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1 - (96, -)

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4 5147-80

Joint couplings.
Parameters, design and dimensions

2002—01—01

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15150, 45°, 11,2 1120

2

9.301—86

9.303—84

9.306—85

3129—70

4543—71

8908—81

10774—80

15150—69

24643—81

3

3.1 :
1— ;
2— .

1— ;
2— .

5147-97

3.2 : , 1 / , 1.

3.3 , ,

3.4 = 140 • , 1, 3 15150: $d = 20$, 1,

140-1-20- 1- 5147-97

, $d = 22$ 2, 2, $d = 19$ 2 15150: 1,

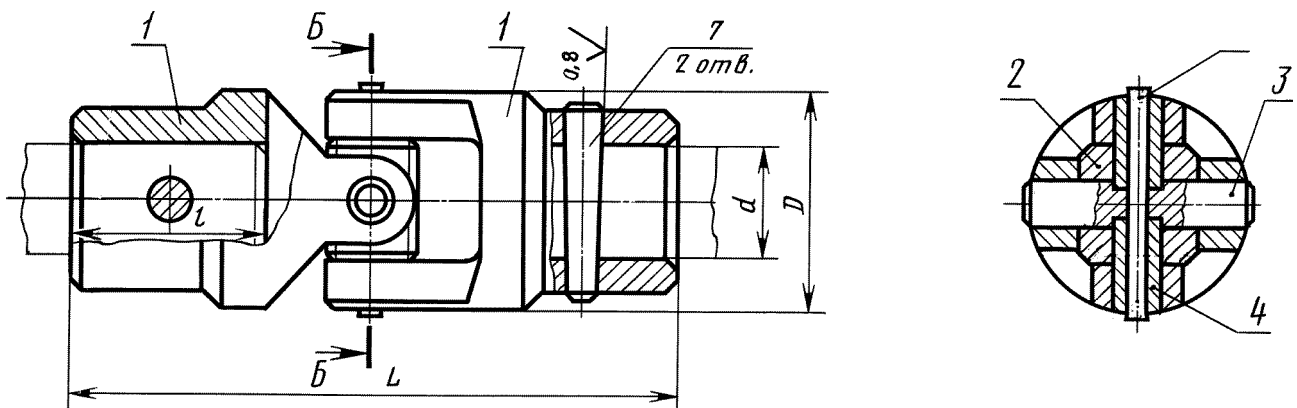
140-2-19-1-22-2- 2 5147-97

3.5 d . d -

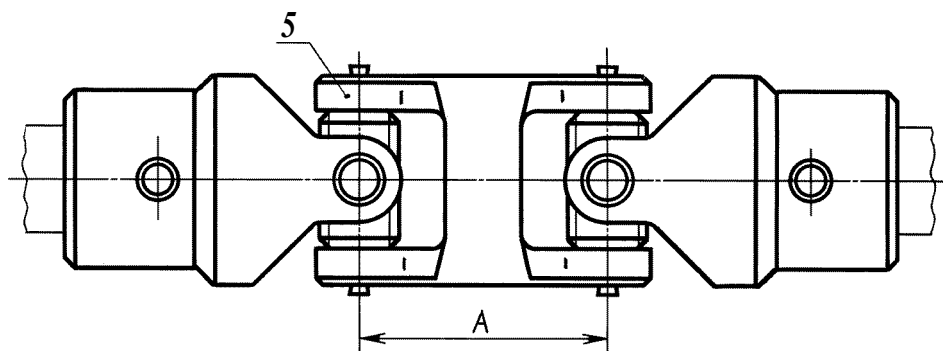
3.6 - 3129, 35 ... 49 HRC₃.

3.7 — 8- 8908.

1



Тип 2



1 — 2 ; 2 — 2, ; 3 — ; 4 — ; 5 — ; 6 — 10774 (1 .) 1 ; 7 — 3129 (2 . ,)

1 —

1

\bullet	d 7 1 (2)	D 4		/	L		$\bullet \cdot 2 \cdot 10^{-6}$		$\cdot \cdot$	
					1	2	1	2	1	2
					1(2)					
11,2	8	16	20	20	56	76	0,22	0,32	0,057	0,080
	9							0,051	0,074	
	10				62 (56)	82 (76)	0,22 (0,20)	0,32 (0,29)	0,058 (0,047)	0,076 (0,070)
22,4	10	20	26	23 (20)	66 (60)	92 (86)	0,63 (0,56)	0,92 (0,87)	0,109 (0,092)	0,147 (0,139)
	11								0,094 (0,080)	0,141 (0,127)
	12				30 (25)	80 (70)			106 (96)	0,102 (0,096)
45,0	12	25	32	30 (25)	86 (76)	118 (108)	1,44 (1,29)	2,09 (1,94)	0,170 (0,152)	0,242 (0,224)
	14								0,150 (0,135)	0,222 (0,207)
71,0	16	32	38	40 (28)	112 (88)	150 (126)	5,90 (4,84)	8,53 (7,46)	0,390 (0,321)	0,558 (0,489)
	18								0,367 (0,299)	0,535 (0,467)
140,0	(19)	40	48	40 (28)	140 (112)	188 (160)	16,3 (12,9)	24,0 (20,6)	0,653 (0,480)	0,973 (0,800)
	20								0,720 (0,590)	1,040 (0,910)
	22			50 (36)					0,667 (0,550)	0,987 (0,870)
280,0	(24)	50	58	50 (36)	148 (120)	206 (178)	45,6 (36,6)	68,8 (59,6)	1,170 (0,960)	1,780 (1,570)
	25			60 (42)	168 (132)	326 (190)			1,280 (1,030)	1,890 (1,640)
	28								1,160 (0,900)	1,770 (1,510)
560,0	30	60	70	80 (58)	222 (178)	292 (248)	148,0 (117,0)	207,0 (176,7)	2,830 (2,310)	3,900 (3,380)
	32								2,710 (2,210)	3,780 (3,280)
	35								2,510 (1,870)	3,580 (2,940)
1120,0	(38)	75	92	80 (58)	236 (192)	328 (284)	396,0 (338,0)	585,0 (525,0)	4,310 (3,630)	6,530 (5,850)
	40			60 (42)	296 (240)	388 (332)			5,030 (4,410)	7,250 (6,630)
	(42)								4,810 (4,050)	7,030 (6,270)

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7 —

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40 4543.

20 40

49 ... 53 HRC₃,

57 ... 63 HRC₃.

0,4—0,8

9.303 9.306.

— 0,02

d_x — 0,02 ;

10- 24643.

: 14, 4, 1 14/2.

1,

$d = 20$,

140 • ,

3 15150:

140-20-1- 5147-97

140- 5147-97

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140- 5147-97

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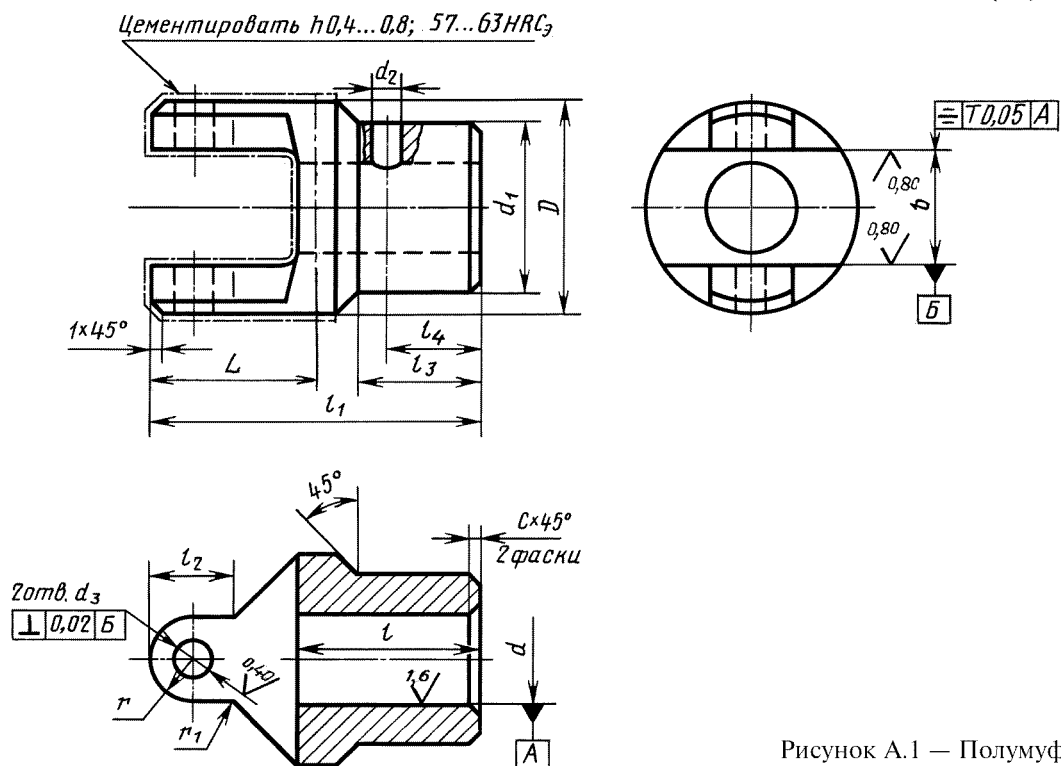
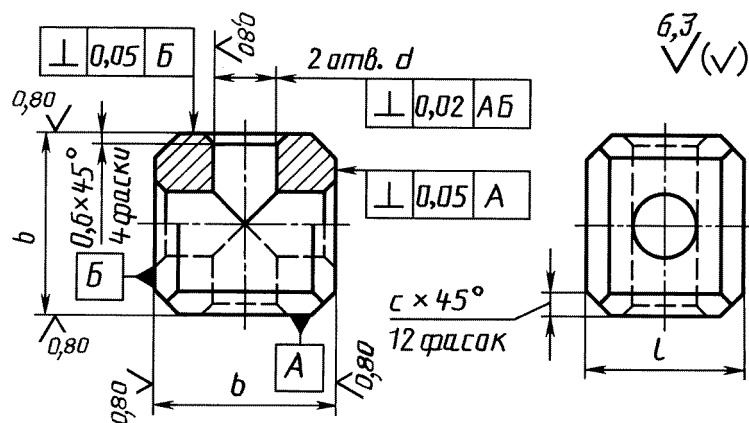
 $6,3 \sqrt{(\checkmark)}$ 

Рисунок А.1 — Полумуфта

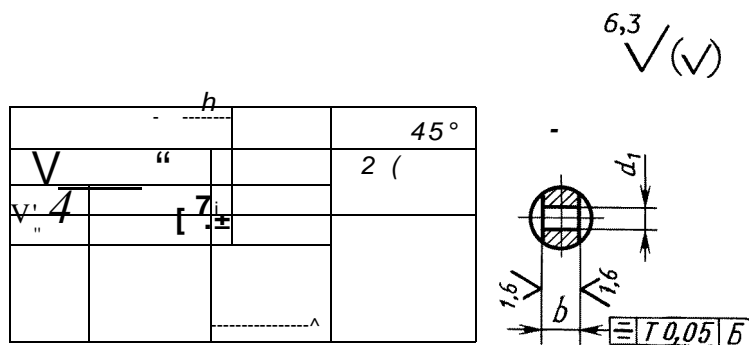
№	$\frac{l}{7}$ 1(2)	d_1	d_2	d_3 F8	D	b H7	$\frac{1}{2}$	A	h	h	k	r	n	C	$\sigma_{ср}$ 1(2)	
							1(2)			1(2)					$\sigma_{ср}$ 1(2)	
11,2	8	15	3	4	16	10	20	32	8	15	12	4	0,6	0,6	0,025	
	9						23 (20)	35 (32)	10	18 (15)	15 (12)				0,022	
	10														0,023 (0,020)	
22,4	10	18	4	5	20	12	38 (35)	10	18 (15)	15 (12)	5	1,0	1,0		0,044 (0,040)	
	11														0,041 (0,037)	
	12						30 (25)	45 (40)	12	25 (20)					21 (16)	0,045 (0,042)
45,0	12	21	5	6	25	14	30 (25)	49 (44)	12	22 (17)	18 (13)			6	1,0	0,079 (0,070)
	14															0,069 (0,061)
71,0	16	28	6	7	32	18	40 (28)	63 (51)	14	30 (18)	25 (12)			7		1,6
	18											0,162 (0,128)				
140,0	(19)	34	8	8	40	22	40 (28)	68 (56)	16	28 (16)	22 (10)	8	2,0	1,6		0,286 (0,227)
	20						50 (36)	78 (64)		38 (24)	32 (18)					0,323 (0,258)
	22														0,297 (0,239)	
280,0	(24)	42	10	10	50	28	50 (36)	84 (70)	19	34 (20)	26 (12)	10	2,5		0,506 (0,403)	
	25						60 (42)	94 (75)		44 (26)	36 (18)				0,561 (0,435)	
	28														0,502 (0,393)	
560,0	30	53	12	13	60	34	80 (58)	124 (102)	28	64 (42)	50 (28)	13	3,0		1,260 (1,000)	
	32														1,200 (0,950)	
	35															1,100 (0,880)
1120,0	(38)	63	16	16	75	42	(82)	134 (112)	35	60 (38)	45 (23)	16			1,860 (1,520)	
	40							164 (136)		90 (62)	75 (46)				2,220 (1,910)	
	(42)						2,110 (1,730)									



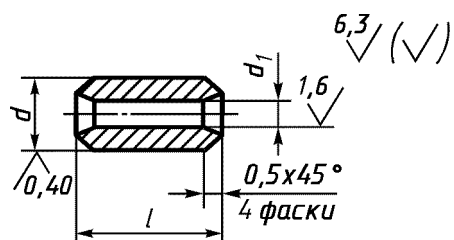
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\bullet	h6	1 hi 1	d 7		
11,2	10	8	4	1	0,004
22,4	12	10	5		0,007
45,0	14	12	6		0,012
71,0	18	15	7		0,027
140,0	22	19	8	3	0,054
280,0	28	24	10		0,108
560,0	34	30	13		0,202
1120,0	42	38	16		0,380



$\frac{7}{\bullet}$,	d	$d \setminus$	$/$, ,
11,2	4	2,0	16	4	2	0,6	0,0014
22,4	5	2,5	20	5	3		0,0028
45,0	6	3,0	25	6	4		0,0050
71,0	7	4,0	32	7	5		0,0090
140,0	8	5,0	40	8	6		0,0140
280,0	10	6,0	50	10	7	1,0	0,0280
560,0	13	8,0	60	13	9		0,0590
1120,0	16	10,0	75	16	10		0,1130



.4 —

.4

	d	d_1	/	
11,2	4	2,0	7,0	0,0005
22,4	5	2,5	8,5	0,0010
45,0	6	3,0	10,5	0,0016
71,0	7	4,0	13,5	0,0032
140,0	8	5,0	17,0	0,0050
280,0	10	6,0	21,5	0,0100
560,0	13	8,0	25,5	0,0220
1120,0	16	10,0	32,5	0,0430

6,3 (✓)

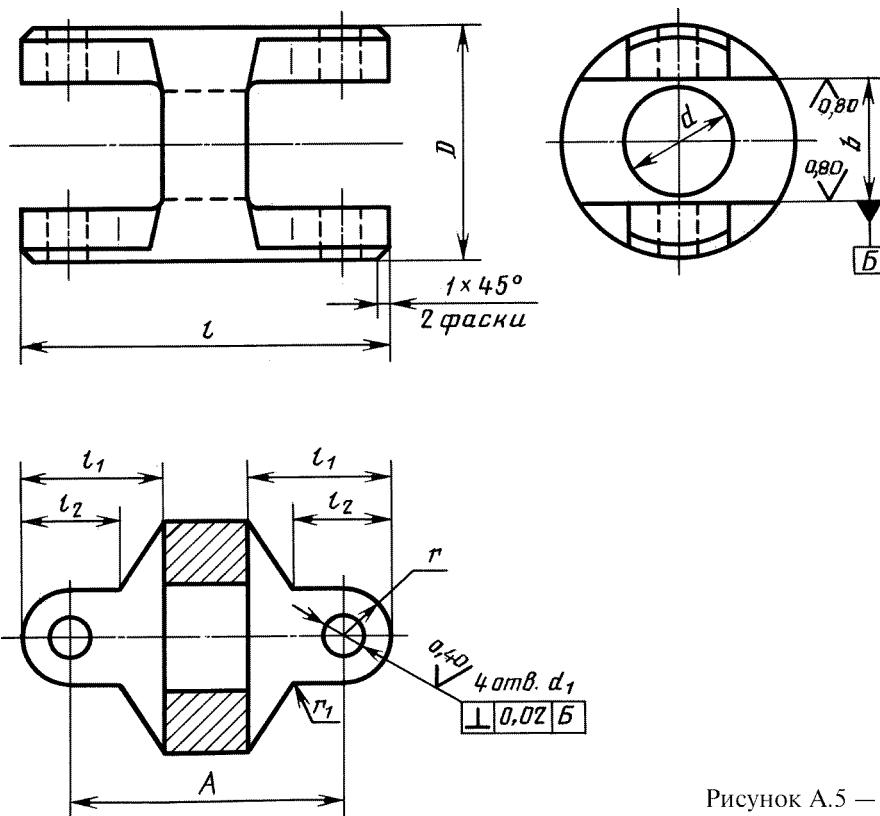


Рисунок А.5 — Вилка спаренная

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σ	$(l$	D	$/$		7	d F8	$>l$	h			$'$
11,2	8	16	28	20	10	4	12	8	4	0,6	0,016
22,4	10	20	36	26	12	5	15	10	5	1,0	0,035
45,0	12	25	44	32	14	6	19	12	6	1,0	0,060
71,0	16	32	52	38	18	7	32	14	7	1,6	0,125
140,0	20	40	64	48	22	8	28	16	8	2,0	0,239
280,0	25	50	78	58	28	10	34	19	10	2,5	0,456
560,0	32	60	96	70	34	13	44	28	13	3,0	0,767
1120,0	40	75	124	92	42	16	54	35	16	3,0	1,630

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• ,	. 6 10774	. 7 3129
11,2	2 20	16
22,4	2,5 25	4 20
45,0	30	5 25
71,0	4 36	6 30
140,0	5x4 5	8 36
280,0	6 55	10 45
560,0	8 65	12 55
1120,0	10 80	16 65

5147-97

621.825.6 : 006.354

21.120.20

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41 7150

1. The first step is to identify the problem. This involves understanding the situation, gathering information, and defining the problem clearly.

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06.08.2001.

21.09.2001.

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563 . 2053. . 870.

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http://www.standards.ru e-mail: info@standards.ru

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