14	-60	0	-46	+13	-33	+23	-23	+1	46	+46 0
250 315	0	-35	-14	-66	0	-52	+16	-36	+26	-26	+36	46	+52 0
315 400	0	-40	-16	-73	0	-57	+17	-40	+28	-28	+39	-18	+57 0
« 400 500	0	-45	-17	-80	0	-63	+18	45	+31	-31	+43	-20	+63
500 630	0	-50	-44	414	-26	-96	0	-70	+35	-35			+70 0


18 30	0	-9	+28	-2	<b>421</b>	<b>JL</b>	+15	-15	<b>410</b>	-19	49	-21	0	-30
.30 60	0	-	4-33	-3	425	1	+18	-18	412	-23	411	-25	0	-36
,50 80	0	-13	439	-4	+30	-13	+	-22	415	-28	+12	-31	0	"43
.80 120	0	-15	+45	-5	+35	-15	425	-25	+17	-32	+13	-37	0	-50
,120 150	0	-18	452	-6	+40	-18	428	-30	+20	-38	+16	-44	0	-58
.150 180	0	-25	452	-13	+40	-25	+28	"37	+20	-45	4	-51	0	-65
.180 250	0	-30	460	-16	446	-30	+33	-43	+23	-53	+16	-60	0	<b>ZH</b>
.250 315	0	-35	466	-21	452	<b>-35</b>	+36	-51	+26	-61	+16	-71	0	-87
,315 400	0	-40	473	-28	+57	-40	+40	-57	428	-68	+18	-78	0	-97
.400 500	0	-45	<b>480</b>	-24	+63	-45	+65	-63	431	-76	<b>420</b>	-88	0	-108
,500 630	0	-50	+114	-6	+96	-24	470	-50	+35	-85			0	-120

1		4>		, ,											
				V			J*			h6					
		—	—	X	X	X	X	X	X	X	X	X	X	X	X
10 18	0	-7	+23	+12	+18	+7	+12	+1	+5	-5	48	-3	0	-	-6 48
. 18 30	0	-8	+28	+15	+21	+8	+15	+2	+6	^1	+9	*	0	-13	-7 -20
30 50	0	-10	+33	+17	+25	+9	+18	+2	+8	“	+11	-5	0	-16	-9 -25
50 80	0		+39	+20	+30	+	+21	+2	+9	-9	+12	-7	0	-19	-10 -29
. 80 120	0	45		+23	+35	+13	+25	+3	+	-	+13	-9	0	-22	-12 -34
, 120 180	0	48	+52	+27	+40	+15	+28	+3	+12	-12	+14	-	—	-25	-14 -39
. 181) 258	0	-22	+60	+31	+46	+17	+33	+4	+14	-14	+16	43	0	-29	45 -44
. 250 315	0	-25	+66	+34	+52	+20	+36	+4	+10	-16	+16	-	0	-32	-17 49
. 315 400	0	-30	+73	+37	+67	+21	+40	+4	+18	-18	+18	-18	0	-36	-18 -54

i		d <sub>tt</sub>		(+) , (-) ,														
				L6/n6		L6/m6		L6/k6		L6/j <sub>s</sub> 6		LW		L6/h6		L6/g6		
				41	S	»	1 S	•	» X	0	# X	0	X	0	1 S	0	1 X	
10	16	0	-7	+30	+12	+		+7	+19	+1	+12,5	-5,5	+15	-3	+7	-11	+1	-17
.18	30	0	-8	+36	+15	+29	+8	+23	+2	+14,5	-6,5	+17	-4	+8	-13	+1	-20	
30	60	0	*10		+i?	+45	+0	+28	+2	+18,0	-8,0	+21	4	+10	46	+1	-25	
50	80	0	-12	+51	+20	+42	+11	+33	+2	+21,5	-9,5	+24	-7	+12	49	+2	-29	
.80	120	0	-15	+60	+23	+50	+13	+40	+3	4-26,0	41,0	+28	-9	415	-22	+3	£1	
.120		0	-18	+70	+27		+15	+46	£	+33,5	-12,5	+32	-11	+18	-25	+4	-39	
.188	258	0	-22	+82	+31	+68	+17	+55	+4	+36,5	-14,5	+38	-13	+22	-29	+7		
.250	315	0	-25	+91	+34	+77	+20	+51	44	+41,0	-16,0	+41	46	+25	-32	+8	49	
315	488	0	-30	+103	+37	+87	+21	+70	+4	+48,0	-18,0	+48	-18	+30	-36	+12	-54	

↓

o.	V»	N7		7		7		V		J7			
18 30	0	-8	-7	-28	0	-21		15	+10	40	+12	4	421 0
30 50	0	»9	~8	-33	0	-25	+7	48	+12	42	+	-	+8 0
50 80	0	-	it	-39	0	40	+3	41	+15	-15	418	42	430 0
80 120	0	»11	-10	-45	0	45	+10	-25	417	47	+22	-13	+35 0
120 150	1	-15	42		0	-40	+12	48	+20	-20	426	44	+40 0
150 180	0	-18	-12	4	0	-40	+12	*^"28	+20	40	+26	44	+40 0
180 250	0	-20	-	-60	0	46	+13	-33	+23	-23	430	-16	+46 J)
250 315	0	-25	-14	4	0	42	+16	46	426	-26	436	-16	+52 0
315 400	0	-28	-16	-73	0	47	+17	-40	+28	48	+39	^18	457 0
400 500	0	-33	-17	-80	0	43	+18	45	+31	41			+63 0

D,		,		,		(+),		(-),		,		,		,	
														M7/16	
		,	,	,	,	,	,	,	,	,	,	,	,	aafIH,	,
0t	30	0	-8	+28	-1	+21		115	-14	+10	-18	+9	-20	0	-29
.30	50	0	-9	+33			-9	+18	-16	+12	-21			0	-34
.50	80	0	-11	+39	-2	+30	-	+21	-20	+15	-26	+			-41
.83	120	0	43		4	+35	-13	+25	-23		-30	+13	-35	0	-48
.120	150	0	-15	+52	-3		-15	+28	-25	+20	-35	+14			J8
.150	180	0	-18	+52	-	+40	-18	+28	-30	+20	-38	+11	-44	0	
,180	250	0	-20	+60	-6	+46	-20	+33	-33	+23	-43	+16	-50	0	-66
.250	315	0	-25	(-66	-11	+52	-25	+36	-41	+26	-51	+16	-51	0	dL
.315	«0	0	-28	j-	-12	+5?	-28	+40	-45	+28	-56	+18	-67	0	-85
,400	600	0	-33	+80	-16	+63	-33	+45	-51	+31	-64	+20	^76	0	-96

4		, ,															
		5		m5		1(5						15		h5			
		•	х	и	и	х	и	0	х	и	0	х	и	е	х	х	0
10 18	0	-7	420	+12	+15	+7	+9	+1	+4	-4	+5	-3	0	-8	-6	-14	
.18 30	0	-8	+24	+15	+17	+8	111	12	+4	-4	+5	-4	0	-9	-7	-16	
.30 50	0	-10	-28	+17	+20	+9	+13	+2	+5	-5	+6	-5	0	-11	-9	-20	
.50 80	0	-12	+33	+20	+24	+11	+15	+2	+6	-6	+6,	jj	0	-13	-10	-23	
.80 120	0	-15	+38	+23	+28	+13	+18	+3	47	-7		-9	0	-15	-12	-27	
.12» 180	0	-18	+45	+27	+33	+15	+21	+3	+9	-9	+7	-11	0	-18	-14	-32	
.180 2§	0	-22	451	+34	+37	+17	+24	+4	+10	-10	+7	-13	0	-20	-15	-35	
250 315	0	-25	+57	+34		+20	+27	+4	+11	-11	+7	-16	0	-23	-17	-40	
.315 «	0	-30	+62	+37	+46	+21	+29	+4	+12	-12	+7	-18	0	-25	-*18	-43	

i		-		(+) , , ,															
				L5/n5		L5/m5		L5/k5		LS/1,5				1 >					
				s f <sup>t</sup> )	s <sup>•</sup>	«	0 <sup>•</sup>	s <sup>•</sup>	«	t	s <sup>t</sup>	0 <sup>t</sup>	« 1	0 <sup>t</sup>	x «	«	1		
10	18			0	-7	+27	+12	+22	+7	+16	41	+11		+12	-3	+7	-8	+1	-14
18	34)			0	-8	+8	+15	+25	+8	+19	+2	+12	-4	+13	-4	+8	-9	+1	-16
, 30	50			0	-10	+38	+17	+30	+9	+23	+2	+15	-5	+16	-5	+10	-11	+1	-20
50	80			0	-12	+45	+20	+36	+	+27	+2	+18	-6	+18	-7	+12	-13	+2	-23
, 80	120			0	-15	+53	+23	+43	+13	+33	+3	+22	-1	+21	-9	+15	-15	43	-27
. 120	180			0	-18	+63	+27	+51	+15	+39	+3	+27	-9	+25	-	+18	-18	+4	-32
180	250			0	-22	+73	+31	+59	+17	+45	+4	+32	-	+29	-13	+22	-20	+7	-35
260	3-15			0	-25	482	+34	+68	720	+52	+4	+35	-11	+32	-16	+25	-23	+8	-40
. 315	4			0	-30	+02	+37	+76	+21	+59	+4	+42	-12	+37	-18	+30	-25	+12	-43

		0 ,		N6										J <sub>s</sub> 6		J6		H6	
				t X •	g X X	S EQ	g X	*	*	X	-	*	0	g 31 0	θspX	g 8 8	g X g	X X	
18 30		0	-8	-	-24	-4	-17	+2	-11	+6,5	-6,5	-	-8	-5	4 <sup>13</sup>	0			
.1 50		0	-9	-12	-28	-4	-20	+3	J-U	+8,0	-8,0	•jjfl	-6	416	0				
50 80		0	-11	-14	-33	-5	-24		-15	+9,5	-9,5	413	-6	419	0				
.80 120		0	-13	-16	-38	-6	-28	4	-18	+11,0	-11,0		-6	+22	0				
.120 150		0	-15	-20	-45	-8	-33	4-4		412,5	-12,5	+18	-7	11	0				
.150 180		0	-	-20	-45	-8	-33	44	-21	+12,5	-12,5	418	-7	425	0				
.180 250		0	-20	-22	-51	-8	-37	45	-24	+14,5	-14,5	422	-7	+29	0				
.250 315		0	-25	-25	-57	-9	-41	45	-27	+16,0	-16,0	425	-7	+32	0				
,315 400		0	-28	-26	-62	-10	-46	+7	-29	+16,0	-18,0	429	-7	436	0				
,400 500		0	-33	-27	-57	-10	-50	+8	-32	+20,0	-20,0	433	-7	440	0				

D, .	,	(+) , (-) ,													
		N6//5			/S		6//5			J6//5					
		2) ±±1	Hi S	3 X	1 X	2 X	% X	0 X	i	X X	X X*	2 X	.	X X	X X
18 30	0	-8	+24	43	+17	4	+11	-10	+6	-14	+6	-16	0	-21	
30 50	0	-9	+28	+3	+20	4	+11	42	+8	47	+6	-19	0	-25	
50 80	0	41	"1*33	+3	+24	-6	+15	-15	+9	-20	+6	-24	0	-30	
.80 120	0	-13	+38	+3	+28	-7	"1^	-17	+11	-24	+6	-29	0	45	
.120 159	0	-15		+L	+33	-7	421	-19	+12	-27	-17	43	0	-40	
.150 180	0	48	+45	+2	+33	-10	+21	"22	42	-30	17	46	0	-43	
.180 250	0	-20	+51	il	+37	-12	+24	-25	+14	44	+7	42	0	-49	
.250 315	0	-25	+57	0	+41	46	+27	-30	+16	"41	+7	-50	0	47	
315 400	0	-28	+62	-2	+46	48	+29	-35	+19	-46	41	-57	0	-64	
.400 500	0	-33	+67	-6	+50	-23	+32	41	+29	-53	+7	46	0	-73	

1		da,		,										
				5	5	k5	1,5	15	5	g5				
X 4)	ä	X 4)	ns s	s ä)	s X ä)	t X ä)	X	X 4)	X s	*	X 4)	X ä)	g X ä)	
10 18	0	-5	+20	+12	+15	+7	19	+i	+4	-4	-3	0	-8	-14
.18 30	0	-6	+24	+15	+17	18	+ii	+2	+4	-4	-4	0	-9	-1 -16
,30 50	0	-8^28	+1720	9	+13	+2	+5	-5	+6	-5	0-11	-9	-20	
.50 80	0	-9	+33	+20	+24	+15	-2	+6	-7	0-13	-10	-23		
,80 10	0	-10t38	+2328	1318	+3	+7		+6	-9	0	-15	-12	-27	
120 1800	-13	+45	+2733	1521	+3	+9		+7-11	0-18	-14	-20	-15	-32	
.180 2500	-15	15	+3137	1724	+4	+10-10	+7	-130	-20	-15	-35			

i		$d_a$		(+) (0), ,												
				L4/m5		LijkS		UI1.S		5		L4/h5		i#		
		« X » X	1 X	1 X X	0 X X	4 X X	« X X	0 X X	*	X X	“ t V!	i 1)	X X	0 X X	1 X	
10	13 0	-5	25	+12	20	7 <sup>-14</sup>	+1	+9	-4	+	-3	+5	-8	""	1-14	
. 18	300	-6	30	+15	23	+17	2+10	-4	+12	-4,	+6	-9	-1	-1	-16	
. 30	500	-8	+35	+17	28 <sub>9</sub>	+21	+2	+13	-5	+14	-5	+8	-11	1	-20	
. 50	80	0	-9	+42	+20	33	1+24	+13	-6	+15	-7	+9	-13	-1	-23	
. 80	120	0	*10	+48	+23	38 <sup>3</sup>	+28+3+17	-7	+15	-9	+10	-15	-2	-2	-27	
. 120	180	0	-13	58	+27	6	+15	+34	+3	+22	-9	+20	-	+13	-18	-32
, IM	250	-15	+66	+31	52	7	+39	+4	+25	-10	+22	-13	+15	20	0	-35

## 4

A		i o l																	
		N6		6		N		0)		X &		a X V		g t g		X t t		%	
		X f t	§	X f t	X X	R	N	X 0)	X &	a X V	g t g	X t t	%	S	X	g X	;		
18	30	0	-6	-	-24		-17	+2	-	+6	""		-5	+13	0				
30	50	0	-7	-12	-28	-4	-20	-f3	-11	+8	-8	+10	-6	+16	0				
50	80	0	-9	-14	-33	-5	-24	+4	-15	+9	-9	+13		+19	0				
120		0	-10	**16	-38	-^6	-28	+4	-18	+11	-	+16	4	+22	0				
120	1*50	0	-	-20	-45	-8	-33	+4	-21	+12	-12	+18	-7	+25	0				
150	180	0	-13	-20	-45	4	-33	+4	-21	+12	-12	+18	-7	+25	0				
1	250	0	-15	-22	-51	'8	-31	+5	-24	+14	-14	+22	-7	+29	0				
250	315	D	-18	-25	-57	-9	-41	+5	-27	+16	-16	+25	27	+32	0				
315	400	0	-20	-26	-62	-10	-46	+1	-29	+18	-18	+29		+36	0				

D,	N6/14	(+), (-), ,												
		6/		ip		ip		ip		ip		ip		
		X 0)	X *	0 3	% X	S S	S S	X 03 X	X X	V 8	I «	1 X X	S X	1 8
18 30	0 4	424	+5	<b>+17</b>	-2	+11	-8	+6,5	-12,5	+5	<b>-14</b>	0	-19	
3» 59	0 -7	+28	+5	+20	-3	+11	-10	+8,0	-15,0	+6	<b>-17</b>	0	-23	
.50 30	0 <b>-9</b>	+33	+5	+24	-4	+15	-13	+9,5	-18,5	+6	-22	0	-28	
.80 120	0 -10	+38	<b>+6-28</b>	<b>-4</b>	+18	<b>-14</b>	+11,0	<b>-21,0</b>		-26	<b>0</b>	-32		
.129 159	0 - <b>+45</b>	<b>+9</b>	+33	-3	<b>+21</b>	<b>-15</b>	+12,5	-23,5		<b>+7-29</b>	<b>0</b>	-36		
150 180	0 <b>-13-45</b>	<b>+7-33</b>	<b>-5+21</b>	<b>-17</b>			+12,5	-25,5		<b>+7-31</b>	<b>0</b>	-38		
.189 259	-15	<b>+51</b>	<b>+7-37</b>	<b>-7+24</b>		-20	+14,5	-29,6		<b>+7-37</b>	<b>0</b>	-44		
.250 315	<b>0</b>	-18	<b>+5?</b>	<b>+7-41</b>	<b>-9+27</b>	<b>-23</b>	+16,0	<b>-34,0</b>	<b>+7-43</b>	<b>0</b>	<b>-50</b>			
.315 400	0	-20	+62	<b>+6-46</b>	<b>-10-29</b>	<b>-27</b>	+18,0	-38,0		<b>+7</b>	<b>-49</b>	<b>0</b>	-56	

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10	18	0	-4,0	+17	<b>+12</b>	+12	+7	+6	+1	+2,5	-2,5	0	-5	-6	-11
18	30	0	-4,0	+21	+15	+14	+«	+8	+2	+3,0	-3,0	0	-6	-7	-13
30	50	0	-4,0	+24	+17	+16	+9	+9	+2	+3,5	-3,5	0	-7	-9	-16
<b>.50</b>	<b>50</b>	0	<b>-5,0</b>	+28	<b>+20</b>	+19	+	+10	+2	<b>+4,0</b>	4,0	0	"8	-10	-18
.80	120	0	<b>-5,0</b>	+33	+23	+23	+13	+13	+3	+5,0	-5,0	0	-10	-12	-22
.@	180	0	<b>-6,5</b>	+39	+27	+27	+15	+15	+3	<b>+6,0</b>	-6,0	0	-12	-14	-26
, 180	250	0	-9,0	+45	+31	+31	+17	+18	+4	<b>+7,0</b>	-7,0	0	-6	-15	-29

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			L2/m4		L2/M		L2/l.4		L2/H4		U/«4				
			,	,	,	,	,	,	,	,	,	,			
10	18	0	-4,0	+21	2	+16	+7	+10	+1	+6,5	2,5	+4,0	-5	-2,0	-11
.	18	300	-4,0	+25	+15	{18	+6	+12	+2	+7,0	3,0	+4,0	-6	-3,0	-13
,	30	500	-4,0	+28	+17	+20	+9	+13	{2	+7,5	3,5	{4,0	-7	-5,0	-16
,	50	800	-5,0	+33	+20	+24	,	{15	^2	+9,0	4,0	+5,0	-8	-5,0	-18
,	89	130	-5,0	+38	+23	+28	+13	+18	+3	+10,6	5,0	+5,0	40	-7,0	-22
.	130	180	-6,5	+45	+27	+33	+15	+21	3	{12,0	6,0	+6,5	12	-7,5	-26
.	180	250	-9,0	+54	+31	+40	+17	+27	+4	+16,9	7,0	+9,0	14	-6,0	-29

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18 30	0	-4,0	-12	-21	-5	-14	4*1	-8	+4,5	-4,5	49	0	+16	+7
30 50	0		-13	-24	-5	-16	+2	-9	+5,5	-5,5	+	0	+20	+9
50 80	0	-	-15	-28	-6	-19	+3	-10	+6,5	-6,5	+13	0	+23	+10
,8D 120	0	-5,0	-18	-33	-8	t-23	+2	-13	+7,5	-7,5	+15	0	+27	+12
,120 150	0	-5,0	-21	-39	-9	-27	*1*3	-15	+9,0	-9,0	+18	0	+32	+14
.150 180	0	*6,5	-21	-39	-9	-27	+3	**45	-9,0	-9,0	+18	0	+32	+14
180 250	0	-8,0	-25	-45	-11	-31	+2	-18	+10	-10,0	+20	0	+35	+15
.250 315	0	-10,0	-27	-50	-13	-36	+3	-20	+11,5	-11,5	+23	0	+40	+17
,315 400	0	-12,0	-30	-55	-	-	+3	-22	+12,5	-12,5	+25	0	+43	+18

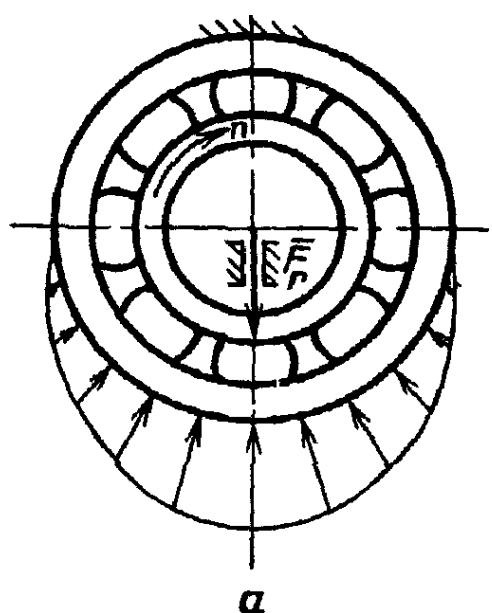
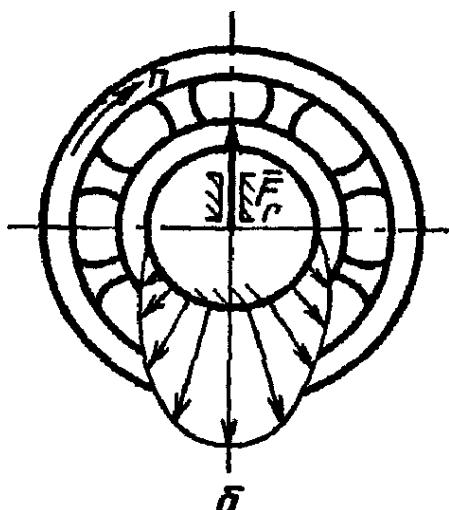


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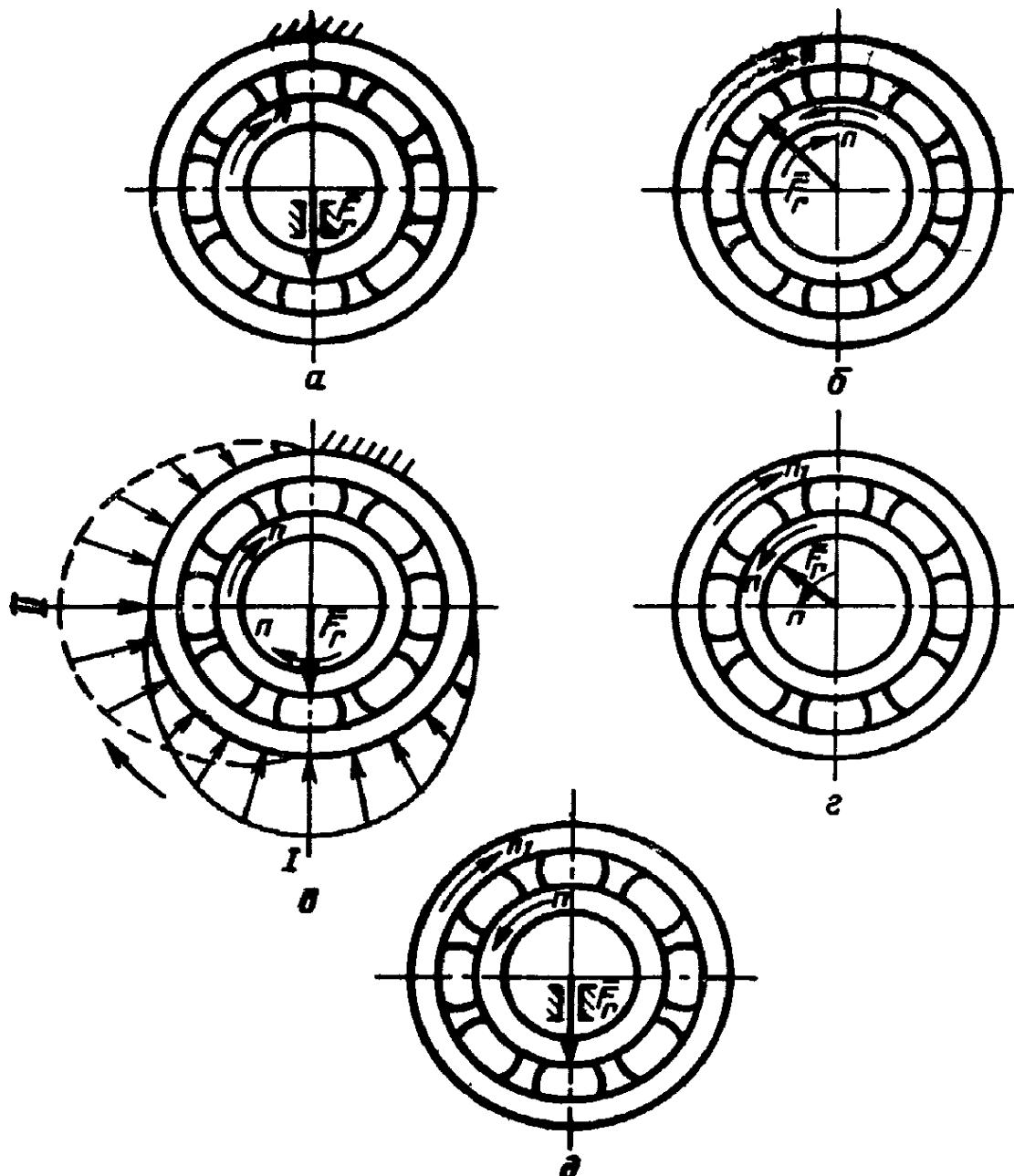
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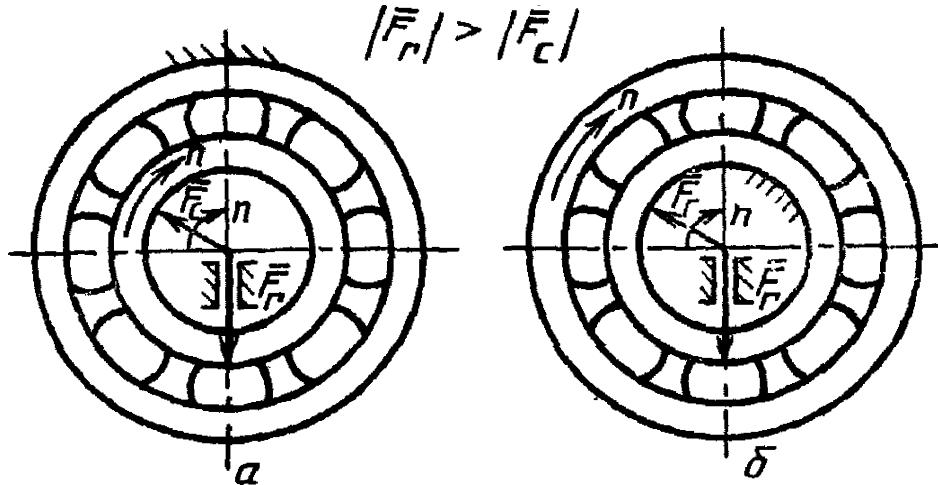
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$$\frac{-F_t}{F_c}$$



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$$F_f + c^* = Fr + 7_c$$

$$, |F_C| < |F_B| =$$

$$|\mathbf{F}_r| + |\mathbf{F}_c| = |\mathbf{F}_r| + |\mathbf{F}_c|$$

$$|F_r| = |F_{cl}|$$

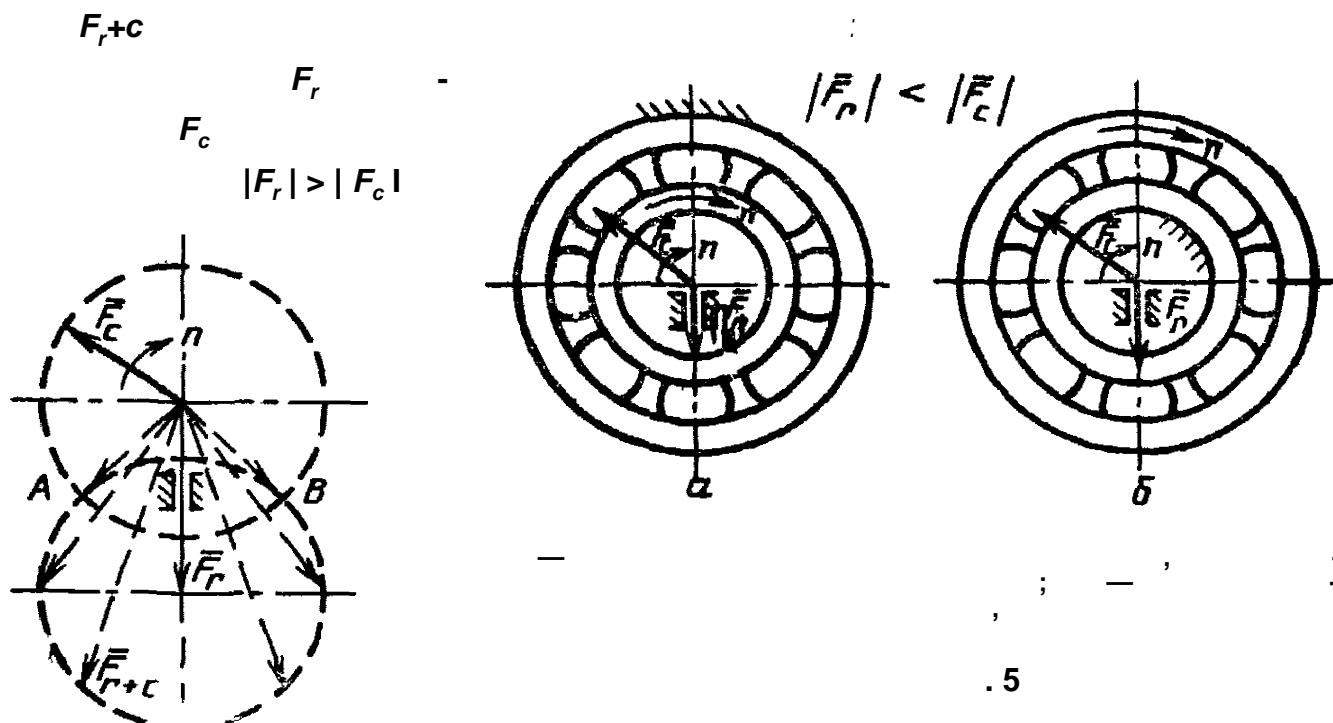
0 2 |FVi.

$\leq jF_{\alpha}1$

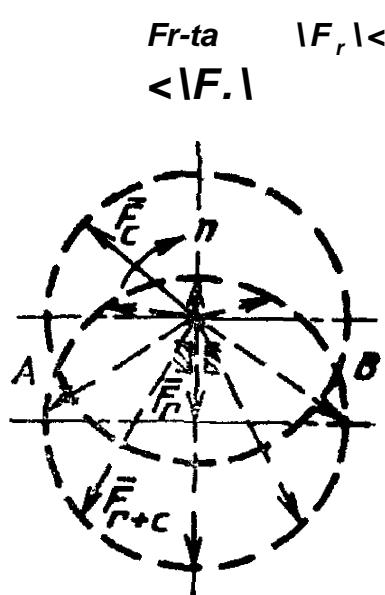
$$(|F_r| + |F_{<j}|) - (|F_c| - |F_r|).$$

$$|F_r| \leq$$

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Черт. 4



. 6

Условия, определяющие выбор посадки		Подшипники с отверстиями диаметром, мм				Примеры машин и подшипниковых узлов	Рекомендуемые посадки		
Вид нагружения внутреннего кольца	Режим работы	радиальные		радиально-упорные					
		шариковые	роликовые	шариковые	роликовые				
	Легкий или нормальный $P \leq 0,07C$					Ролики ленточных транспортеров, конвейеров и подвесных дорог для небольших грузов, барабаны самописцев, опоры волновых передач	$L0/g6; L6/g6$		
Местное (вал не вращается)	Нормальный или тяжелый $0,07C < P \leq 0,15C$	Подшипники всех диаметров				Передние и задние колеса автомобилей и тракторов, колеса вагонеток, самолетов и т. п. Валки мелкосортных прокатных станков	$L0/g6; L6/g6; L0/f7; L6/f7; L0/h6; L6/h6$		
						Блоки грузоподъемных машин, ролики рольгантов, валки станов для прокатки труб, крюковые обоймицы кранов	$L0/h6; L6/h6$		



< 5		250		®				L5/n5; L2/n4; L6/n6; L5/p6		
( )	50 140		-		-				L0/m6; UJ/nfr,	
	110 200		-		-					
	200 *250		*						100 L0/p6; li/p6 L6/16; L0/r7; L6/r7	


				L0/j6;	
				1 L6/jj6	
				D8/k6	
		.200 250		LD/ ;L6/m6	

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) (	/»7 < <0,15	,	, W;



Bn			
	0,07C <		H8/10; H8/16
).	>0,15		H8/10; 8/6; H9/10; H9/16; H6/15;
			G7//0; 07/18; G8/15; G6/14
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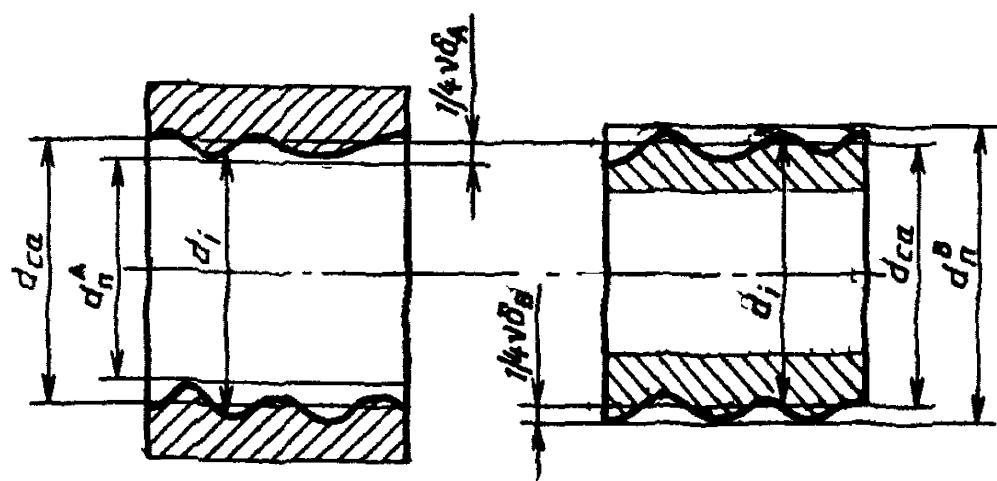
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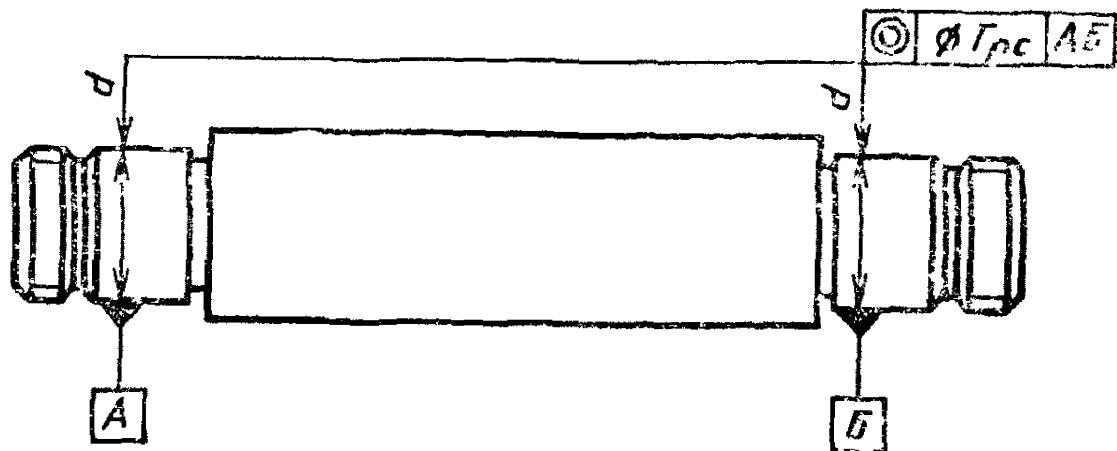
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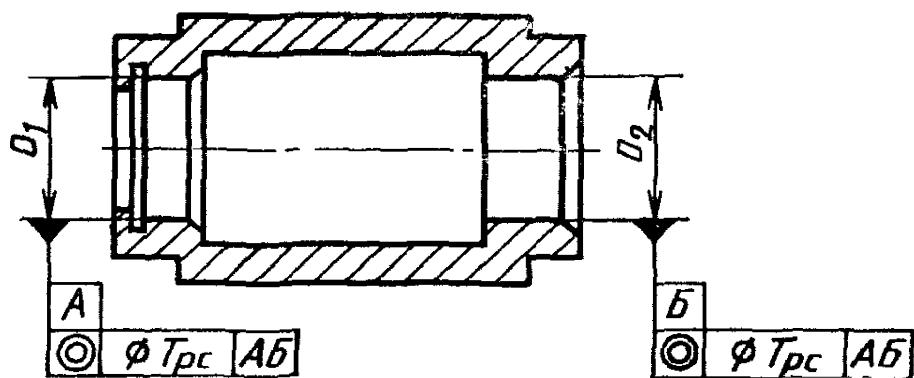
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=26*	5'	W	"	1	3,0	6,0
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4'	2'	40"	1V	2,0		4,0
		10"	20"	0,5		10
5720-75	4°	6	2'		6,0	120
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5721-75	2°	6	2'		6,0	12,0
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