



880—75

880—75

1986

880.75**

Articles made of metal-ceramic hard alloys for mining
tools. Shapes and dimensions

880—67

19 6500

9 1975 , 1744**01.07.76****1985 .**

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11



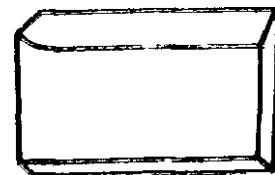
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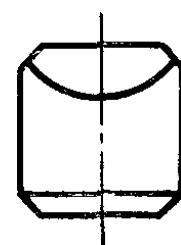
(1986 .)
19791, 2,
1985 . (6—79, 4—86).

.2

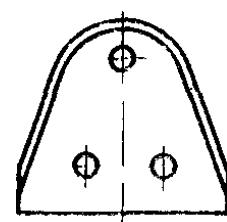
880—75

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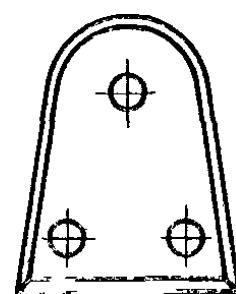
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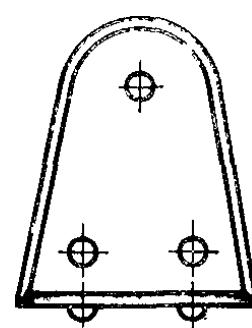
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24



24



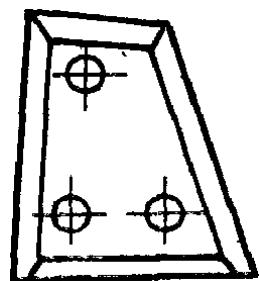
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	-		(]	
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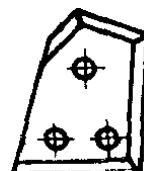
880—75

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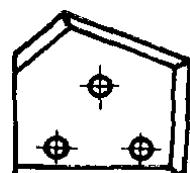
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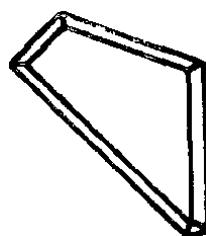
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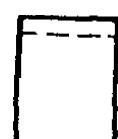


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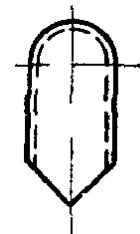
51



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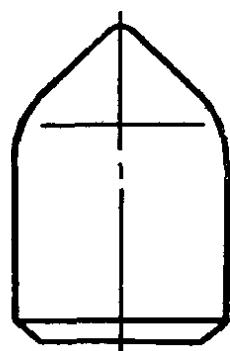
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63	- -	.^
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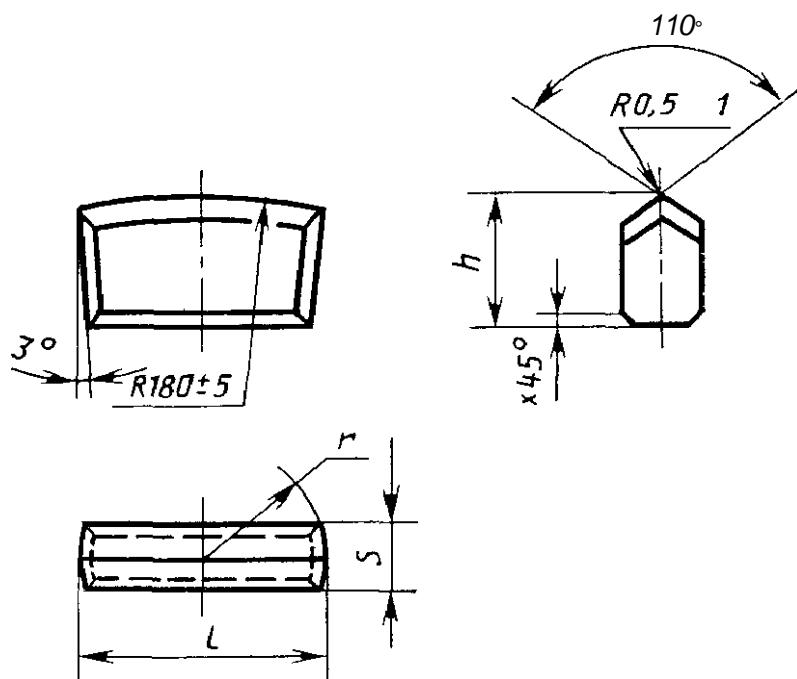
67



2.

* 1—35

. 2—20.



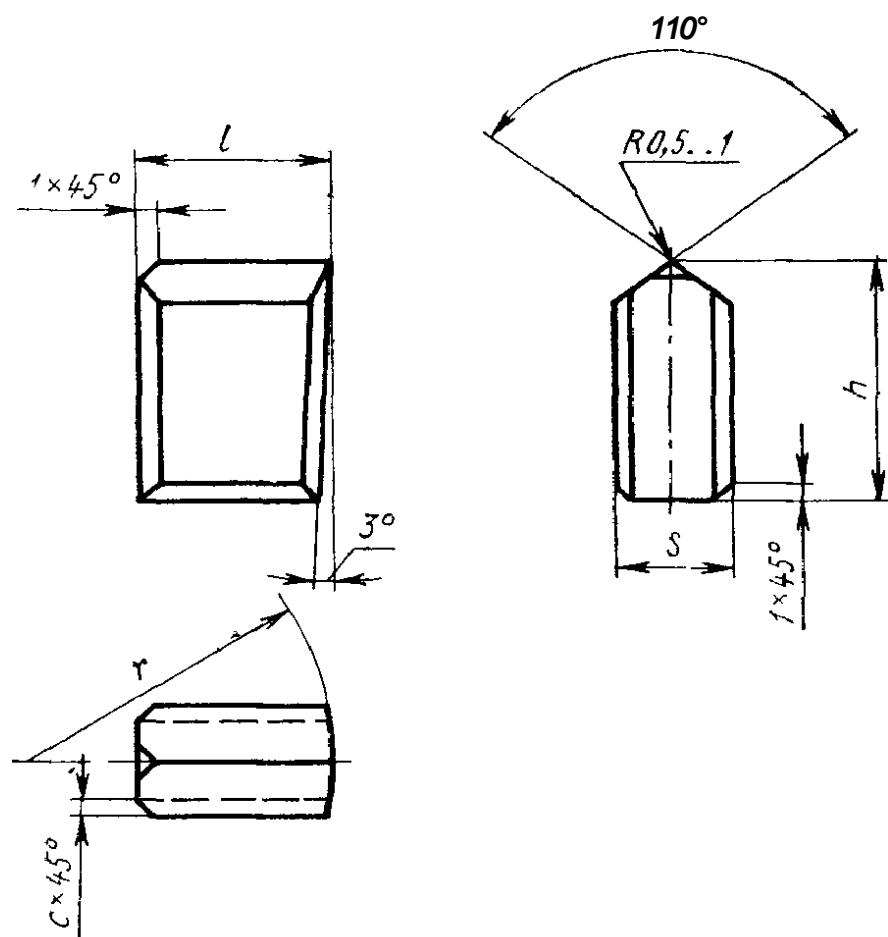
Черт.

2

	(+ 1) .	(- 0,8) .	(+ 0,5) .	(db 1,0) .
1101	28			14,0
1102	32		7,5	16,0
1103				18,0
1104	36		9,5	
1105			7,5	
1106	40			20,0
1107	43			21,5
1108	46	16	9,5	23,0
1109	52			26,0
1110	49			24,5

$$R=120\pm 5$$

12



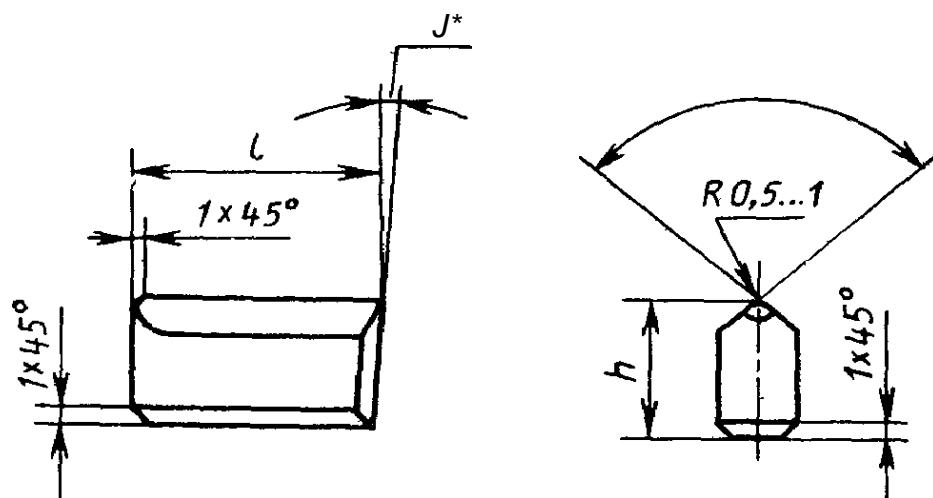
Черт. 2

3

	(t $\pm 0,5$)	(h $-0,8$)	(s $+0,5$)	($\pm 1,0$)	($\pm 0,5$)
1201	12		7,5	16	
1202	13		9,5	20	
1203	14		7,5	18	
1204		15		21	1,0
1205				20	
1206	16		9,5		
1207	17	18	7,5	21	1,5
1208	18		9,5	18	1,0
1209	12	16			

 45°

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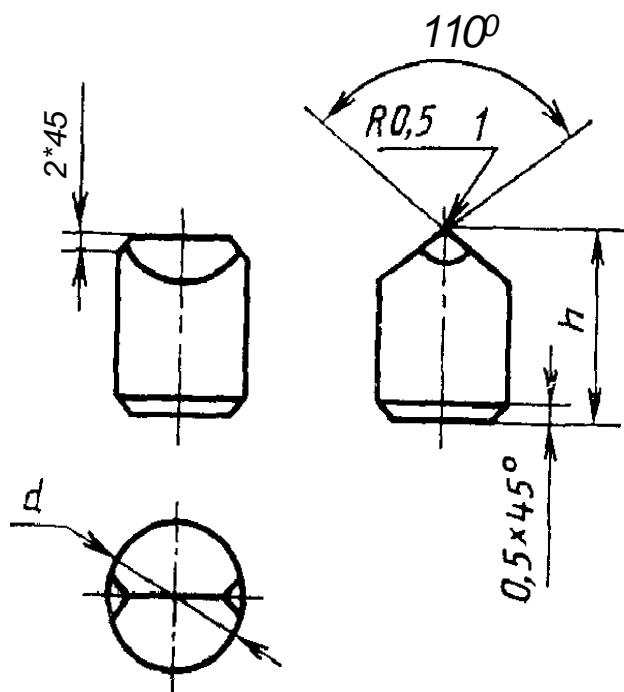
Черт. 3

4

ММ

	(1 $\pm 0,5$)	(—0,8)	(s $+ 0,5$)'	R^*	($\pm 1,0$)
1301	28				52
1302	32				
1303	49		9,5	5	78
1304	36				
1305	40				64
1306	14				
1307	16				
1308	16		11,5	6	30
1309	20				
1310	24				
1311	23				
1312	37		24	13,5	7
					62

14



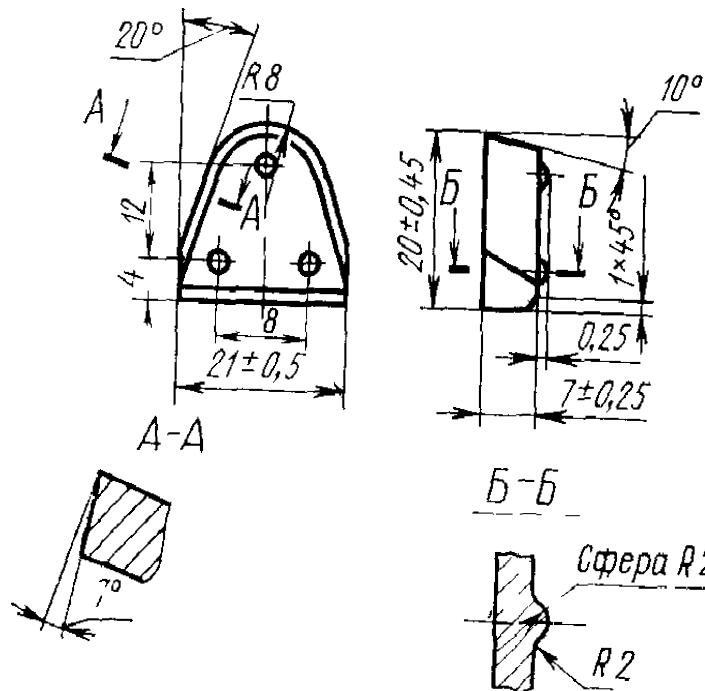
Черт. 4

5

	<i>d</i>	<i>h</i> ($\pm 0,4$)
1401	8	-0,35
1402	10	-0,45
1403	12	
1404	14	
1405	15	
1406	16	
1407		-0,60
1408	17	
1409	18	
1410	20	

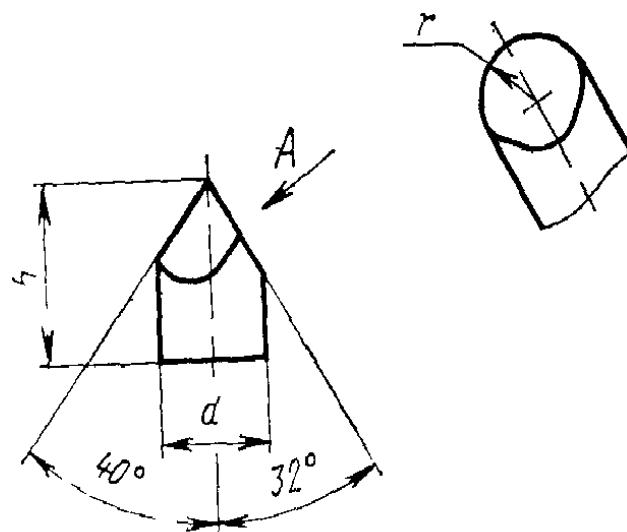
(2).

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. 6 (. 5).

23



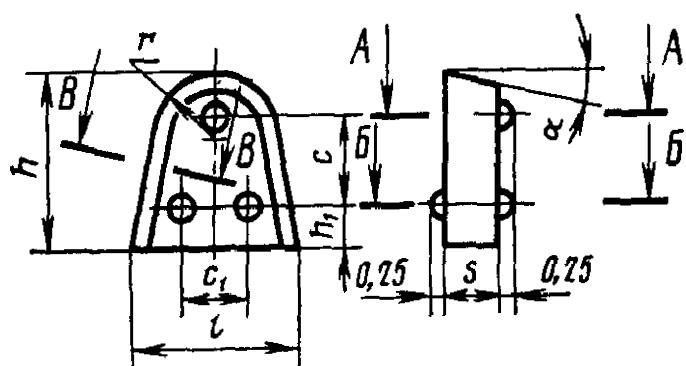
Черт. 7

6

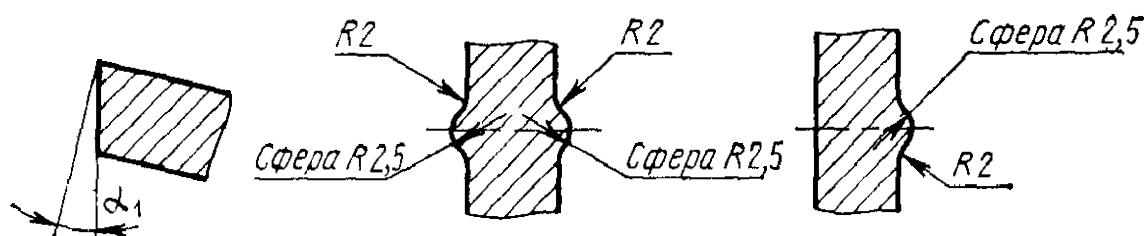
	<i>d</i>		<i>h</i>		$(\pm 0,25)$
	.	,	.	,	
2301	8,2		14		4,5
2302			12		$\pm 0,35$
2303*	10,0		16		5,5
2307	12,2		20	$\pm 0,40$	6,5

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24



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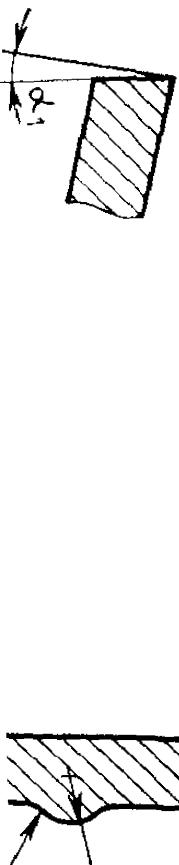
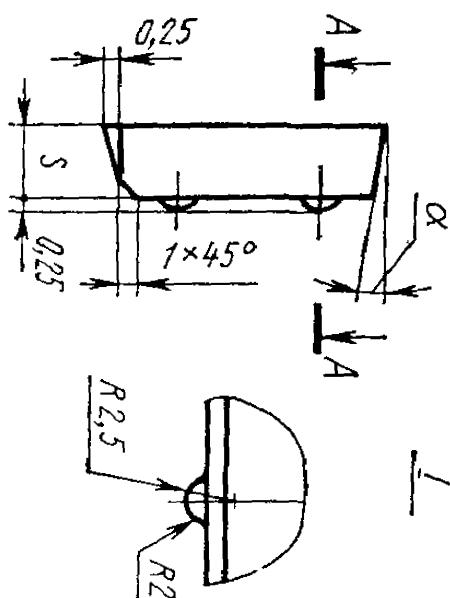
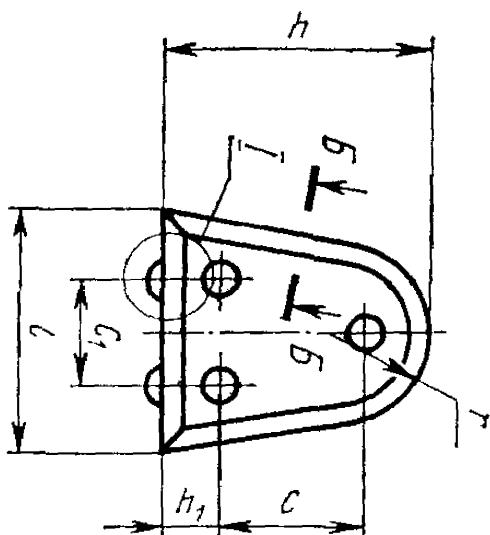


Черт. 8

7

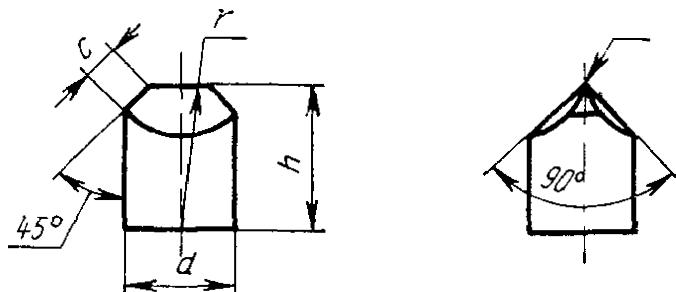
	h		1		S					C_i		a_t
2401	15	$\pm 0,4$	12	$\pm 0,35$	4,0	$\pm 0,20$		4,5	2,5	8,0	6,5	10°
2402					5,5	$\pm 0,25$						
2403	21	$\pm 0,5$	18	$\pm 0,45$	7,0	$\pm 0,25$	5,5	4,0	11,5	8,0	15°	4Q

to 4* &J	n to 4*. S3	•"1 to 4^ ta	n to 4-		
03		CO			
K> si		to to	05	.	S*
	1+		1+ 4».	.	
20		05		.	
-		±0,40	-	.	
05		-4	4^	.	
-			1+ N0	.	
-4			4*	*	
4^				S'	
," "4 !			-		
," "			05		
*—			*—		
4»	1	0		fi	∞



$R_{2,5}$

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Черт. 10

9

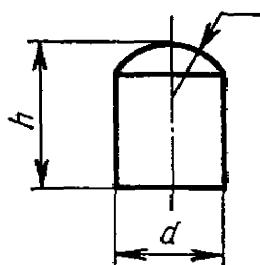
ММ

	<i>d</i>	<i>h</i>					
	.	:		:		:	

<u>2501</u>	<u>3,2</u>		<u>$\pm 0,20$</u>				
<u>2502</u>			<u>$\pm 0,25$</u>	<u>8</u>			
<u>2503</u>	<u>4,2</u>		<u>$\pm 0,20$</u>				
<u>2504</u>							
<u>2505</u>	<u>5,2</u>	<u>8</u>		<u>10</u>			
<u>2506</u>							
<u>2507</u>		<u>10</u>	<u>$\pm 0,25$</u>				
<u>2508</u>	<u>6,2</u>			<u>12</u>			
<u>2509</u>		<u>8</u>					
<u>2510</u>		<u>12</u>					
<u>2511</u>	<u>7,2</u>	<u>10</u>		<u>14</u>	<u>$\pm 0,15$</u>	<u>0,5</u>	<u>0,5</u>
<u>2512</u>		<u>13</u>	<u>$\pm 0,30$</u>				
<u>2513</u>		<u>12</u>					
<u>2514</u>	<u>8,2</u>	<u>21</u>		<u>16</u>			
<u>2515</u>		<u>10</u>					
<u>2516</u>		<u>21</u>					
<u>2517</u>		<u>13</u>	<u>$\pm 0,25$</u>				
<u>2518</u>	<u>9,2</u>	<u>21</u>		<u>18</u>			
<u>2519</u>		<u>—</u>					
<u>2520</u>		<u>16</u>					
<u>2521</u>		<u>21</u>					
<u>2522</u>	<u>10,2</u>	<u>21</u>	<u>$\pm 0,30$</u>	<u>20</u>	<u>$\pm 0,20$</u>	<u>1,0</u>	<u>1,0</u>
<u>2523</u>		<u>13</u>					
<u>2524</u>		<u>12</u>					

	<i>d</i>		<i>h</i>				
	
2525			16				
2526			15				
2527			14				
2528	11,2		13	—f— 0,30	22		
2529			12				
2530			11				
2531			10				
2532		0,3	18				
2533			17	±0,40			
2534	12,3		16			24	
2535			15	±0,30			
2536			14				
2537			19	±0,40			
2538			18				
2539	13,3		17			26	
2540			16	—0,30			
2541			15				±0,20
2542			21	±0,40			
2543			20				
2544	14,3		18			28	
2545			17				
2546			16				
2547			22				
2548			21				
2549	15,3	+ 0,4	20			30	
2550			19	-4-0,30			
2551			18				
2552			24				
2553			22				
2554	16,3		20			32	
2555			19				
2556			18				

26

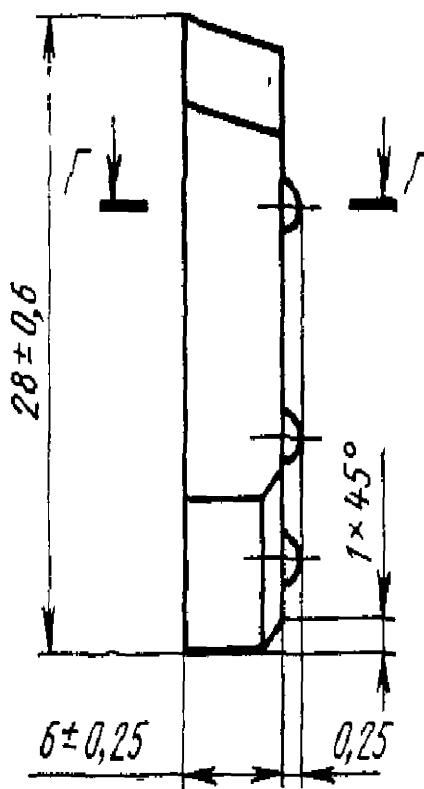
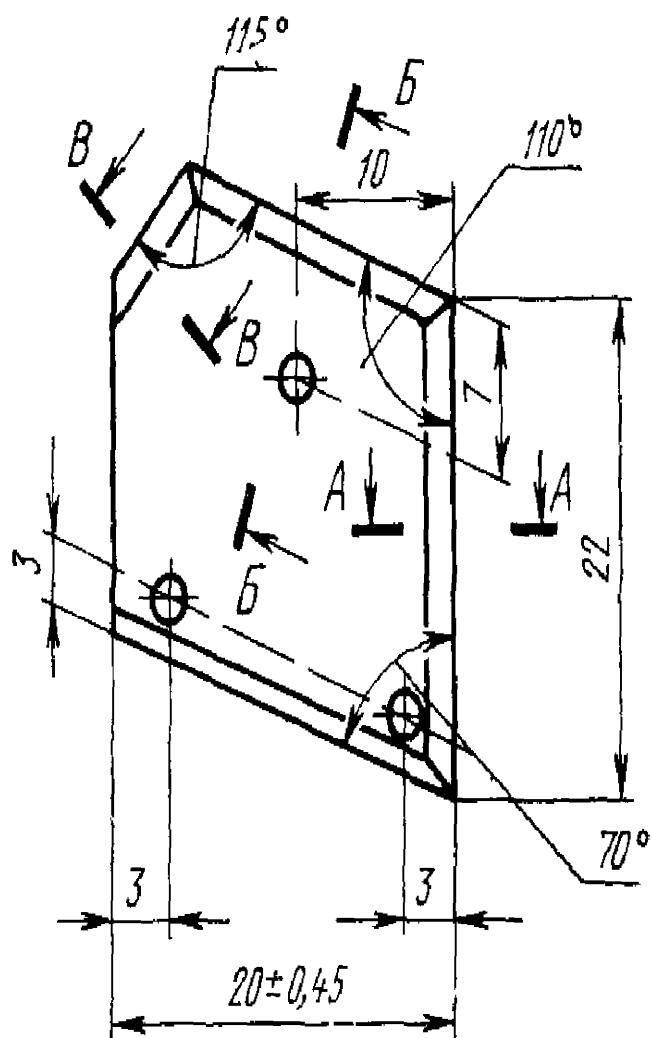
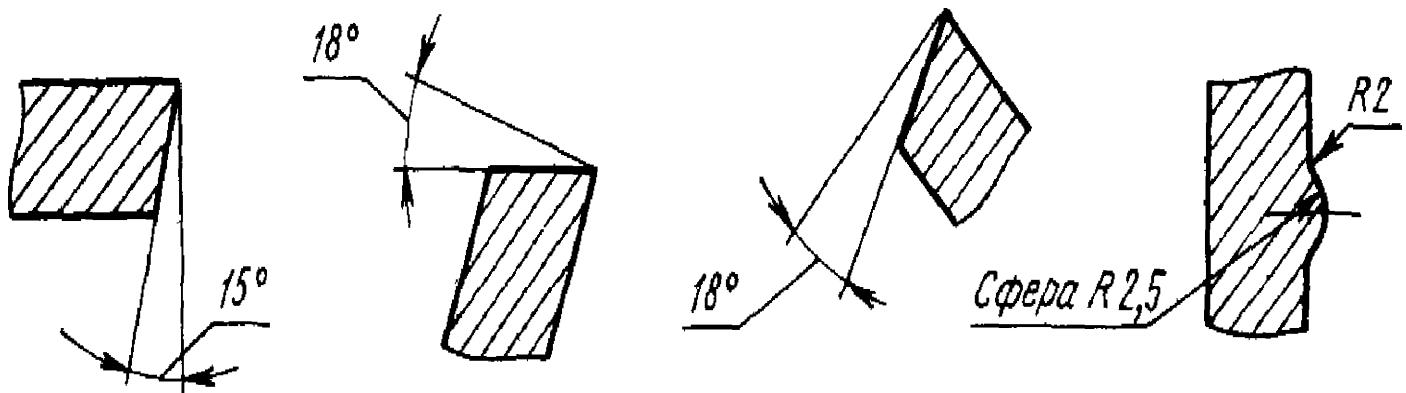


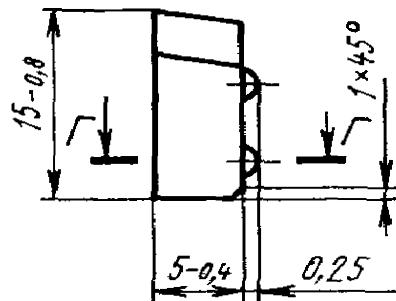
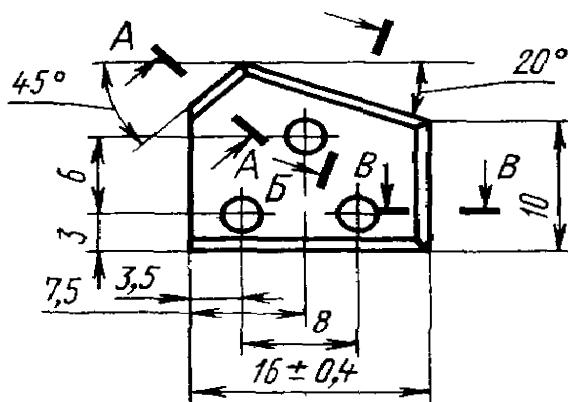
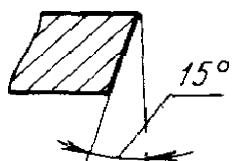
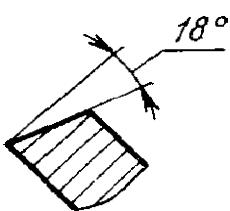
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	d			h			X		d			h			
2601	3,2			5		1,8			2620			10			
2602		4,2		6	+ 0,20		2,3		-2621			9			$\pm 0,20$
2603			5						2622			8			
2604		5,2	8		$\pm 0,25$				2623			7			
2605			7						2624			14			
2606		6,2	6	$\pm 0,20$					2625			13			$+0,30$
2607			9						2626			12			
2608			8	$\pm 0,25$		3,4		$\pm 0,20$	2627			11			5,0
2609			7						2628			10			
2610			6	$\pm 0,20$					2629			9			$+0,25$
2611			11	$\pm 0,30$					2630			8			
2612			10						2631			16			$\pm 0,25$
2613		7,2	9						2632			15			
2614			8	$\pm 0,25$		3,9			2633			14			$\pm 0,30$
2615			7						2634			13			
2616				$+ 0,20$					2635			12			
2617			13						2636			—			
2618	8,2		12	$\pm 0,30$		4,5			2637			10			$\pm 0,25$
2619			11						2638			9			

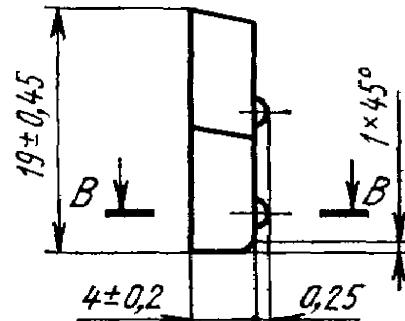
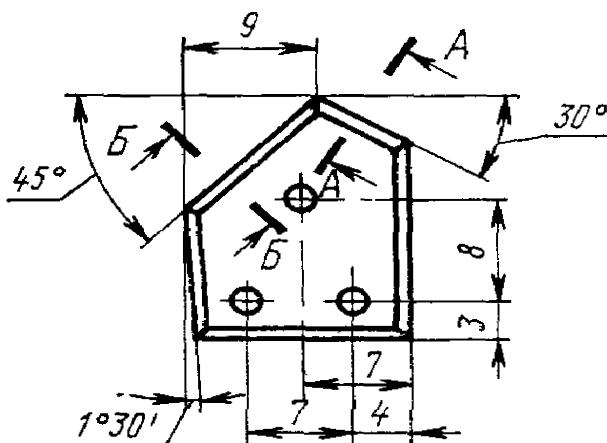
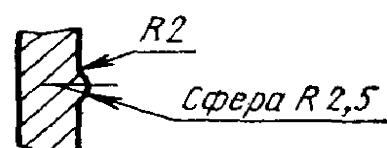
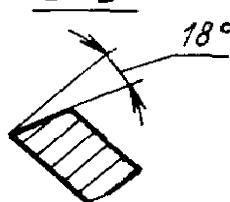
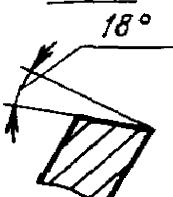
	<i>d</i>		<i>h</i>				<i>d</i>		<i>h</i>		$\frac{4}{\text{£}} \frac{*}{\text{£}} \frac{4}{\text{£}}$
	.	.	x	2	X	
2639			16				2662		21		
2640			15				2663		20		
2641			14				2664		18		
2642	11,2		13				2665		17		
2643			12				2666		16		
2644			11				2667		15		
2645			10	$\pm 0,25$			2668		14		
2646			18				2669		13		
2647			17				2670		22		
2648			16				2671		21		
2649		4-0,3	15				2672		20		
2650		12,3	14				2673		19		
2651			13				2674		18		
2652			12	$\pm 0,30$			2675		17		
2653			11				2676		16		
2654			19				2677		15		
2655			18				2678		24		
2656			17				2679		22		
2657			16				2680		20		
2658		13,3	15				2681		19		
2659			14				2682		18		
2660			13	$\pm 0,40$			2683		17		
2661			12				2684		16		

A-AB-BB-BF-F

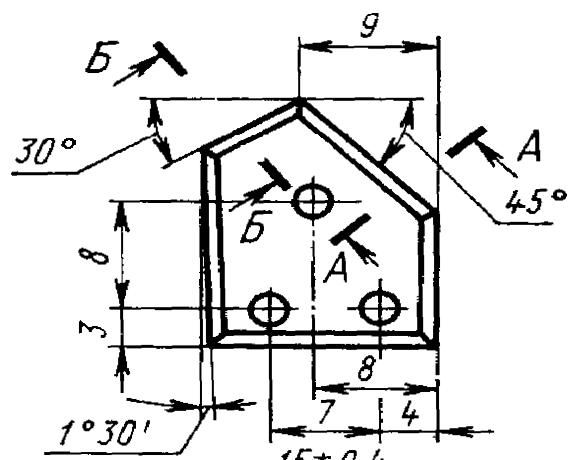
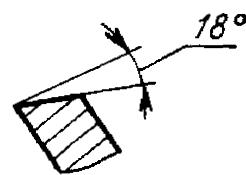
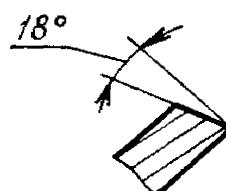
*A-A**B-B**B-B**G-G*

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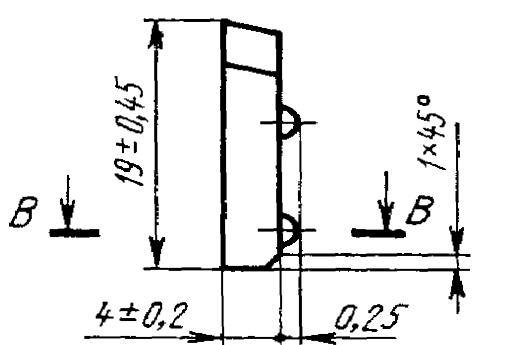
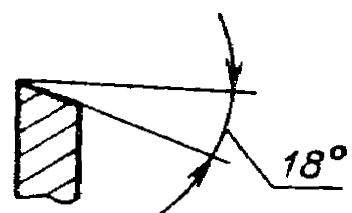
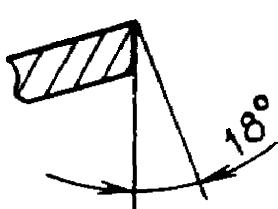
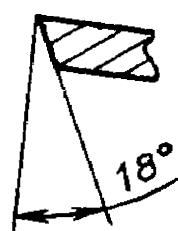
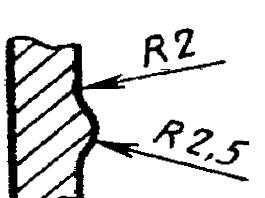
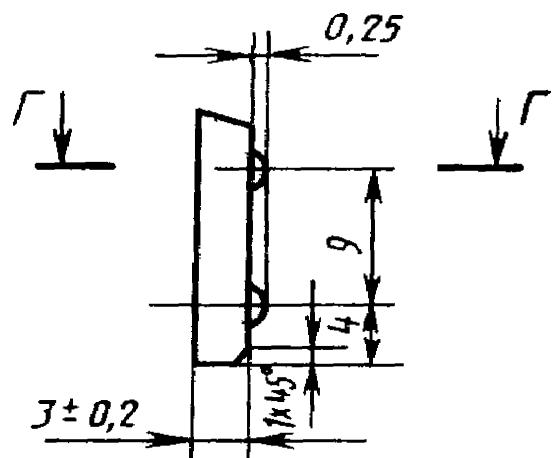
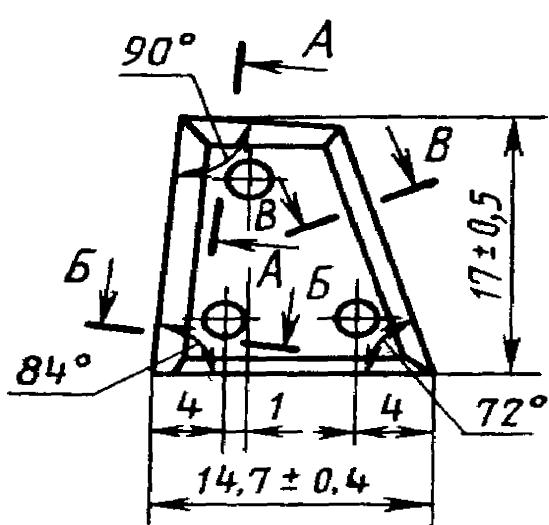
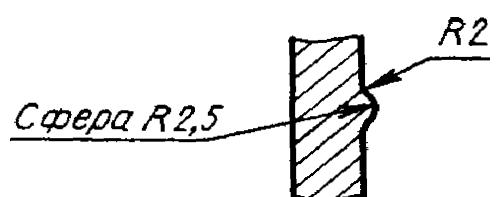
34

*A-A**B-B**B-B*

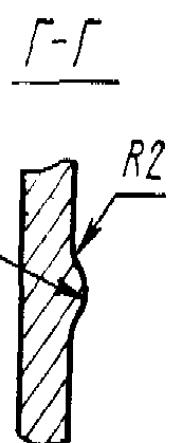
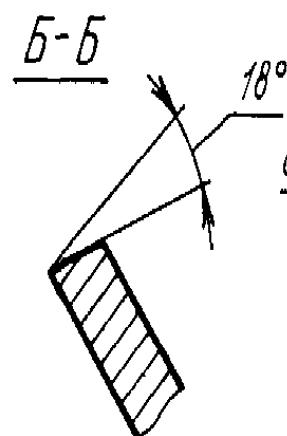
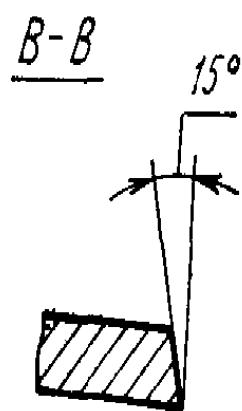
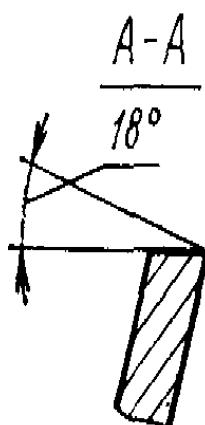
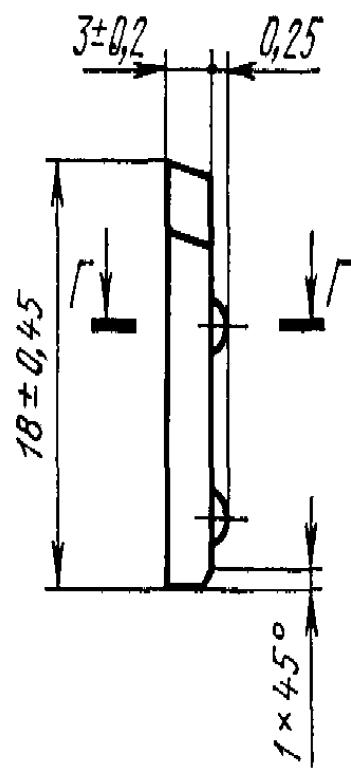
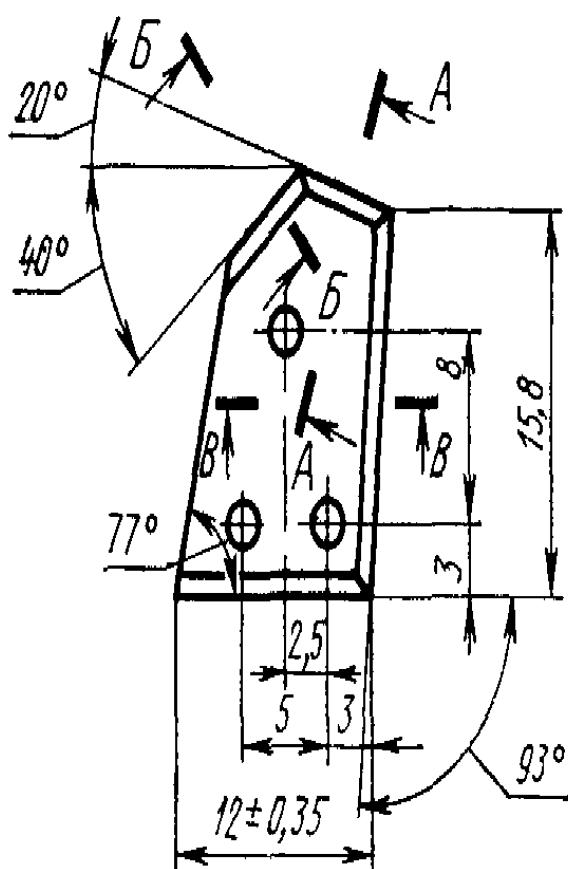
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*A-A**B-B*

Черт. 15
Форма Г36

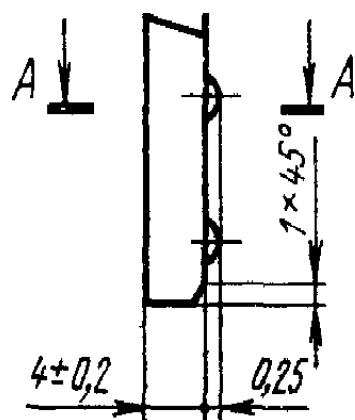
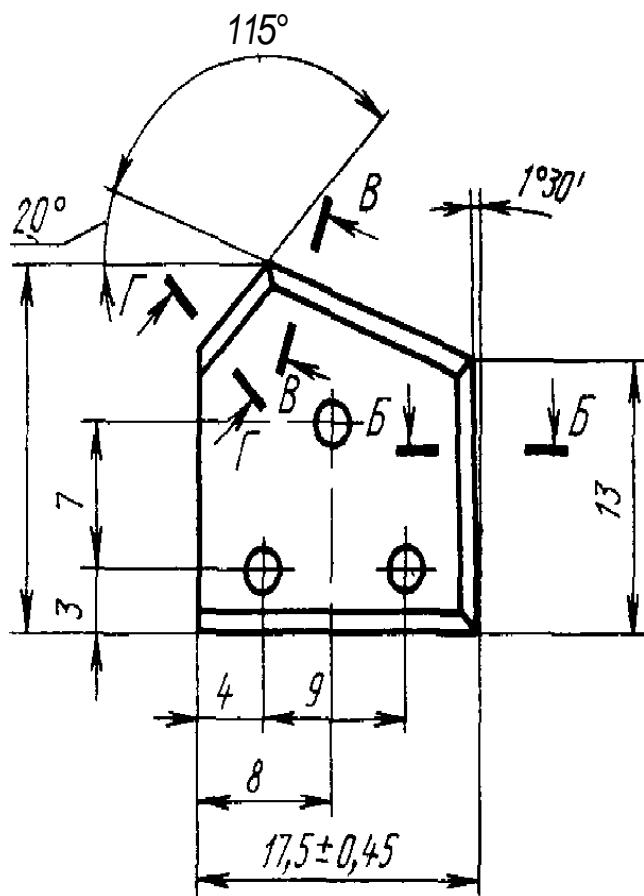
*B-B*

37

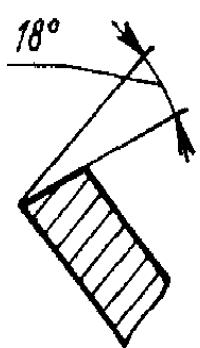
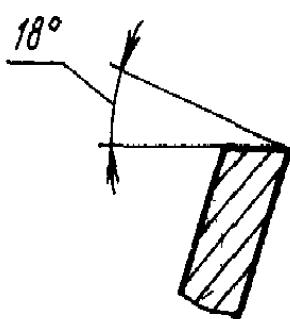
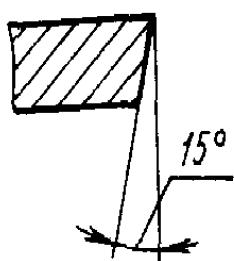
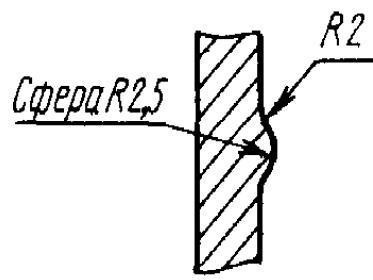


.17

38

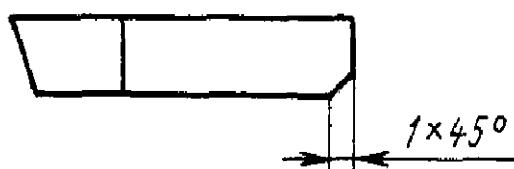
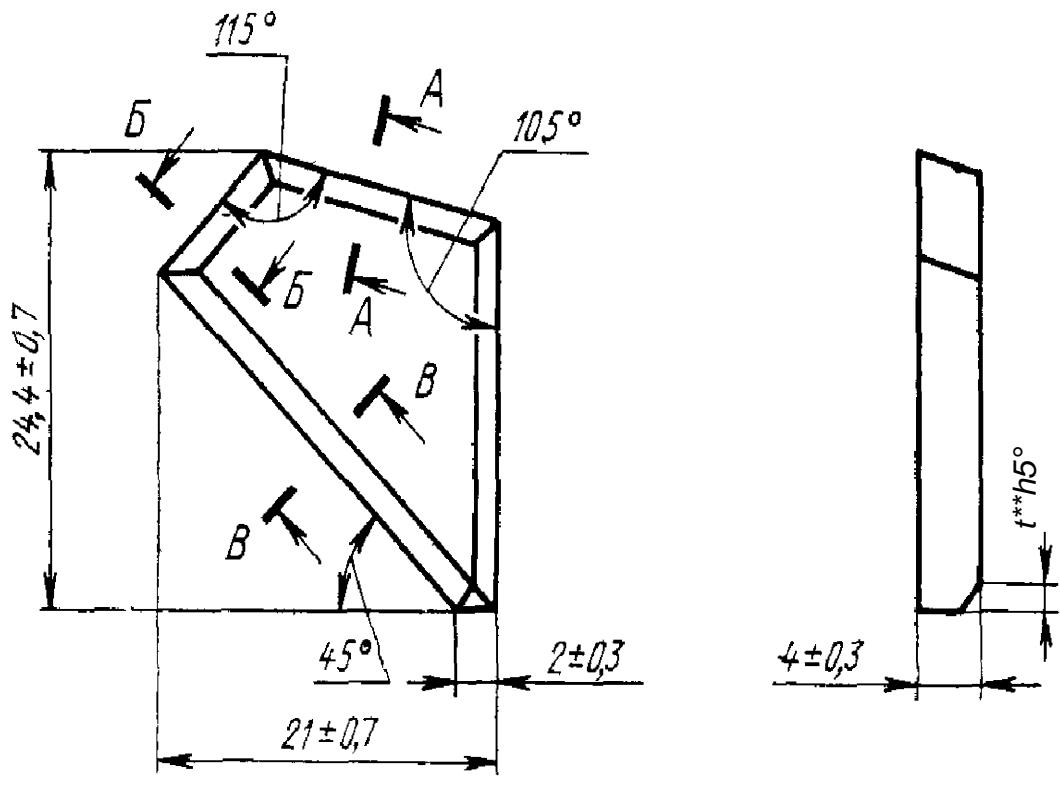
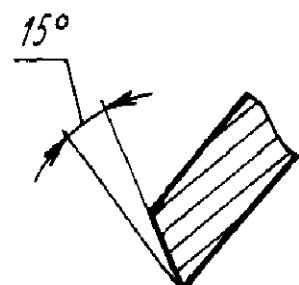
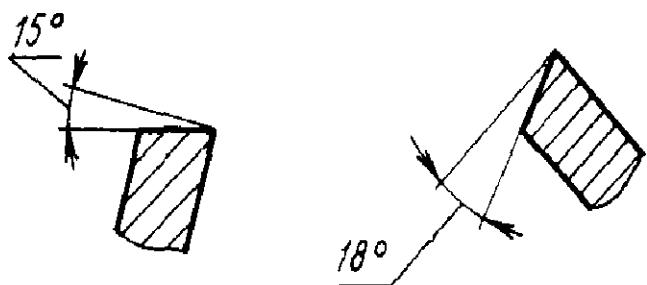


5-5



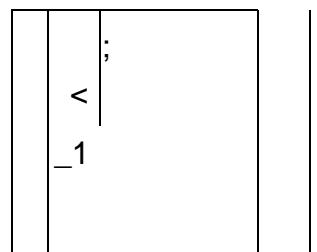
.18

40

A - AB - BB - B

Черт 20*

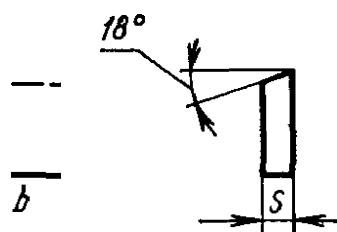
*. 19



			k		£	

4101	3,0	$\pm 0,20$	15	$\pm 0,40$	1,5	$\pm 0,15$
4102	6,0	$\pm 0,25$	20	$\pm 0,45$	4,0	$\pm 0,20$
4103	8,0				6,0	$\pm 0,25$
4104	7,5	$\pm 0,20$	15	$\pm 0,25$	0,7	
4105	8,5					
4106	9,5					

51



. 22

12

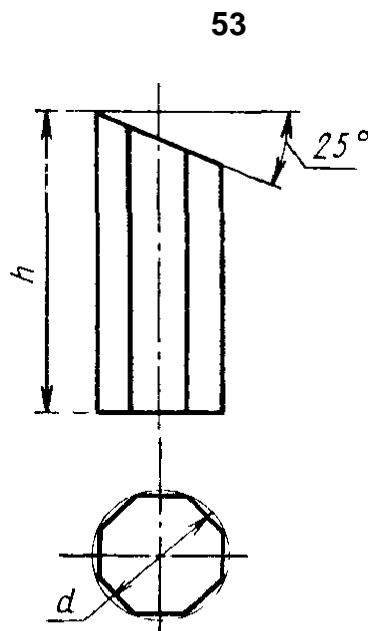
			<i>h</i>		<i>S</i> (±0,2)
			.	.	
5101	5,0	— 0,20	7	±0,25	
5102	7,5	±0,25	10	±0,30	
5103	8,5	±0,30	8	±0,25	3
5 4			10	-+•0,30	
5105	10,0		14	±0,40	
5106	1,5	±0,10	12	±0,35	3
5107	4,0	±0,20	10	±0,30	4
5108	3,0		8	±0,25	
5109	2,5	±0,15	12	±0,35	3
5110	2,0				
5111	3,0		20	±0,50	4

1X45°

25°.

5110

5111—



13

	d ($\pm 0,2$)	h	
5301	5	5	$\pm 0,20$
5302		8	$\pm 0,25$
5303		10	$\pm 0,30$
5304		15	
5305	7	20	$\pm 0,40$

5301— 5303

25°*

Черт. 23

54



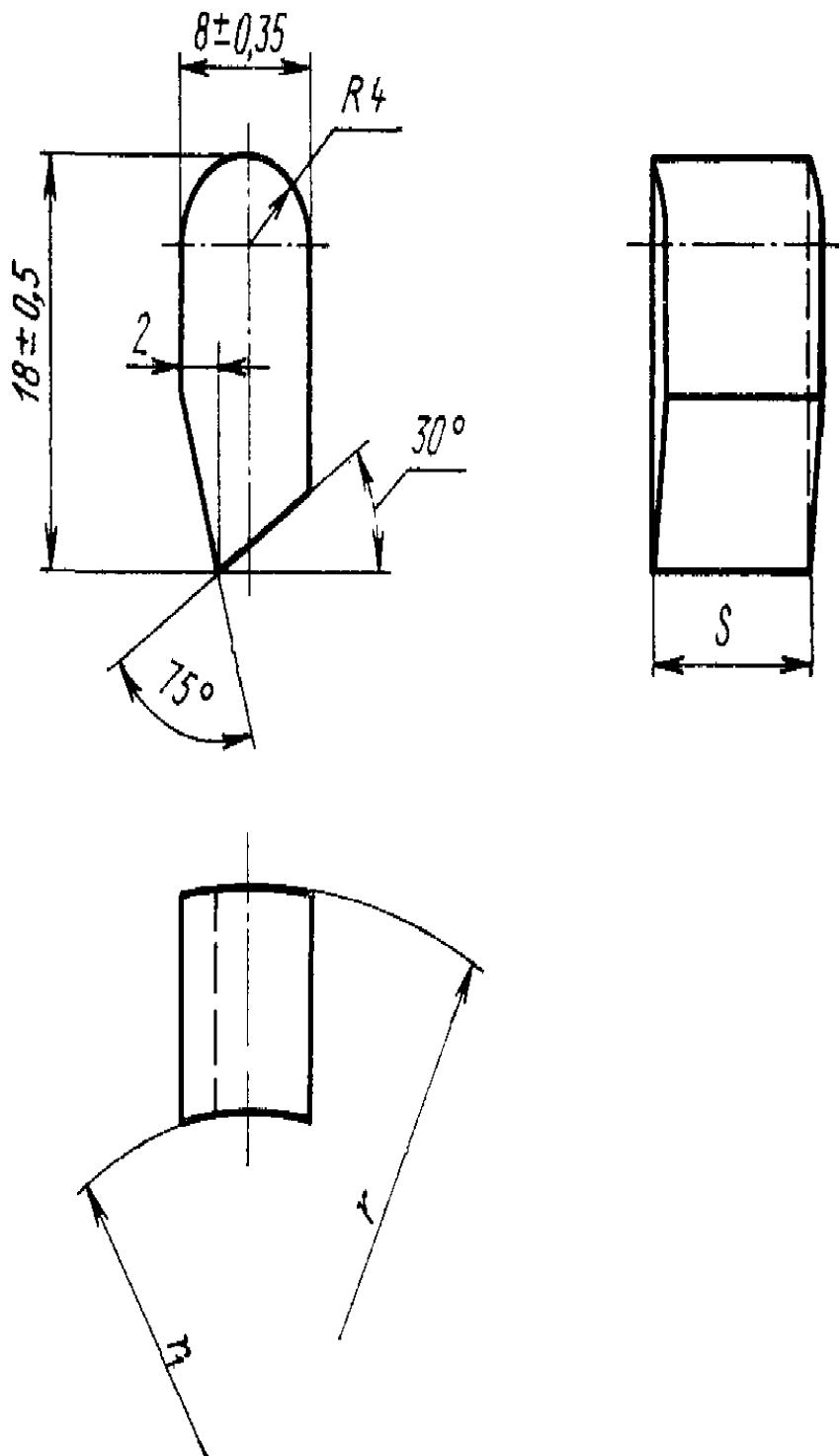
.24

14

	d ($+0,3$)	h			d ($+0,3$)	h	
5401	3,2	3	$\pm 0,15$	5408	7,2	5	$\pm 0,20$
5402	4,2	4		5409	8,2	8	$\pm 0,25$
5403	5,2	5	$\pm 0,20$	5410		7	
5404		4	$\pm 0,15$	5411		6	$\pm 0,20$
5405	6,2	6	$\pm 0,25$	5412	10,2	8	$\pm 0,25$
5406		5	$\pm 0,20$	5413	12,2	10	$\pm 0,30$
5407	7,2	6	$\pm 0,25$	5414		8	$\pm 0,25$

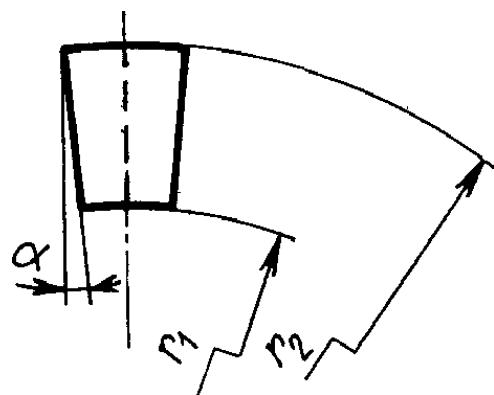
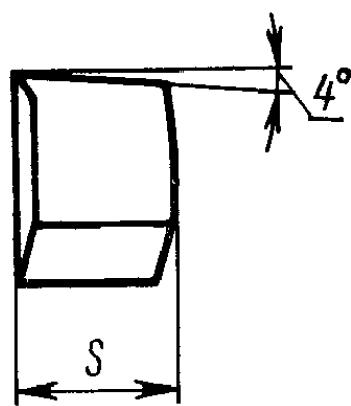
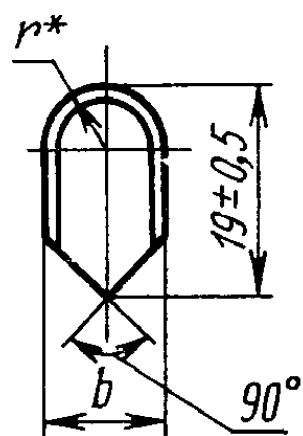
55

		15	
	s $(\pm 0,35)$	1	
		± 1	
5501	10,7	29,5	19,5
5502	17,7	38,0	21,0



.25

57

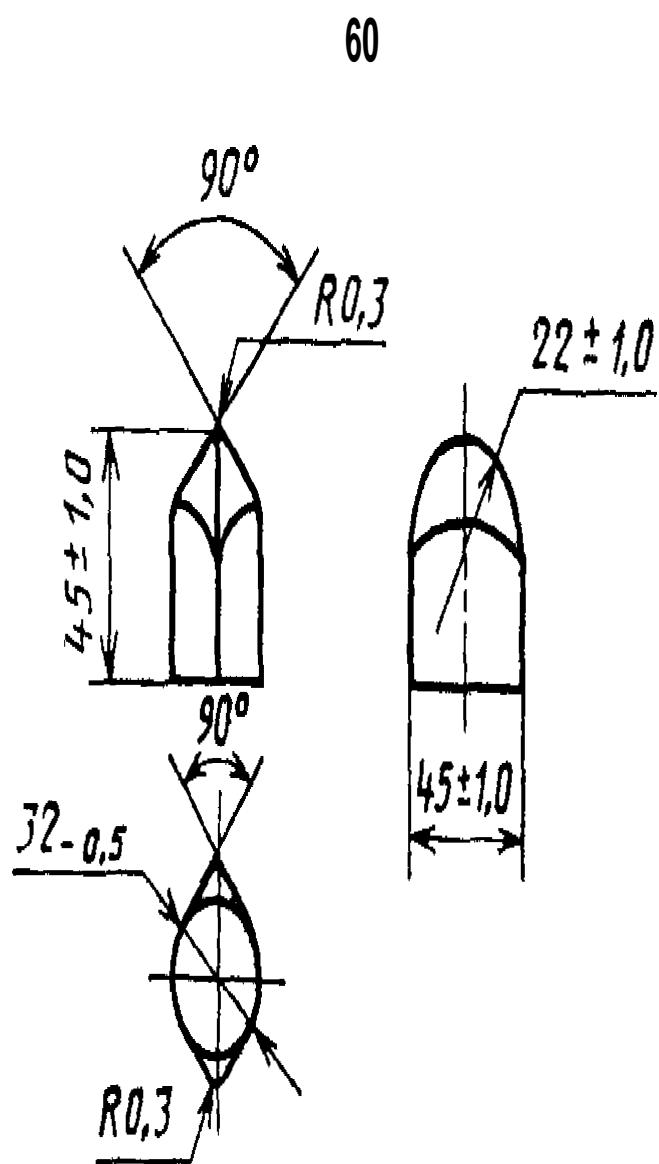


*

. 26

16

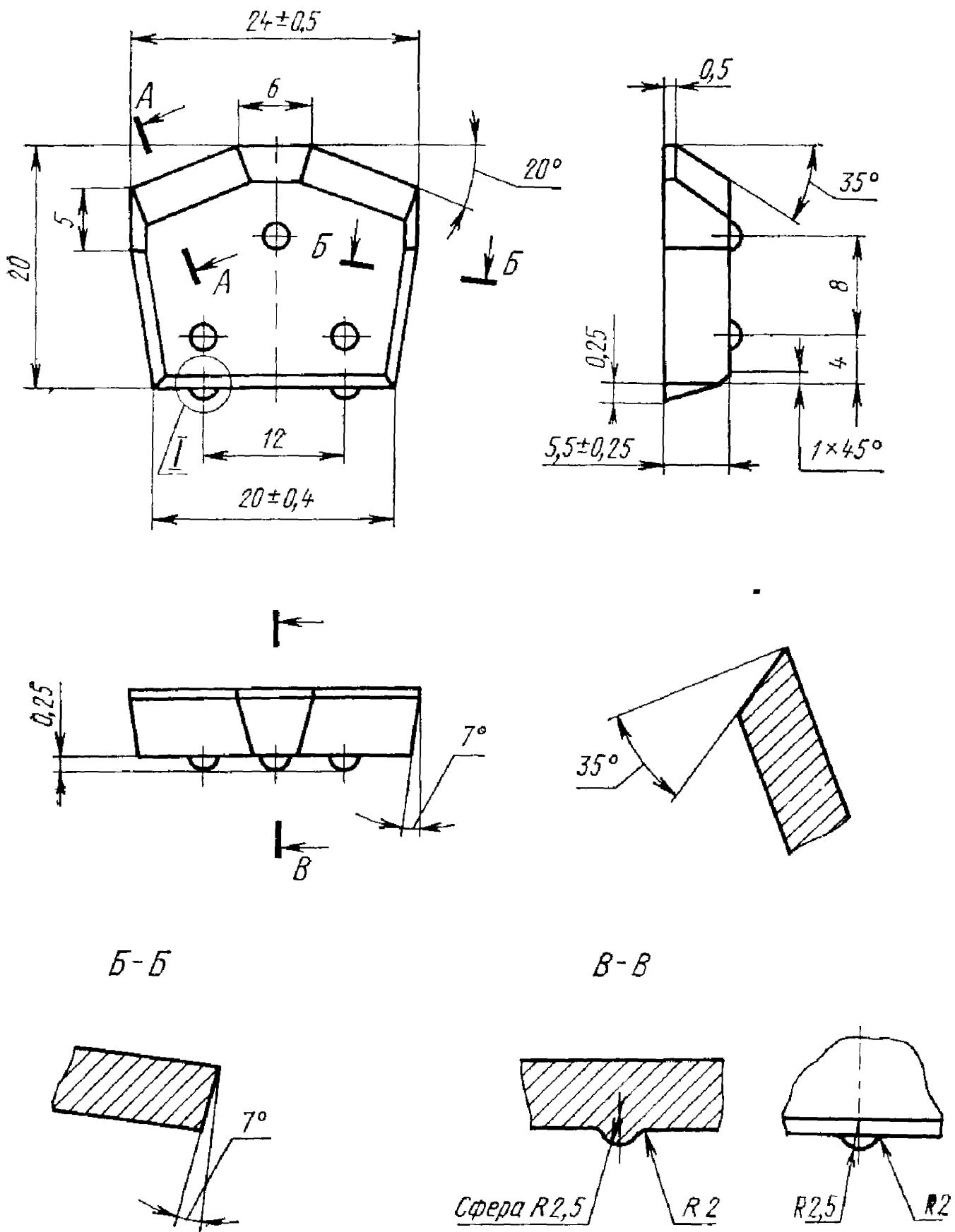
	(±0,35)	(±0,4)		1	2	
	. ±1					
5701	10,7	9	4,5	19,5	29,5	2°
5702	12,7	10	5,0	26,0	38,0	
5703	14,7	11	5,5	43,0	57,5	4°



Черт. 29*

*.27,28

61

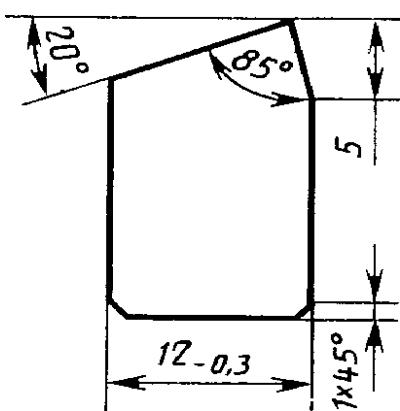
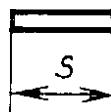


19**

63

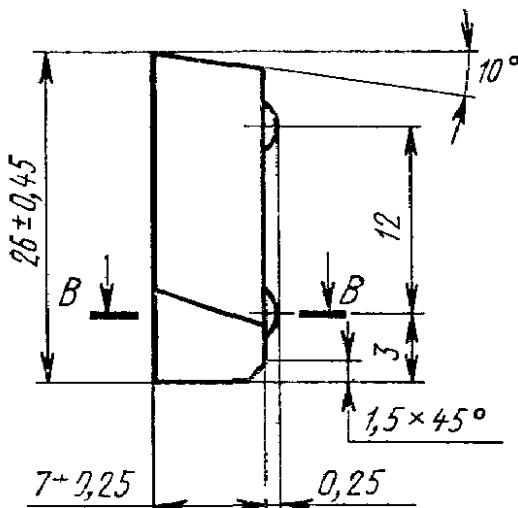
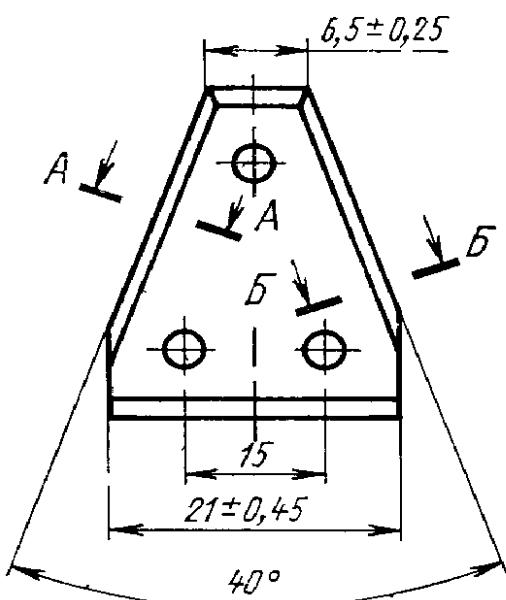
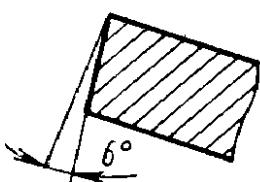
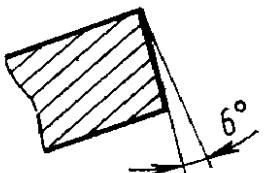
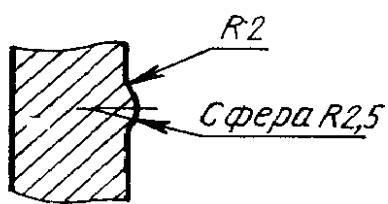
 $(\pm 0,4)$
 s

6301	6
6302	8
6303	10


 $\ll 5$
 $+1$


, 32* **

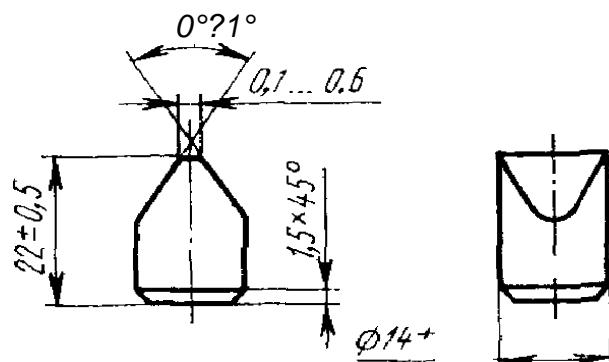
64

A-AB-BB-B

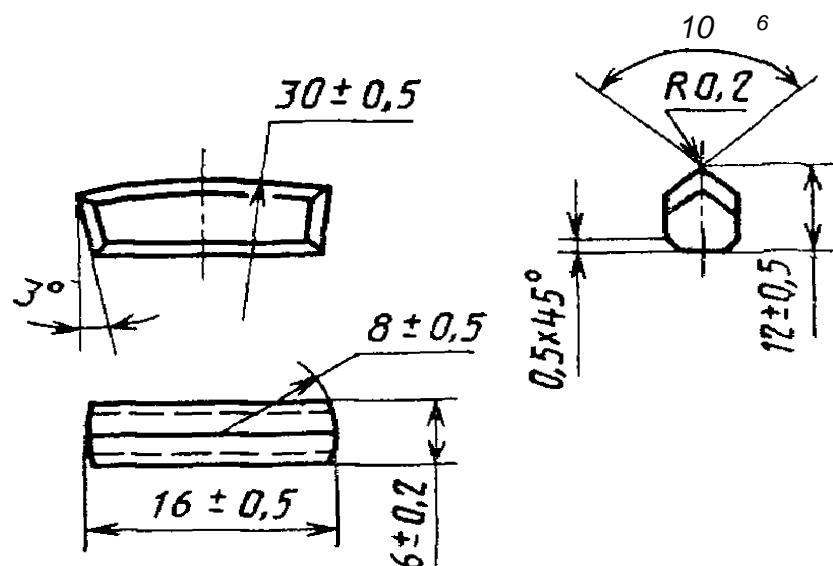
33

 $* .31$
 $** .17, 18$

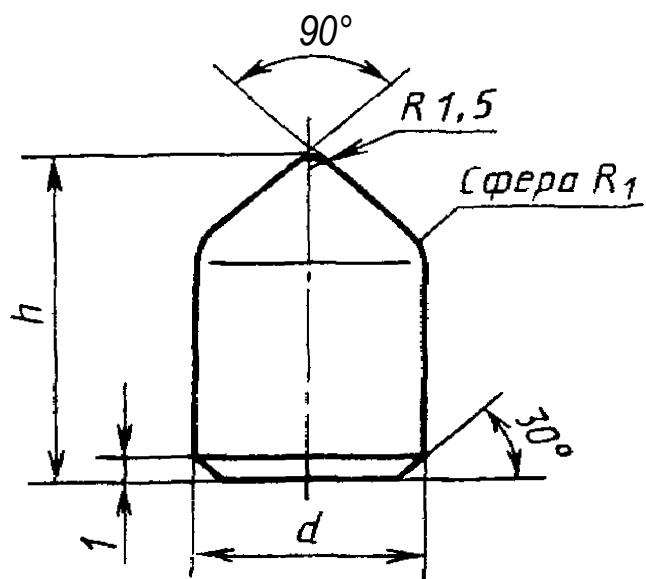
65



Черт. 34
Форма Г66



Черт. 35
Форма Г67



21 *

	<i>d</i>		<i>h</i>		*1
	
6701	7	0,3	15	+0,45	3,5
6702	9	±0,3	17	±0,45	4,5
67 03	12	± >	20	+0,60	6,0
6704	16	±0,3	24	±0,60	8,0

* 20

$$(\quad). \quad 15 \quad (16) \quad : \quad , \quad \underline{\quad} \quad 5 \quad (6) \quad . \quad 2-21.$$

$$\begin{array}{r}
 11 \\
 - 16 \\
 \hline
 5 - 7,5 \\
 \hline
 19\ 6533\ 2852\ 1101 \\
 \hline
 880 - 75
 \end{array}$$

1101 8— 880—75.

$$I = 13, \quad 5 - 4, \quad = 4,5, \quad 24, \quad hi = 3, \quad = 9, \quad / = 16, \quad \backslash = 6, \\ os = 10^\circ, cci = 3^\circ$$

19 6533 2859 24 -02 880-75

24 : 24 = 02 8— 880—75

1, 2. (, , 1, 2).
3.

($\dots, \dots, \dots, -1$).

4.

5°..... + ;
. 5° 15°..... ±1°;
. 15°..... ±2°

5. , ,
24, 24, 25, 26 67

(, . . . , 2).

.34 880-75

6. 23, 25, 26 54

7.

34, 34 , 36, 37 25°.

(, . 2).

8. 2601— 2605

0,3

9. 11, 12, 13, 14, 23, 24 65 -
30-50 . . ,

0,1
65 014+0-3

(, . 1).

10.

3882-74.

11. - 4411-79.

12.

-			-			
1101		43,5		1107		94,8
1102		50,9		1108		103,5
1103		56,9	11	1109	6	113,1
1104		70,1		1110		111,6
1105		58,7				
1106	15	82,5				
1107		89,1		1201		18,5
1108		97,3		1202		20,2
1109		106,3		1203		26,6
1110		106,0		1204		23,4
				1205	15	29,0
				1206		34,8
1101		44,6		1207		30,3
102		52,2		1208		39,4
1103		58,3				
1104		71,8				
1105		60,1				
1106	11	84,5		1201		18,9
1107		91,3		1202		20,7
1108		99,7		1203		27,3
1109		108,4		1204		24,0
1110		108,0		1205	11	29,7
				1206		35,6
			12	1207		31,0
1101		45,7		1208		40,4
1102		53,5				
1103		59,8				
1104		73,6		1201		19,4
1105		61,6		1202		21,2
1106	8	86,6		1203		27,9
1107		93,5		1204		24,6
1108		102,1		1205	8	30,5
1109		111,6		1206		36,5
		110,3		1207		31,8
				1208		41,3
1101		46,3				
1102		54,2				
1103	6	60,6		1201		19,7
1104		74,6		1202	6	21,5
1105		62,5		1203		28,3
1106		87,7		1204		24,9

2515		6,2		2606	1.7
2516		11,0		2607	4.1
2517		10,0		2608	3.0
2518		9,0		2609	2.5
2519		8,1		2610	2.2
2520		16,2		2611	5.9
2521		15,0		2612	5.3
2522		13,9		2613	4.7
2523		12,8		2614	4.1
2524		11,6		2615	3.5
2525		17,7		2616	2.9
2526		16,4		2617	9;i
2527		15,5		2618	8,4
2528		14,0		2619	7,6
2529		12,7		2620	6,8
2530		11,6		2621	6,0
2531		10,5		2622	5,2
2532		24,8		2623	4,4
2533		24,6		2624	12,3
2534		23,0		2625	11,3
2535	15;	19,8		2626	10,3
25	2536	11	18,2	2627	9,3
	2537		30,5	2628	8,4
	2538		27,7	2629	8 ;
	2539		26,2	2630	7,4
	2540		24,6	2631	6,4
	2541		23,1	2632	17,3
	2542		39,2	2633	16,0
	2543		38,9	2634	14,9
	2544		33,9	2635	13,7
	2545		30,2	2636	13,2
	2546		26,9	2637	11,2
	2547		46,8	2638	10,0
	2548		44,2	2639	8,8
	2549		41,6	2640	20,5
	2550		39,1	2641	19,1
	2551		36,5	2642	17,6
	2552		58,2	2643	16,2
	2553		52,4	2644	14,7
	2554		46,5	2645	13,3
	2555		43,6	2646	11,8
	2556		40,7	2647	27,8
				2648	26,1
				2649	24,2
				2650	22,5
	2601		0,5	2651	20,7
	2602	8 :	1,0	2652	18,9
26	2603	8	0,8	2653	17,2
			2,2	2654	15,5
	2605		1,9		34,1

2655		32,0		4101		1,0
2656		29,9		4102		7,1
2657		27,9		4103	6	14,2
2658		25,9		4104		1,2
2659		23,8		4105		1,3
2660		21,8		4106		1,5
2661		19,7				
2662		43,7				
2663		41,3	41			
2664		36,5		4101		0,9
2665		34,2		4102		7,0
2666		31,8		4103	8	14,0
2667		29,4		4104		1,1
2668		27,0		4105		1,2
2669	8	24,7		4106		1,4
2670	8	52,1				
2671		49,4				
2672		46,7				
2673		44,0		5101		1,5
2674		41,2		5102		3,2
2675		38,5		5103		2,9
2676		36,8		5104		3,6
2677		35,8		5105		7,8
2678		64,7		106		0,8
2679		58,5		5107		2,3
2680		52,3		5108		1,1
2681		49,2		5109		1,4
2682		46,1		5110		1,0
2683		43,0		5111		3,5
2684		40,0				
32	—	30,0	51			
	—	14,0		5101		1,4
	—			5102		3,1
	—			5103		2,8
34	—	11,8		5104		3,5
	—			5105		7,7
34	—	11,8		5106	8	0,8
	—			5107		2,2
36	—	10,0		5108		1,0
	—			5109		1,3
37	—	8,0		5110		
	—			5111		3,4
38	—.	14,0				
40	—	14,9				

1,2).

11	15 8- 6-	19 6527 2852 19 6534 2852 19 6533 2852 19 6532 2852
12	15 1 8- 6-	19 6527 2853 19 6534 2853 19 6533 2853 19 6532 2853
13	15 11- 8-	19 6527 2854 19 6534 2854 19 6533 2854
14	15 -	19 6527 2855 19 6534 2855
22	6-	19 6532 2856
23	8 11-	19 6525 2857 19 6537 2857
24	8-	19 6533 2858
24	8-	19 6533 2859
25	15 -	19 6527 2860 6537 2860
26	BK8-B 8-	19 6533 2861 19 6535 2861

32	8	19 6525 2862
	8	19 6525 2863
34	8	19 6525 2864
34	8	19 6525 2865
36	8	19 6525 2866
37		19 6525 2867
38	8	19 6525 2868
40		19 6525 2877
41	8	19 6524 2870 19 6525 2870
51	8	19 6524 2871 19 6525 2871
53	8	19 6525 2872
54	6- 4-	19 6532 2873 19 6531 2873
55	15	19 6527 2874
57	15	19 6527 2878
60	6	19 6524 2880
61	8-	19 6533 2881
63	8	19 6525 2883
64	8	19 6525 2884
65	8	19 6525 2885
66	6- 15 8-	19 6532 2886 19 6527 2886 19 6533 2886
67	8-	19 6533 2887

(, . 2).

3 880—75

25.01.89

01.07.89

2. 11 4107, 4108

			<i>h</i>		<i>s</i>	
	.	,	,	,	,	,
4107		$\pm 0,15$				
4108	3,0	$\pm 0,20$	10	$\pm 0,25$	1.5	$\pm 0,15$

(. . 84}

НВС № 4 1989 г.)

Л'0

0,5

BK6, BK8

Л4108

Л4107

Л41

Изготавливается
стеклоподъемниками

Макет реального
изображения

Изготавливается
стеклоподъемниками

Изготавливается
стеклоподъемниками

Установка изображения
стеклоподъемниками

4 880-75

,

18.10,91 1(28

(1): «
».

	(. . +0,5)	(, , tW)	(. . +15)	*	(, ,
313	23	20	11,5	6	30

(
10 : «
11, 12, 13, 14 10-
4 6 >
1. 11, 12, 13, 14.
: 11 BR11B; .
13 1313
:

	1313	11 ; -	74,4

2, 11, 12, 13, 14 : 19 6536 2852

(ИУС № 1 1992 г.)

Редактор Р. Г. Говердовская

Технический редактор Э. В. Митай

Корректор Г. И. Чуйко

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S**

**mol
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Hz	N	~ ¹ * * —2
J	~' • "2	
W	2 * - "2	
V	2 - "3	
F	•	
S	2 ~ ³ ~	
Wb	m“2ki—! * 4- 2	
	2* - ~Λ *2	
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1	2 • - _2 " "	
1	~2 * -1	
Bq	2* - "2 * *2	
Gy	•	
Sv	"2 •	
		"1
		2 - 2
		2 • "2

*